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Experimental Verification of Mechanism for Microarray Formations in Nanofilms Subject to Large Thermal Gradients

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The free surface of molten nanofilms is known to undergo spontaneous formation of periodic protrusions when exposed to a large transverse thermal gradient. Early time measurements of the array pitch and growth rate in polymer melts confirm a formation process based on a long wavelength thermocapillary instability and not electrostatic attraction or acoustic phonon driven growth as previously believed. We find excellent agreement with theoretical predictions provided the nanofilm out-of-plane thermal conductivity is several times larger than bulk, an enhancement suggestive of polymer chain alignment.

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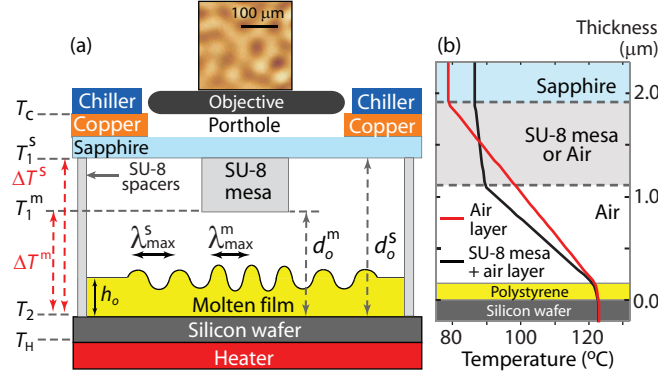


FIG. 1. (color online) (a) Experimental setup (not to scale) showing actual image of molten film deformation at early times. Fastest growing wavelength beneath sapphire (s) and mesa (m) regions are denoted by λ_{\max}^s and λ_{\max}^m . (b) Sample temperature profiles from steady-state finite element simulations (FEM) [9] with axial symmetry, constant temperatures T_H and T_C , and insulating conditions along exterior boundaries. For $T_H = 130^\circ\text{C}$, $T_C = 25^\circ\text{C}$, mesa diameter = $400\text{ }\mu\text{m}$, $h_o = 160\text{ nm}$, $d_o^m = 1100\text{ nm}$ and $d_o^s = 1900\text{ nm}$, results yield $T_2 = 123^\circ\text{C}$, $\Delta T^m = 33.2^\circ\text{C}$ and $\Delta T^s = 44.8^\circ\text{C}$. Black curve (mesa central axis): $T(r = 0, z)$; red curve: $T(r = 700\text{ }\mu\text{m}, z)$. Thermal conductivity constants used in FEM simulations [W/m-K]: silicon = 93 at 130°C [10], copper = 390 at 40°C [11], sapphire = 40 at 60°C [12], SU 8 = 0.3 (MicroChem), air = 0.033 at 110°C [11], and polystyrene (PS) = 0.13 at 130°C [13].

For the past decade, researchers have been exploring the effects of large thermal gradients on molten nanofilms in the hope of harnessing instabilities for generating microarrays [1–4]. When the free surface of a molten nanofilm is exposed to large thermal gradients, periodic protrusions form and grow toward the cooler target until contact is achieved. There is significant interest in this phenomenon since external field gradients can generate three dimensional nanostructures directly from the melt, which exhibit ultra smooth surfaces befitting the most demanding optical applications. Controlled growth of desired shapes, however, requires identification of the dominant growth mechanism, the material and geometric properties affecting structure formation, and the principles which establishes the minimum feature size.

Three different mechanisms have been proposed as the source of instability: electrostatic attraction from surface induced charge between the film and overlying substrate (SC model [2, 5]), internal film pressure caused by interfacial reflections of low frequency acoustic phonons (AP model [3, 6]), and thermocapillary flow from temperature variations along the interface which draw fluid toward cooler regions (TC model [7, 8]). The first two mechanisms rely on properties specific to polymeric films. The thermocapillary mechanism is applicable to any fluid nanofilm - it represents an extreme limit of (Bénard) Marangoni instability for long wavelength fluctuations in which gravitational effects are absent and thermocapillary forces overcome stabilization by capillary forces. Previous investigations have confronted limitations imposed by the typical experimental setup shown in Fig. 1(a), namely no direct measure of the thermal gradient within the narrow gap, lack of parallelism between opposing substrates, and lack of visualization during structure formation and growth. In fact, all measurements to date have relied on solidified formations resulting from prolonged contact with the cooler target.

We find that physical contact with the overlying substrate results in smaller wavelengths from fluid reorganization. While this ultimately reduces the array pitch, it compromises direct comparison to models based on linear stability analysis, which also require amplitude fluctuations small in comparison to the initial film thickness. In this Letter, we report *in situ* optical microscopy measurements of the lateral spacing and growth time for evolving protrusions in polymer nanofilms. Excellent quantitative agreement with the thermocapillary model is obtained so long as the out-of-plane film thermal conductivity is several times larger than reported bulk values, an enhancement suggestive of polymer chain alignment.

