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Modal spectra extracted from non-equilibrium fluid patterns in laboratory experiments on Rayleigh-Bénard convection

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We describe a method to extract from experimental data the important dynamical modes in spatio-temporal patterns in a system driven out of thermodynamic equilibrium. Using a novel optical technique for controlling fluid flow, we create an experimental ensemble of Rayleigh-Bénard convection patterns with nearby initial conditions close to the onset of secondary instability. An analysis of the ensemble evolution reveals the spatial structure of the dominant modes of the system as well as the corresponding growth rates. The extracted modes are related to localized versions of instabilities found in the ideal unbounded system. The approach may prove useful in describing instability in experimental systems as a step toward prediction and control.

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Identification of instabilities plays a crucial role in our understanding and description of the the dynamics of many nonlinear physical, biological, and chemical systems driven out of equilibrium [1]. In particular, quantitative description is essential for predicting and/or controlling the evolution of such systems, with weather prediction being a prime example. While linear stability analysis of global disturbances in an idealized, infinite system may provide a description of dynamics and pattern selection, this approach fails for imperfect patterns (e.g., far from onset) and in strongly confined systems. Despite recent numerical advances [2–4] in computing the spatial structure and dynamics of localized disturbances in weakly chaotic patterns, no general approach has been developed for extracting such dynamical information directly from experimental measurements.

In this Letter, we present such an approach, illustrating how dynamical degrees of freedom can be extracted from experiments conducted on the prototypical Rayleigh-Bénard convection (RBC) system. Specifically, we determine the spatial structure and evolution of the dominant dynamical degrees of freedom by analyzing the response of the system to an ensemble of localized perturbations about the stationary straight roll state. In each case, we find the dynamics are dominated by a small number of spatially-localized modes. We also observe slowing down of the dynamics and thus quantify the distance to a particular instability boundary in terms of perturbation lifetimes. The spatial structure of the extracted modes is found to be consistent with the classification of secondary instabilities of spatially infinite perfect patterns. We expect the applicability of the outlined approach to extend to time dependent and/or spatially irregular patterns.

The convection experiments were performed with a layer of sulfur hexafluoride (SF_6) gas of depth $d = 700 \pm 10 \mu\text{m}$ compressed to 14.5 ± 0.1 bar [5]. The gas layer was confined laterally to a 25 mm x 15 mm rectangular region by filter paper sidewalls chosen to match

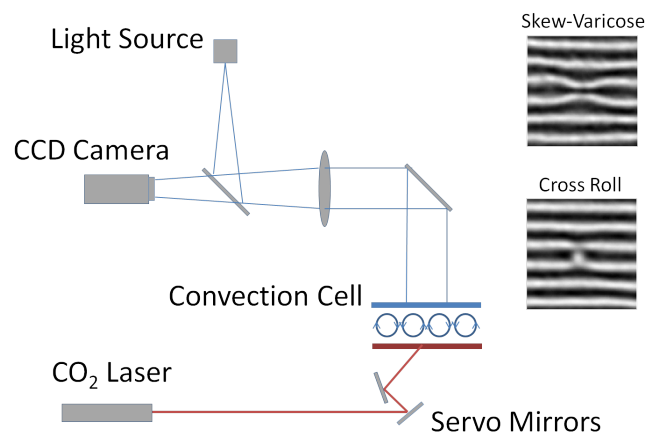


FIG. 1: Experimental setup includes a shadowgraph visualization as well as a system for optical actuation. Inset are observed responses to local perturbations at different parameter values. These disturbances represent the local version of the skew-varicose and cross-roll instabilities, respectively, of the unbounded system.

the fluid conductivity. The layer was bounded from above by a water-cooled sapphire window and from below by a carbon disulfide (CS_2)-cooled zinc selenide (ZnSe) window; the temperatures of these windows were regulated to ± 0.05 °C. Experiments were performed with $\bar{T} = 24.00$ °C and temperature differences of 2.92 and 4.80 °C. Convection was visualized using the shadowgraph method by illuminating from above and imaging the light reflected from the ZnSe surface at the bottom of the gas layer.

SF_6 is a greenhouse gas (it absorbs infrared light strongly); we use this property to optically apply controlled thermal disturbances both to manipulate the global convective flow as well as impose localized perturbations. An infrared (IR) beam from a CO_2 laser ($10.6 \mu\text{m}$ wavelength) is focused to approximately 200 μm in diameter and strikes the gas layer from below (af-

ter passing through the IR-transparent CS₂ coolant and ZnSe window). The beam is steered by two computer-controlled, gold-plated servo mirrors that rotate about orthogonal axes, providing the ability to direct the IR light toward any point over the cell domain. Fig. 1 shows the experimental setup. The extinction length of the beam in the SF₆ is $< 10 \mu\text{m}$ [6], less than 2% of the cell depth, so the absorbed beam induces a highly localized heating that takes place very near the bottom of the gas layer. Software developed in-house works with a commercial program (LD2000) to synchronize laser power with mirror rotations. The strong absorption and rapid scanning allow for flow manipulation on a time scale much faster than the typical dynamical time scale (vertical thermal diffusion time of 2.7 s). This technique improves on previous attempts to manipulate convection patterns optically [7, 8] by introducing dynamic pattern control while minimizing unwanted disturbances such as thermal inertia effects from perturbative boundary heating.

