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Yuri Lubomirsky, Chih-Hung Chen, Alain Karma, and Eran Bouchbinder Phys. Rev. Lett. **121**, 134301 — Published 25 September 2018 DOI: 10.1103/PhysRevLett.121.134301

Universality and stability phase-diagram of two-dimensional brittle fracture

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The two-dimensional oscillatory crack instability, experimentally observed in a class of brittle materials under strongly dynamic conditions, has been recently reproduced by a nonlinear phase-field fracture theory. Here we highlight the universal character of this instability by showing that it is present in materials exhibiting widely different near crack tip elastic nonlinearity, and by demonstrating that the oscillations wavelength follows a universal master curve in terms of dissipation-related and nonlinear elastic intrinsic length scales. Moreover, we show that upon increasing the driving force for fracture, a high-velocity tip-splitting instability emerges, as experimentally demonstrated. The analysis culminates in a comprehensive stability phase-diagram of two-dimensional brittle fracture, whose salient properties and topology are independent of the form of near tip nonlinearity.

Cracks mediate materials failure and hence understanding their spatiotemporal dynamics is of prime fundamental and practical importance [1-5]. It is experimentally well-established that cracks in brittle materials undergo various symmetry-breaking instabilities [5– 13]. Most notably, straight cracks in three-dimensional (3D) samples of isotropic materials universally undergo a micro-branching instability, where short-lived microcracks branch out sideways from the main crack, at low to medium propagation velocities [5–11]. Recent experiments performed on a class of neo-Hookean (NH) — a nonlinear extension of linear, Hookean elasticity — brittle materials revealed that upon reducing the system's thickness, approaching the two-dimensional (2D) limit, the micro-branching instability is severely suppressed; as a result, straight cracks accelerate to unprecedentedly high velocities, approaching the relevant sonic velocity, until they undergo an oscillatory instability [4, 12, 13].

Our understanding of these dynamic fracture instabilities is far from complete. In particular, the classical theory of brittle cracks — Linear Elastic Fracture Mechanics (LEFM) [1, 2] — intrinsically falls short of explaining these instabilities [4, 14, 15]. Recently, integrating theoretical ideas about the existence and importance of elastic nonlinearity near cracks tips [4, 13, 16–19] into a phasefield fracture theory, the 2D oscillatory instability in brittle NH materials has been quantitatively reproduced in large-scale simulations for the first time [14], cf. Fig. 1a. The theory has shown, in agreement with experiments, that the wavelength of oscillations scales linearly with an intrinsic nonlinear elastic length scale, which does not exist in LEFM, hence explicitly demonstrating the failure of the classical theory of brittle cracks.

This significant progress raised several pressing questions of fundamental importance. First, is the oscillatory instability universal, i.e. observed in various brittle materials independently of the nature and form of near tip elastic nonlinearity? Second, what are the minimal physical conditions for the existence of the oscillatory instability? Third, are there additional, previously undiscov-



FIG. 1. (a) A zoom in on the 2D oscillatory instability in a phase-field simulation of brittle neo-Hookean (NH) materials under tensile (mode I) loading [14]. The color code corresponds to the normalized strain energy density and ξ is the dissipation length. (b) The same, but for brittle Saint-Venant-Kirchhoff (SVK) materials, see text and [20] for details. (c) Examples of the normalized crack speed v/c_s (c_s is the shear wave speed) vs. normalized crack propagation distance d/ξ for SVK (top curve) and NH materials (bottom curve). The onset of oscillations is marked by the horizontal dashed lines. (d) The uniaxial stress σ (normalized by the shear modulus μ) vs. strain ε for SVK (solid line) and NH materials (dashed line), along with their linear approximation (dashed-dotted line).

ered instabilities in 2D dynamic fracture? Finally, can one derive a comprehensive stability phase-diagram of two-dimensional brittle fracture and if so, is it universal? In this Letter, we extensively address these important questions using theoretical considerations and large-scale simulations in the framework of the recently developed nonlinear phase-field theory of fracture [14].

This theory belongs to a broader class of diffuseinterface approaches to fracture [21–26] that avoid the difficulty of tracking the evolution of sharp crack surfaces, and at the same time allow a self-consistent selection of the crack's velocity and path, which are far from being understood in general. These properties emerge from the dynamics of an auxiliary phase-field ϕ and its coupling to other fields, which provide a mathematical machinery that renders the fracture problem self-contained. In particular, it gives rise to a dissipation-related length scale ξ and a fracture energy $\Gamma(v)$ (the energy dissipated per unit crack surface, where v is the crack propagation). The smooth transition in space between the pristine ($\phi = 1$) and the fully broken ($\phi = 0$) states of the material is initiated when the elastic strain energy functional $e_{\text{strain}}(\mathbf{H})$ exceeds a threshold e_c , where $\boldsymbol{H} = \nabla \boldsymbol{u}$ is the displacement gradient tensor and $\boldsymbol{u}(x, y, t)$ is the displacement vector field.

