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### 1 **Low magnetic damping of ferrimagnetic GdFeCo alloys**

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**We investigate the Gilbert damping parameter** α **for rare earth (RE)– transition metal (TM) ferrimagnets over a wide temperature range. Extracted from the field-driven magnetic domain-wall mobility,**  $\alpha$  **was as low as the order of**  $10^{-3}$  **and was almost constant across the angular momentum compensation temperature**  $T_A$ **, starkly contrasting previous predictions that**  $\alpha$  **should diverge at**  $T_A$  **due to vanishing total angular momentum. Thus, magnetic damping of RE-TM ferrimagnets is not related to the total angular momentum but is dominated by electron scattering at the Fermi level where the TM has a dominant damping role.**

Magnetic damping, commonly described by the Gilbert damping parameter, represents the magnetization relaxation phenomenon, describing how quickly magnetization spins reach equilibrium [1–3]. Understanding the fundamental origin of the damping as well as searching for low damping materials has been a central theme of magnetism research. Several theoretical models for magnetic damping have been proposed [4–11] and compared with experiments [12–20]. Ultra-low damping was predicted in ferromagnetic alloys using a linear response damping model [11] and was demonstrated experimentally for CoFe alloys [20]. However, the majority of these studies have focused only on ferromagnetic systems.

Antiferromagnets, which have alternating orientations of their neighboring magnetic moments, have recently received considerable attention because of their potential importance for spintronic applications [21–30]. Antiferromagnetic spin systems can have much faster spin dynamics than their ferromagnetic counterparts, which is advantageous in spintronic applications [21, 25, 31–39]. However, the manipulation and control of antiferromagnets is challenging because the net magnetic moment is effectively zero. Recently, antiferromagnetic spin dynamics have been successfully demonstrated using the magnetic domain-wall (DW) dynamics in ferrimagnets with finite magnetization in the vicinity of the angular momentum compensation temperature, at which the net angular momentum vanishes [38]. This field-driven antiferromagnetic spin dynamics is possible because the time evolution of the magnetization is governed by the commutation relation of the angular momentum rather than the commutation relation of the magnetic moment.

Motivated by the aforementioned result, in this letter, we investigate the magnetic damping of ferrimagnets across the angular momentum compensation temperature, which will allow us to understand magnetic damping in antiferromagnetically coupled system. We selected rare earth (RE)–transition metal (TM) ferrimagnets for the material platforms 57 because they have an angular momentum compensation temperature  $T_A$  where antiferromagnetic spin dynamics are achieved [38, 40, 41]. The magnetic-field-driven DW 59 motion was explored over a wide range of temperatures including  $T_A$ , and the Gilbert damping parameter was extracted from the measured DW mobility at each temperature by employing the collective coordinate model initially developed for ferrimagnetic spin dynamics [38]. Contrary to the previous prediction that the Gilbert damping parameter would 63 diverge at  $T_A$  due to the vanishing of the total angular momentum [42, 43], we found that the Gilbert damping parameter remained nearly constant over a wide range of temperatures 65 across  $T_A$  with the estimated value as low as the order of  $10^{-3}$ , which was similar to the reported values of TM-only ferromagnets [20]. These results suggest that Gilbert damping is mainly governed by electron scattering at the Fermi level, and hence, the 4f electron of the RE element, which lies far below the Fermi level, does not play an important role in the magnetic damping of RE–TM ferrimagnets.

For this study, we prepared perpendicularly magnetized ferrimagnetic GdFeCo films in which the Gd and FeCo moments were coupled antiferromagnetically. Specifically, the 72 films were 5-nm SiN/30-nm  $Gd_{23.5}Fe_{66.9}Co_{9.6}/100$ -nm SiN on an intrinsic Si substrate. The GdFeCo films were then patterned into 5-µm-wide and 500-µm-long microwires with a Hall cross structure using electron beam lithography and Ar ion milling. For current injection, 100-nm Au/5-nm Ti electrodes were stacked on the wire. A Hall bar was designed to detect the DW velocity via the anomalous Hall effect (AHE).

We measured the magnetic DW motion using a real-time DW detection technique [38, 40, 41, 44, 45] [see Fig. 1(a) for a schematic]. We first applied a magnetic field higher than

coercive field to saturate the magnetization along the –z direction. Subsequently, a constant 80 perpendicular magnetic field  $\mu_0 H$ , which was lower than the coercive field, was applied along +z direction. Next, a d.c. current was applied along the wire to measure the anomalous Hall voltage. Then, a current pulse (12 V, 100 ns) was injected through the writing line to nucleate the DW in the wire. The created DW was moved along the wire and passed through 84 the Hall bar because of the presence of  $\mu_0 H$ . The DW arrival time was detected by monitoring the change in the Hall voltage using a real-time oscilloscope. The DW velocity could then be calculated from the arrival time and the travel distance between the writing line 87 and the Hall bar  $(400 \mu m)$ .