A pattern of straight rolls with wavenumber q was imposed by sending one line of laser light into the cell at the desired location of hot upflow for each roll, at 1 s intervals. After drawing a full set, the process was repeated until the straight roll pattern was established in about 30 s. To minimize sidewall effects, the pattern was imposed in the central portion of the cell, 2 wavelengths from either of the sidewalls in the wavevector direction. This provides room for 7-9 interior roll pairs.

Secondary instabilities of the straight roll state are predicted to define the boundaries of a stability (Busse) balloon in (ϵ, q) space at fixed Prandtl number; crossing one of these instability thresholds results in a re-organization of the pattern [9]. Here, $\epsilon = (R - R_c)/R_c$ is the reduced bifurcation parameter that measures the distance from onset of the primary instability of the purely conducting state. Fig. 2 shows the Busse balloon for the spatially unbounded system at the conditions of our experiments ($Pr = 0.84$). The Busse balloon is conventionally calculated assuming an infinite system; we may expect the thresholds for the localized instabilities in a bounded system to take place at slightly different parameter values. Nonetheless, the balloon provides a useful reference as different areas in the parameter space are visited, and the dynamics of the dominant modes of the system can be expected to depend on the distances between a given (ϵ, q) point and the various instability boundaries.

Pattern manipulation allows us to use both ϵ and q as control parameters. The initial pattern wavenumber was chosen to be within the stable band. Following the initial imprinting, actuation is restricted to only the two outer-most rolls between which the straight roll pattern is confined. The pattern wavenumber is adjusted by moving the positions of these outer rolls toward or away from one another; the interior pattern equilibrates on a timescale of approximately $50 t_v$ for our domain size. A closed-loop feedback algorithm constantly analyzes images for

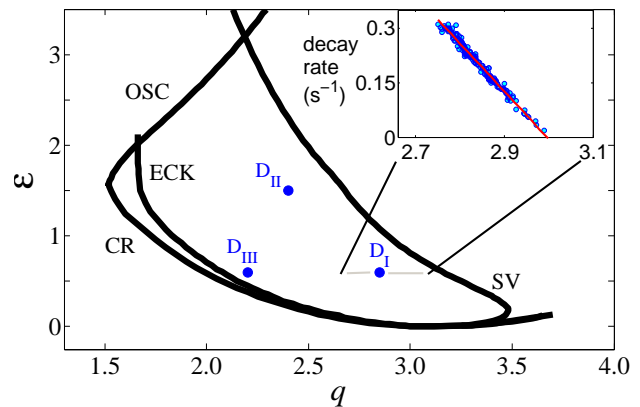


FIG. 2: Stability balloon at $Pr = 0.84$ showing various instabilities (CR = Cross Roll, ECK = Eckhaus, SV = Skew Varicose, OSC = Oscillatory) of the straight roll state along with the parameters at which the experimental data were taken for the three data sets. $D_I = (0.60, 2.85)$, $D_{II} = (1.50, 2.40)$, and $D_{III} = (0.60, 2.20)$. The inset plot shows the disturbance decay rate (s^{-1}) as a function of wavenumber q at fixed $\epsilon = 0.60$.

deviations of the two boundary roll positions from desired locations and adjusts laser power accordingly.

Sufficiently close to a particular instability boundary, the spatial modes of that instability are weakly damped and can therefore be excited by small perturbations to the base state (straight rolls). Each perturbation takes the form of a brief (about 100 ms) well-localized laser pulse directed to a single location in the convection pattern. We estimate that the applied heating results in an initially axisymmetric disturbance of diameter $\sim d/2$.

We first probed the pattern response to perturbations for different q near the high-wavenumber instability boundary, with fixed $\epsilon = 0.60$. Upon perturbation, two adjacent upflow regions appear to bend toward one another and then relax back to their initial locations; a snapshot of a typical response is shown in the inset of Fig. 1. The disturbance decay is slower at higher q , which suggests using the perturbation lifetime as a measure of distance from instability. The perturbation lifetime is measured most easily from the apparent local roll separation as a function of time. This signal typically displays a large spike immediately after the perturbation, followed by exponential decay to the original value; analysis is restricted to this period of linear decay.