Unlike previous phase-field approaches [22, 23, 25], the formulation in [14] maintains the wave speeds constant inside the dissipation zone, thereby allowing cracks to accelerate to unprecedentedly high velocities without undergoing tip-splitting instabilities at marginally dynamic velocities [27, 28]. Moreover, $e_{\text{strain}}(\boldsymbol{H})$ is taken to be nonlinear, introducing nonlinearity on a length ℓ in the near vicinity of the crack tip, while the linear elastic (quadratic) approximation to $e_{\text{strain}}(\boldsymbol{H})$ remains very good on larger scales. Hence, this theory features an intrinsic dissipation length ξ and intrinsic length ℓ associated with near tip elastic nonlinearity, which can be independently varied.

The strain energy functional $e_{\rm strain}^{\rm \scriptscriptstyle NH}({\pmb H})\!=\!\frac{1}{2}\mu({\rm tr}({\pmb F}^{\rm T}{\pmb F})\!+\!$ $[\det(\mathbf{F})]^{-2} - 3$) of 2D incompressible NH materials [29], where F = I + H (I is the identity tensor) and μ is the shear modulus, has been shown [14] to quantitatively predict the experimentally observed oscillatory instability in 2D brittle polymeric elastomers under tensile (mode I) loading conditions [4, 12, 13]. Most notably, the oscillations (see example in Fig. 1a) emerge at a critical velocity v_c (see the lower horizontal dashed line in Fig. 1c) and their wavelength follows $\lambda = \alpha \xi + \beta \Gamma_0 / \mu$ (shown by the squares in Fig. 2a), both in quantitative agreement with experiments [13, 14]. Here α and β are dimensionless numbers, ξ is the dissipation length defined above, $\Gamma_0 \equiv \Gamma(v \to 0)$ and Γ_0/μ is proportional to the intrinsic nonlinear elastic length ℓ [4, 13, 17, 19]. $e_{\text{strain}}^{\text{NH}}$ is of entropic origin, which is well-understood in terms of the statistical thermodynamics of cross-linked polymer chains [30].

To assess the generality of these results, our first goal is to consider near tip elastic nonlinearity which is sufficiently general, yet of qualitatively different physical origin and emerging properties compared to $e_{\text{strain}}^{\text{NH}}$. To that aim, we invoke the minimal elastic nonlinearity associated with the rotational invariance of isotropic materials. That is, we use the rotationally-invariant (Green-Lagrange) metric strain tensor $\boldsymbol{E} = \frac{1}{2}(\boldsymbol{F}^{\text{T}}\boldsymbol{F} - \boldsymbol{I}) = \boldsymbol{\varepsilon} + \frac{1}{2}(\boldsymbol{H}^{T}\boldsymbol{H})$, instead of its widespread linear approximation $\boldsymbol{\varepsilon} = \frac{1}{2}(\boldsymbol{H} + \boldsymbol{H}^{T})$ [31]. When combined with constitutive linearity, i.e. with a quadratic energy functional in which the linearized strain measure $\boldsymbol{\varepsilon}$ is replaced by its nonlinear rotationally-invariant counterpart \boldsymbol{E} , we obtain

$$e_{\text{strain}}^{\text{SVK}}(\boldsymbol{H}) = \frac{1}{2} \tilde{\lambda} \operatorname{tr}^{2}(\boldsymbol{E}) + \mu \operatorname{tr}(\boldsymbol{E}^{2}) \quad . \tag{1}$$

This energy functional, corresponding to Saint-Venant-Kirchhoff (SVK) materials [32], is constitutively identical to linearized Hookean elasticity (where $\tilde{\lambda}$ is the first Lamé constant [31]), but features geometric nonlinearity embedded inside \boldsymbol{E} .