88 Figure 1(b) shows the averaged DW velocity  $\langle v \rangle$  as a function of the perpendicular 89 magnetic field  $\mu_0 H$  for several temperatures  $T^*$ . Here, we used the d.c. current density of 90 |J| =1.3×10<sup>10</sup> A/m<sup>2</sup> to measure the AHE change due to DW motion. Note that  $T^*$  is a 91 calibrated device temperature where Joule heating by d.c. current is considered [46]. To 92 eliminate the undesired current-induced spin-transfer-torque effect, we averaged the DW 93 velocity for +*J* and  $-J$ , i.e.,  $\langle v \rangle = [v(+J) + v(-J)]/2$ . Figure 1(b) shows that  $\langle v \rangle$ 94 increases linearly with  $\mu_0 H$  for all  $T^*$ . Such linear behavior can be described by  $\langle v \rangle =$ 95  $\mu[\mu_0H - \mu_0H_0]$ , where  $\mu$  is the DW mobility and  $\mu_0H_0$  is the correction field, which 96 generally arises from imperfections in the sample or complexities of the internal DW 97 structure [47, 48]. We note that  $\mu_0 H_0$  can also depend on the temperature dependence of the 98 magnetic properties of ferrimagnets [45]. Figure 1(c) shows  $\mu$  as a function of  $T^*$  at several expansion of the current densities ( $|J| = 1.3$ , 1.7, and  $2.0 \times 10^{10}$  A/m<sup>2</sup>). A sharp peak clearly occurs for  $\mu$  at 100  $T^* = 241.5$  K irrespective of |J|. The drastic increase of  $\mu$  is evidence of antiferromagnetic 101 spin dynamics at  $T_A$ , as demonstrated in the previous reports [38, 40, 41].

102 The obtained DW mobility was theoretically analyzed as follows. The DW velocity 103 of ferrimagnets in the precessional regime is given by [38, 39]

$$
V = \lambda \alpha \frac{(s_1 + s_2)(M_1 - M_2)}{[\alpha(s_1 + s_2)]^2 + (s_1 - s_2)^2} \mu_0 H,\tag{1}
$$

104 where V is the DW velocity,  $\lambda$  is the DW width,  $\mu_0 H$  is the perpendicular magnetic field, 105  $\alpha$  is the Gilbert damping parameter which is the phenomenological dimensionless number 106 describing the energy-dissipation rate associated with the dynamics of the collinear order,  $M_i$ 107 and  $s_i$  are the magnetization and the spin angular momentum of one sublattice, respectively. 108 The spin angular momentum densities are given by  $s_i = M_i / \gamma_i$  [49], where  $\gamma_i = g_i \mu_B / \hbar$  is the gyromagnetic ratio of lattice *i*,  $g_i$  is the Landé g-factor of lattice *i*,  $\mu_B$  is the Bohr 110 magneton, and  $\hbar$  is the reduced Plank's constant. Eq. (1) gives the DW mobility  $\mu$  as 111  $\lambda \alpha (s_1 + s_2)(M_1 - M_2)/{\lbrace [\alpha (s_1 + s_2)]^2 + (s_1 - s_2)^2 \rbrace}$ , which can be rearranged as

$$
\mu(s_1 + s_2)^2 \alpha^2 - \lambda(s_1 + s_2)(M_1 - M_2)\alpha + \mu(s_1 - s_2)^2 = 0
$$
\n(2)

112 Using Eq. (2) to find the solution of  $\alpha$ , we find

$$
\alpha_{\pm} = \frac{\lambda (M_1 - M_2) \pm \sqrt{[\lambda^2 (M_1 - M_2)^2 - 4\mu^2 (s_1 - s_2)^2]}}{2\mu (s_1 + s_2)}.
$$
\n(3)

113 Eq. (3) allows us to estimate  $\alpha$  for the given  $\mu$ . We note that for each value of  $\mu$ ,  $\alpha$  can 114 have two values,  $\alpha_+$  and  $\alpha_-$  because of the quadratic nature of Eq. (2). Only one of these 115 two solutions is physically sound, which can be obtained using the following energy 116 dissipation analysis.