We find that the disturbance decay rate decreases linearly over an order of magnitude with increasing q (see the inset in Fig. 2). The decay-rate distribution shows the expected slowing down of the dynamics near the instability and indicates the critical value $q_c = 3.00$ for the localized skew-varicose instability. Note that this value is slightly smaller than that of the global instability predicted from analysis of an infinite domain ($q_c = 3.15$), reflecting the effect of spatial localization. The low amount

of scatter in the decay-rate plot illustrates the high degree of reproducibility of the imposed perturbations.

In order to excite all dominant localized modes, perturbations were applied at a grid of equally-spaced locations across a wavelength of the pattern. All other perturbations are related to this set through the symmetries of the system (translational invariance in the direction perpendicular to the wavevector, periodicity in the direction of the wavevector), as long as the disturbances are sufficiently well-localized and not near the physical boundaries. Each set contains perturbations at 12 distinct locations; in all experiments, the spatial extent of the laser is of order 10% of the pattern wavelength, so there is no benefit from a finer partition.

Shadowgraph images capture the evolution of an imposed disturbance and thus contain snapshots of the composite structure of the excited modes over time. During the perturbation decay, there exists a period of time over which the dynamics of the disturbance can be described by a linear evolution operator; we seek to represent this evolution operator by computing its matrix elements in a subspace spanned by a set of slow modes extracted from the shadowgraph images. We first subtract the stationary straight roll pattern from all images after the perturbation. The images are then spatially windowed and Fourier filtered. A Karhunen-Loève (KL) decomposition of difference images representing perturbations 2-5 s after each initial disturbance provides a set of basis modes. All perturbations are then projected onto the subspace spanned by this basis. Note that the typical implementation of the KL decomposition uses time-averaging [10], whereas we employ an ensemble average over different initial conditions. We limit our embedding dimension to a small (usually three or four) number of modes that capture 90% of the power of the KL eigenvalue spectrum.

Let us denote the disturbance following an initial perturbation \mathbf{b}^0 , expressed in a low-dimensional basis. After some time T , this state has evolved to \mathbf{b}^T . Then $U\mathbf{b}^0 = \mathbf{b}^T$, where U is the evolution operator. Using an ensemble of initial conditions we define

$$B^0 = [\mathbf{b}_1^0 \mid \mathbf{b}_2^0 \mid \cdots \mid \mathbf{b}_M^0]$$

and similarly,

$$B^T = [\mathbf{b}_1^T \mid \mathbf{b}_2^T \mid \cdots \mid \mathbf{b}_M^T]$$

This gives the over-determined (least-squares) problem for the evolution operator $UB^0 = B^T$, which is solved by $U = B^T(B^0)^{-1}$, where the reciprocal of B^0 is taken to refer to the generalized inverse of the non-square matrix.

During linear decay, each eigenmode decays at a characteristic rate, so we can also write $U\mathbf{e}_i = \exp(\sigma_i T)\mathbf{e}_i$, where \mathbf{e}_i are the eigenvectors and the eigenvalues λ_i are related to the growth rates by $\lambda_i = \exp(\sigma_i T)$.

The discrete translational symmetry of the straight roll pattern implies that a superposition of a well-localized

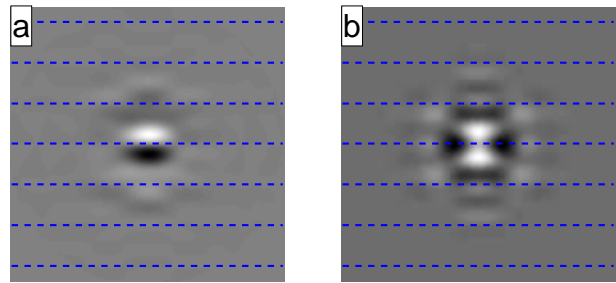


FIG. 3: (a) The fundamental dominant and (b) sub-dominant mode extracted at D_I . Dashed lines mark the approximate locations of the hot fluid of the underlying base state; cold fluid lies between the dashed lines.

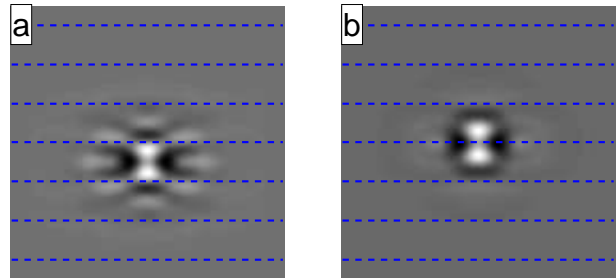


FIG. 4: (a) The fundamental dominant and (b) sub-dominant mode extracted at D_{III} .

eigenmode with a copy of itself translated over an integer number of wavelengths is an eigenmode with the same growth rate. Hence, there exist many possible representations of each eigenmode. Reduction of the dynamics using the symmetries of the base pattern is useful for both unbounded and bounded systems.