While materials typically feature constitutive nonlinearity in addition to geometric nonlinearity, they should at least feature the latter, and hence Eq. (1) constitutes the minimal possible elastic nonlinearity. $e_{\rm strain}^{\rm SVK}$ is not only of a qualitatively different physical origin compared to $e_{\rm strain}^{\rm NH}$, but it also exhibits significantly different properties. In Fig. 1d, we plot the uniaxial tension response corresponding to the two functionals, in addition to their linear elastic approximation (the elastic constants are chosen such that the latter is identical for both functionals). We observe that $e_{\rm strain}^{\rm SVK}$ features a stronger nonlinearity than $e_{\rm strain}^{\rm NH}$ and is of strain-stiffening nature, while the latter is of strain-softening nature. Do materials described by $e_{\rm strain}^{\rm SVK}$ experience the same oscillatory instability as those described by $e_{\rm strain}^{\rm Strain}$?

In Fig. 1b we present results of a large-scale numerical simulation of the nonlinear phase-field fracture theory discussed above, using $e_{\text{strain}}^{\text{SVK}}$ (see simulation details in [20]). An oscillatory instability that is strikingly similar to the oscillatory instability shown in Fig. 1a for brittle NH materials is observed. The onset of instability, see example in Fig. 1c (top curve), takes place at an ultrahigh critical velocity v_c , whose normalized value is similar to the one of brittle NH materials (bottom curve). The fact that the oscillatory instability exists for widely different forms of near crack tip elastic nonlinearity provides a strong indication in favor of its universal nature. In Fig. 2a, we present the oscillations wavelength of brittle SVK materials demonstrating that it scales linearly with Γ_0/μ , $\lambda = \alpha \xi + \beta \Gamma_0/\mu$, exactly as it does for brittle NH materials, yet again supporting the universality of the oscillatory instability. Remarkably, while β is significantly larger for brittle SVK materials compared to brittle NH materials, $\alpha = 13 \pm 1$ is essentially identical for the two classes of materials.



FIG. 2. (a) The normalized oscillations wavelength λ/ξ vs. $\Gamma_0/\mu\xi$ for SVK (circles), NH (squares) and truncated NH (diamonds) materials. (b) The normalized nonlinear length ℓ/ξ (ℓ is defined in the text) vs. $\Gamma_0/\mu\xi$ for SVK (circles) and NH (squares) materials. (c) λ/ξ vs. ℓ/ξ for SVK (circles) and NH (squares) materials. The lines are guides to the eye.

To address the apparent independence of α on the form of near tip elastic nonlinearity and its physical implications, we consider yet another energy functional. In selecting the latter, we aim at addressing also a different question: Is the wavelength significantly affected by strong elastic nonlinearity deep inside the near tip nonlinear elastic zone or mainly by weak elastic nonlinearity, as predicted by the weakly nonlinear theory of fracture [4, 15, 17]? To address these questions, we consider the incompressible NH functional truncated to leading order nonlinearity

$$\begin{aligned} e_{\text{strain}}^{\text{TNH}}(\boldsymbol{H})/\mu &\simeq \text{tr}(\boldsymbol{\varepsilon}^2) + \text{tr}(\boldsymbol{\varepsilon})^2 - \frac{1}{2}\text{tr}(\boldsymbol{H})^3 - \frac{3}{2}\text{tr}(\boldsymbol{H}) \text{tr}(\boldsymbol{H}^2) \\ &- \frac{1}{8}\text{tr}(\boldsymbol{H})^4 + \frac{9}{4}\text{tr}(\boldsymbol{H})^2 \text{tr}(\boldsymbol{H}^2) + \frac{3}{8}\text{tr}(\boldsymbol{H}^2)^2 + \mathcal{O}(\boldsymbol{H}^5) . \end{aligned}$$

Unlike the weakly nonlinear theory of fracture, which is an analytic perturbative theory that takes into account only cubic nonlinearity in the energy, here we are looking for global numerical solutions and hence should include also quartic nonlinearity to ensure the well-posedness of the global fracture problem [20].

Phase-field theory calculations with $e_{\rm strain}^{\rm TNH}$ of Eq. (2) demonstrated the existence of an oscillatory instability (not shown), whose wavelength is essentially indistinguishable from that of $e_{\rm strain}^{\rm NH}$, as shown in Fig. 2a (diamonds). This result indicates that weak elastic nonlinearity controls the oscillatory instability and further highlights the independence of α on the form of nonlinearity. The latter raises an intriguing possibility; if elastic nonlinearity vanishes, $\ell \propto \Gamma_0/\mu \rightarrow 0$, the results of Fig. 2a imply that $\lambda \approx 13\xi$. That is, the oscillatory instability may exist in the absence of elastic nonlinearity, where its wavelength is determined by the intrinsic dissipation length ξ .