117 The energy dissipation (per unit cross section) through the DW dynamics is given by 118  $P = 2\alpha(s_1 + s_2)V^2/\lambda + 2\alpha(s_1 + s_2)\lambda\Omega^2$  [38, 39], where  $\Omega$  is the angular velocity of the

119 DW. The first and the second terms represent the energy dissipation through the translational 120 and angular motion of the DW, respectively. In the precessional regime, the angular velocity is proportional to the translational velocity:  $\Omega = (s_1 - s_2)V/\alpha(s_1 + s_2)\lambda$ . Replacing  $\Omega$  by the previous expression yields  $P = \eta V^2$  where  $\eta = 2(M_1 - M_2)/\mu$  is the viscous 123 coefficient for the DW motion:

$$
\eta = \frac{2}{\lambda} \left\{ \alpha(s_1 + s_2) + \frac{(s_1 - s_2)^2}{\alpha(s_1 + s_2)} \right\}.
$$
\n(4)

124 The first and the second terms in parenthesis capture the contributions to the energy 125 dissipation from the translational and angular dynamics of the DW, respectively. The two 126 solutions for the Gilbert damping parameter,  $\alpha_+$  and  $\alpha_-$ , can yield the same viscous 127 coefficient  $\eta$ . The case of the equal solutions,  $\alpha_+ = \alpha_-$ , corresponds to the situation when the two contributions are identical:  $\alpha_{\pm} = (s_1 - s_2)/(s_1 + s_2)$ . For the larger solution 129  $\alpha = \alpha_+$ , the energy dissipation is dominated by the first term, i.e., through the translational 130 DW motion, which should be the case in the vicinity of  $T_A$  where the net spin density 131  $(s_1 - s_2)$  is small and thus the angular velocity is negligible. For example, at exact  $T_A$ , the 132 larger solution  $\alpha_+$  is the only possible solution because the smaller solution is zero,  $\alpha_- = 0$ , 133 and thus unphysical. For the smaller solution  $\alpha = \alpha_{-}$ , the dissipation is dominated by the 134 second term, i.e., through the precessional motion, which should describe cases away from 135  $T_A$ . Therefore, in the subsequent analysis, we chose the larger solution  $\alpha_+$  in the vicinity of 136  $T_A$  and the smaller solution  $\alpha$  far away from  $T_A$  and connected the solution continuously 137 in between.

The other material parameters such as  $M_1$ ,  $M_2$ ,  $S_1$ , and  $S_2$  are estimated by 139 measuring the net magnetic moment of GdFeCo film,  $|M_{net}|$ , for various temperatures.

140 Because  $M_{\text{net}}$  includes contributions from both the Gd and FeCo sub-moments, the subnagnetic moments,  $M_1$  and  $M_2$ , could be decoupled based on the power law criticality [see 142 details in refs. 38, 40]. The spin angular momentums,  $s_1$  and  $s_2$ , were calculated using the 143 known Landé g-factor of FeCo and Gd (the Landé g-factor of FeCo is 2.2 and that of Gd is 144 2.0) [50–52].

145 Figures 2(a)–(c) show the temperature-dependent DW mobility  $\mu$ , sub-magnetic 146 moment  $M_i$ , and sub-angular momentum  $s_i$ , respectively. Here, we used the relative temperature defined as  $\Delta T = T^* - T_A$  to investigate the Gilbert damping near  $T_A$ . The 148 Gilbert damping parameter  $\alpha$  was obtained based on Eq. (3) and the information in Fig. 149 2(a)–(c). Figure 2(d) shows the resulting values of  $\alpha_{\pm}$  as a function of  $\Delta T$ . For  $\Delta T_1$  <  $\Delta T < \Delta T_2$ ,  $\alpha_+$  is nearly constant, while  $\alpha_-$  varies significantly. For  $\Delta T < \Delta T_1$  and  $\Delta T > \Delta T_2$ , on the other hand,  $\alpha_-$  is almost constant, while  $\alpha_+$  varies significantly. At 152  $\Delta T = \Delta T_1$  and  $\Delta T = \Delta T_2$ , the two solutions are equal, corresponding to the aforementioned 153 case when the energy dissipation through the translational and angular motion of the DW are 154 identical.

155 The proper damping solution can be selected by following the guideline obtained from the above analysis. For  $\Delta T_1 < \Delta T < \Delta T_2$ , which includes  $T_A$ , the energy dissipation 157 should be dominated by the translational motion, and thus  $\alpha_+$  is a physical solution. Note 158 also that  $\alpha_{-}$  becomes zero at  $T_A$ , which results in infinite DW mobility in contradiction with the experimental observation. For  $\Delta T < \Delta T_1$  and  $\Delta T > \Delta T_2$ , where the energy dissipation is 160 dominated by the angular motion of the DW,  $\alpha_{-}$  is the physical solution.