In particular, all disturbances can be decomposed in terms of symmetries related to a roll pair. By defining two symmetry planes, one coinciding with the center of upflowing hot fluid, the other at the center of adjacent cold fluid, we can define four symmetric versions of every initial disturbance, each even/odd about the two symmetry planes. Each of the corresponding four subspaces is invariant: evolving disturbances retain their symmetry.

The entire collection of initial and final conditions extracted from experiment was decomposed using these symmetries, producing four independent ensembles. All eigenmodes extracted from the four ensembles are eigenmodes of the system, but in the cases when multiple eigenmodes share an eigenvalue (growth rate) we eliminate redundant representations by computing the most spatially-localized eigenmode structure.

We estimate the uncertainty in the growth rates to be less than 10%. This allows one to group all extracted modes and define the fundamental mode as the most-localized structure with a particular growth rate. The fundamental modes were computed by minimizing the p -norm ($p < 2$) among linear combinations of all modes

(and their translated copies) in each group. Here the p -norm of a vector \mathbf{v} , with i -th component v_i , is defined as $(\sum_i v_i^p)^{1/p}$. The symmetries imply that all extracted modes in each group can be represented as linear superpositions of the fundamental mode along with its translated and/or reflected copies. We verified that this is indeed the case as such representation was accurate, with mutual projection > 0.94 .

The first ensemble was produced at the point D_I of the parameter space (see Fig. 2). The two dominant modes are shown in Fig. 3. As the lifetime measurements indicate, the least-stable mode ($\sigma_1 = -0.13 \text{ s}^{-1}$) tended to be excited from perturbations to cold fluid. Note, however, that while the structures excited from these disturbances are even about the downflow symmetry plane, the most-localized representation of this mode does not obey that symmetry. The sub-dominant mode ($\sigma_2 = -0.70 \text{ s}^{-1}$) tended to be excited from perturbations to hot fluid.

A second set of perturbations at high q was performed at D_{II} , with ϵ increased relative to D_I . Again, two modes are extracted; $\sigma_1 = -0.15 \text{ s}^{-1}$ and $\sigma_2 = -0.55 \text{ s}^{-1}$. Mutual projections of the modes extracted at D_I and D_{II} indicate that the spatial structure of the two dominant modes remains unchanged (after scaling by the wavelength) between these two locations. There is also, in both cases, a large separation between the two growth rates. This suggests we can identify the dominant mode (Fig. 3a) as the one representing the secondary instability at the high wavenumber boundary. Its structure is consistent with a skew-varicose type instability.

We also created an ensemble of perturbations to pattern with low q , at D_{III} . Again, two modes were extracted, with growth rates $\sigma_1 = -0.20 \text{ s}^{-1}$ and $\sigma_2 = -0.27 \text{ s}^{-1}$. Shown in Fig. 4, the spatial structure of the dominant mode does not resemble any of the previously extracted modes, while the sub-dominant mode resembles the sub-dominant mode extracted at both D_I and D_{II} . The closeness of the growth rates is consistent with the existence of two low- q instability types of the unbounded system that occur at very nearly the same parameter values, namely, the Eckhaus and cross-roll instabilities (see the Busse balloon in Fig. 2). The dominant mode is again excited from perturbations to cold fluid; this is not surprising, as heating of cold fluid tends to reduce the amplitude of the saturated state. We find experimentally that sufficiently strong perturbations of this kind result in the growth of rolls perpendicular to the base pattern. We therefore identify the dominant low-wavenumber mode with the localized cross-roll instability and the sub-dominant mode with the localized Eckhaus instability.

Further experiments are needed to explore the applicability of this approach to states exhibiting more complex dynamics. One such state, occurring in gas convection experiments with $Pr \approx 1$, is the spatiotemporally chaotic state known as Spiral Defect Chaos (SDC) [11]. While

there exists a bistability between stationary straight rolls and SDC [12] over the parameter range of the experiments reported here, localized instability in the straight roll pattern introduces defects which tend to lead to a disordered pattern, thus providing a mechanism for the transition to chaotic behavior. Additionally, it was determined in a numerical study [2] that the chaotic dynamics of SDC are largely driven by the creation/annihilation of defects occurring in straight roll regions of the pattern. We expect, therefore, that spatially-localized modes are dynamically important in both the transition to and the driving of chaotic behavior, suggesting a natural extension of our experimental approach to investigations of more complex convection patterns. Moreover, the outlined procedure is general enough to be used in a variety of other dynamical systems, so long as an appropriate means of system actuation can be developed. In addition to being of fundamental interest and of use in increasing predictive power, knowledge of the modes of instability could be particularly advantageous in system control, where small, controlled perturbations could be used to guide system dynamics [13].

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