This possibility is quite intriguing because, if true, it means that near tip elastic nonlinearity is not necessary for the existence of the oscillatory instability, which can alternatively inherit its characteristic length from the dissipation zone. The extensive calculations that gave rise to the wavelength λ in Fig. 2a, where the ratio Γ_0/μ has been reduced as much as possible within numerical limitations, also showed that the *amplitude* of the oscillations diminishes as $\ell \propto \Gamma_0 / \mu$ is reduced. This observation might support the possibility that the instability exists with a finite wavelength and a vanishingly small amplitude as elastic nonlinearity vanishes. Hence, the observation in [14] in which no oscillatory instability is observed when $\ell = 0$, i.e. using the linear elastic (quadratic) approximation of e_{strain} to begin with, may simply be explained in terms of a vanishing amplitude, not as indicating the absence of instability in this limit. On the other hand, based on presently available evidence, we cannot exclude the possibility that the instability disappears at a finite (yet very small) value of $\ell \propto \Gamma_0/\mu$, as further discussed below.

While α appears to be independent of the form of near tip elastic nonlinearity, the slope β in the linear $\lambda - \Gamma_0 / \mu$ relation does depend on it. To understand this dependence, recall that the nonlinear length ℓ is proportional to Γ_0/μ , but is not identical to it (e.g. Γ_0/μ exists also in the absence of elastic nonlinearity, while ℓ does not) [4]. Consequently, material dependence (in addition to v-dependence) is expected to be encapsulated in the proportionality factor. To test this possibility, we should directly calculate ℓ , instead of using its dimensional estimate. To calculate ℓ in our large-scale simulations, we need to estimate the actual length at which near tip nonlinearity becomes significant. Any energy functional $e_{\scriptscriptstyle\rm strain}$ can be uniquely decomposed into its linear $e_{\text{strain}}^{\text{le}}$ and nonlinear $e_{\text{strain}}^{\text{nl}} \equiv e_{\text{strain}} - e_{\text{strain}}^{\text{le}}$ parts. The region near the tip at which $\|\partial_{\boldsymbol{H}} e_{\text{strain}}^{\text{nl}}\| / \|\partial_{\boldsymbol{H}} e_{\text{strain}}^{\text{le}}\|$ becomes non-negligible can be used to define $\ell (\|\cdot\|)$ is the magnitude of a tensor, i.e. the square root of the sum of the squares of its elements). In particular, we define $\ell \equiv \sqrt{\mathcal{A}}$, where \mathcal{A} is the area of the region in which $\|\partial_{\mathcal{H}} e_{\text{strain}}^{\text{nl}}\| / \|\partial_{\mathcal{H}} e_{\text{strain}}^{\text{le}}\| \ge 0.5$ (see Fig. S1 in [20]), consistently with earlier definitions [4]. While the existence of a threshold (here 0.5) involves some degree of arbitrariness in the definition of ℓ , the results themselves do not strongly depend on the exact threshold (see Fig. S2 in [20]).

In Fig. 2b we plot ℓ (as just defined) vs. Γ_0/μ for both NH and SVK brittle materials. For both types of materials we observe $\ell \propto \Gamma_0/\mu$, as predicted theoretically. Moreover, the pre-factor in this relation is significantly larger for SVK materials compared to NH materials, which is consistent with the already discussed stronger nonlinearity of the former. In fact, the variability in the pre-factor appears to be similar in magnitude to the variability in the slope of the linear $\lambda - \Gamma_0/\mu$ relation shown in Fig. 2a. To test whether the material dependence of the pre-factor indeed accounts for the material dependence of the wavelength shown in Fig. 2a, we plot λ vs. ℓ in Fig. 2c. We observe that the two curves approximately collapse one on top of the other, suggesting that in fact the oscillations wavelength follows a universal master curve $\lambda = \alpha \xi + \beta \ell$, where α and $\beta = 0.3 \pm 0.07$ are nearly material independent. These results yet again strongly support the universal character of the 2D oscillatory instability.



FIG. 3. (a) Oscillations followed by tip-splitting in a phasefield simulation of NH materials under a large driving force (see Supplemental Movie S1). (b) The corresponding experimental observation (courtesy of Jay Fineberg, experimental details can be found in [10]).