161 Figure 3 shows the resultant Gilbert damping parameter in all tested temperature

162 ranges. The Gilbert damping parameter was almost constant across  $T_A$  with  $\alpha = 7.2 \times 10^{-3}$ (see the solid line in Fig. 3). This result is in stark contrast to the previous prediction. In ref. [42], Stanciu *et al*. investigated the temperature dependence of the effective Gilbert damping 165 parameter based on a ferromagnet-based model and found that the damping diverged at  $T_A$ because they analyzed the magnetic resonance in ferrimagnetic materials based on a ferromagnet-based model. By modifying the ferromagnet-based model to describe general ferrimagnets with the tunable spin density, it is possible to analyze the magnetic resonance in ferrimagnetic/antiferromagnetic materials and the correct Gilbert damping parameter can be obtained. However, our theoretical analysis for field-driven ferromagnetic DW motion based on the collective coordinate approach can properly describe both the antiferromagnetic 172 dynamics in the vicinity of  $T_A$  and the ferromagnetic dynamics away from  $T_A$  [38]. 173 Therefore, the unphysical divergence of the Gilbert damping parameter at  $T_A$  is absent in our analysis.

Our results, namely the insensitivity of damping to the compensation condition and its low value, have important implications not only for fundamental physics but also for technological applications. From the viewpoint of fundamental physics, nearly constant 178 damping across  $T_A$  indicates that the damping is almost independent of the total angular momentum and is mostly determined by electron spin scattering near the Fermi level. Specifically, our results suggest that the 4f electrons of RE elements, which lie in a band far below the Fermi level, do not play an important role in the magnetic damping of RE-TM ferrimagnets, whereas the 3d and 4s bands of TM elements have a governing role in magnetic damping. This result is consistent with the recently reported theoretical and experimental results in FeCo alloys [20]. From the viewpoint of practical application, we note that the 185 estimated damping of  $\alpha = 7.2 \times 10^{-3}$  is the upper limit, as the damping estimated from DW dynamics is usually overestimated due to disorders [53]. The experimental results from FMR measurements and the corresponding theoretical analysis will be published elsewhere. This low value of the Gilbert damping parameter suggests that ferrimagnets can serve as versatile platforms for low-dissipation high-speed magnetic devices such as spin-transfer-torque magnetic random-access memory and terahertz magnetic oscillators.

In conclusion, we investigated the field-driven magnetic DW motion in ferrimagnetic 192 GdFeCo alloys over a wide range of temperatures across  $T_A$  and extracted the Gilbert damping parameter from the DW mobility. The estimated Gilbert damping parameter was as 194 low as the order of  $10^{-3}$  and almost constant over the temperature range including  $T_A$ , which is in stark contrast to the previous prediction in that the Gilbert damping parameter would 196 diverge at  $T_A$  due to the vanishing total angular momentum. Our finding suggests that the magnetic damping of RE-TM ferrimagnets is not related to the total angular momentum but is mostly governed by the scattering of electrons at the Fermi level where the TM element has a dominant role for the magnetic damping.

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### 289 **Figure Captions**

290 Figure 1(a) Schematic illustration of the GdFeCo microwire device. (b) The averaged DW

291 velocity  $\langle v \rangle$  as a function of the perpendicular magnetic field  $\mu_0 H$  for several temperatures

292  $T^*$  (202, 222, 242, 262, and 282 K). The dots indicate the best linear fits. (c) The DW

293 mobility  $\mu$  as a function of  $T^*$  at several current densities ( $|J| = 1.3$ , 1.7, and 2.0 ×10<sup>10</sup> 294  $A/m^2$ ).

Figure 2 The temperature-dependent (a) DW mobility  $\mu$ , (b) sub-magnetic moment  $M_i$ , and 296 (c) sub-angular momentum  $s_i$ . Here, we use the relative temperature defined as  $\Delta T = T^*$  – 297  $T_A$ . (d) The Gilbert damping parameter  $\alpha_{\pm}$  as a function of  $\Delta T$ . Here, we use  $\lambda = 15$  nm for 298 proper solutions of Eq. (3).

299 Figure 3 The resultant Gilbert damping parameter  $\alpha$  as a function of  $\Delta T$  (see the open 300 circles). The purple solid line indicates  $\alpha = 7.2 \times 10^{-3}$ .

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### **Competing financial interests**

The authors declare no competing financial interests.





### Figure 1



# Figure 2

## Figure 3