When the driving force for fracture W, i.e. the stored elastic energy per unit area ahead of the crack, is sufficiently large to allow cracks to accelerate to the critical velocity v_c , the oscillatory instability emerges. Are there additional, previously undiscovered instabilities in 2D dynamic fracture triggered when cracks are driven even more strongly? When W is further increased, there exists a range of driving forces for which steady-state oscillatory cracks exist. As W is increased even more, a tip-splitting instability emerges. It can emerge either from oscillatory crack states (resulting in asymmetric tipsplitting, as shown in Fig. 3 and in Supplemental Movie S1) or directly from straight crack states (resulting in symmetric tip-splitting, as shown in Supplemental Movie S2). This ultra-high-velocity tip-splitting instability in 2D dynamic fracture appears to be different from tipsplitting in 2D simulations [27, 28, 33–42] and from the micro-branching instability in 3D experiments [5]. In

Fig. 3a we present tip-splitting that emerges after oscillations (see Supplemental Movie S1). Remarkably, such oscillations followed by tip-splitting have been recently observed under strong driving force conditions in previously unpublished experiments on brittle NH materials, see Fig. 3b.



FIG. 4. Stability phase-diagram of 2D dynamic fracture in the $W/\Gamma_0 - \Gamma_0/\mu\xi$ plane for SVK (a) and NH materials (b). Shown are straight cracks (diamonds), oscillatory cracks (circles), and oscillatory or straight cracks undergoing tipsplitting (squares). See Supplemental Movies corresponding to the thick-lined squares in panel b. The upper thick-lined square also corresponds to Fig. 3a. The thick-lined circles in panels a and b correspond to Figs. 1b and 1a, respectively.

We are now in a position to construct a comprehensive stability phase-diagram of 2D dynamic fracture. The analysis presented above indicates that the relevant dimensionless parameters for such a stability phasediagram are the ratio between the intrinsic nonlinear scale $\ell \propto \Gamma_0/\mu$ and the intrinsic dissipation scale ξ , and the ratio between the driving force for fracture W and the fracture energy scale Γ_0 . The stability phase-diagram in the $W/\Gamma_0 - \Gamma_0/\mu\xi$ plane is shown in Fig. 4 for both brittle SVK (panel a) and NH (panel b) materials. For both classes of materials, for a fixed and finite $\Gamma_0/\mu\xi$, the phase-diagram exhibits the sequence of transitions with increasing W/Γ_0 described in the previous paragraph; for $W/\Gamma_0 < 1$ no crack propagation is possible (not shown), steady-state straight cracks exist upon increasing W/Γ_0 beyond unity over some range of W/Γ_0 (diamonds), then steady-state oscillatory cracks exist over some range for yet larger values of W/Γ_0 (circles), then tip-splitting emerges (squares), either after oscillations (asymmetric tip-splitting, see Supplemental Movie S1) or before (symmetric tip-splitting, see Supplemental Movie S2).

Interestingly, the W/Γ_0 range over which oscillatory cracks exist decreases with decreasing $\Gamma_0/\mu\xi$. In the limit $\Gamma_0/\mu\xi \to 0$, it appears to vanish altogether such that straight cracks make a direct transition to tip-split cracks. While present numerical limitations do not allow us to conclude with certainty if the oscillatory instability exists or not in the absence of near tip elastic nonlinearity, they at least show that, if present, this instability would only exist over a vanishingly small range of loading, with a vanishingly small oscillations amplitude. Our results further strongly indicate that minute near tip nonlinearity, which is likely to exist in most materials, is sufficient to dramatically affect the instability whose wavelength essentially determined by the dissipation length ξ . Finally, and most remarkably, the salient properties and topology of the stability phase-diagram appear to be universal, i.e. they are the same for two widely different forms of near tip nonlinearity.

In summary, we highlighted in this Letter the universal nature of the 2D oscillatory instability whose wavelength follows a universal master curve in terms of dissipation and nonlinear elastic intrinsic lengths, demonstrated the existence of a high-velocity tip-splitting instability and constructed a universal stability phase-diagram of 2D dynamic fracture. Future research should address the existence of the oscillatory instability in the absence of near tip elastic nonlinearity and the origin of the high-velocity tip-splitting instability.

Acknowledgments.— This research was supported in part by the US-Israel Binational Science Foundation (BSF) grant no. 2012061, which provided partial support for C.-H.C. E.B. acknowledges support from the William Z. and Eda Bess Novick Young Scientist Fund and the Harold Perlman Family. A.K. acknowledges support of grant number DE-FG02-07ER46400 from the US Department of Energy, Office of Basic Energy Sciences. We are grateful to J. Fineberg for providing the experimental result shown in Fig. 3b.

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