Fig. 1(a) depicts a sketch of the experimental apparatus used in our experiments. The bottom substrate consisted of a polished silicon (Si) wafer (Ultrasil, $\langle 100 \rangle$, 150 mm diameter, 650-700 μm thickness, 50-60 Ohm-cm) cleaned with piranha solution and rinsed in 18 M Ω water (Millipore Milli-Q). A solution of polystyrene (PS) [4 wt% of $M_w = 2.46\text{ kg/mol}$, $T_g = 60^\circ\text{C}$ [14] or $M_w = 1.3\text{ kg/mol}$, $T_g = 23^\circ\text{C}$ [14], Scientific Polymer Products) in toluene was extracted

TABLE I. Literature values for material constants of molten polystyrene ($M_w = 2.46$ and 1.3 kg/mol) at $T = 130^\circ\text{C}$ unless otherwise noted. Symbol (E) denotes extrapolated value.

γ	Surface tension [13] (E)	31 mN/m (2.46 kg/mol) 33 mN/m (1.3 kg/mol)
γ_T	$ \partial\gamma/\partial T $ [13] (E)	0.076 mN/m-K (2.46 kg/mol) 0.078 mN/m-K (1.3 kg/mol)
η	Shear viscosity [14] (E)	85 Pa-s (2.46 kg/mol, 125°C) 7.8 Pa-s (1.3 kg/mol, 107°C)
ε_p	Dielectric constant [13] (M_w and T unknown)	2.5
u_p	Speed of sound [15] (M_w and T unknown)	1300 m/s
k_p	Thermal conductivity [13] (E) (M_w and T unknown)	0.13 W/m-K

through a $0.2\ \mu\text{m}$ PTFE filter and spun coat onto the wafer. Films were vacuum baked at 80°C for two hours to remove residual toluene; the resulting thickness h_o of the wetting film was measured by ellipsometry (Gaertner L166C). The top substrate consisted of a cylindrical sapphire window (Edmund Optics, single crystal, diameter $7.5\ \text{mm}$, thickness $400 \pm 50\ \mu\text{m}$) patterned with four photoresist spacers (MicroChem, SU-8 2000) of length $d_o^s = 2.0 \pm 0.1\ \mu\text{m}$ arranged at the vertices of a square measuring either $1\ \text{mm}$ (for $2.46\ \text{kg/mol}$ films) or $3\ \text{mm}$ (for $1.3\ \text{kg/mol}$ films) along the diagonal. Centered between these spacers was a transparent cylindrical SU-8 mesa of diameter $400\ \mu\text{m}$ (for $2.46\ \text{kg/mol}$ films) or $1\ \text{mm}$ (for $1.3\ \text{kg/mol}$ films) and thickness 0.6 to $1.4\ \mu\text{m}$. To prevent polymer adhesion, the sapphire window and protrusions were silanized after a hard-bake of the SU-8 by exposure to a solution of $10\ \text{mL}$ of hexane with 2 drops of FOTS (CAS 78560-45-9) inside an evacuated desiccator. The PS coated wafer was then placed on top of a copper sheet ($1.59\ \text{mm}$ thick) resistively heated from below by a glass slide coated with an indium tin oxide layer. The entire system was clamped between a bottom aluminum plate and a second top copper sheet ($1.59\ \text{mm}$ thick) using three long vertical screws. The copper sheet was perforated with a small hole centered above the SU-8 mesa to view structure formation *in situ*. Perfect parallelism over an extended region was difficult to achieve due to intrinsic limitations on surface flatness (sapphire 2λ @ $632.8\ \text{nm}$) and total thickness variation (Si wafer $< 5\ \mu\text{m}$). To maximize parallelism, the three screws were adjusted to distribute the clamping force while monitoring the resulting interference fringes.

The bottom of the Si wafer was maintained at $T_H = 130^\circ\text{C}$ ($2.46\ \text{kg/mol}$ films) or 114°C ($1.3\ \text{kg/mol}$ films) by a temperature controller (Wavelength Electronics, MPT10000); the exterior face of the top copper sheet was maintained at $23^\circ\text{C} \leq T_C \leq 72^\circ\text{C}$ by a chilled water loop. Both temperatures were monitored by thermocouples (Omega, J type, calibration error $\pm 1^\circ\text{C}$). The extremely small gap size d_o^s prevented direct measurement of the temperature difference $\Delta T^{m,s} = T_2 - T_1^{m,s}$ needed for comparison to theoretical models. Finite element simulations (FEM) [9] based on the dimensions and material properties of the elements shown in Fig.1 were therefore used to compute $\Delta T^{m,s}$. As discussed in Ref. (8), the long wavelength (slender gap) approximation reduces the heat transfer process to a 1D thermal conduction problem along the vertical axis. Shown in Fig. 1(b) are sample temperature profiles beneath the mesa central axis ($r = 0$) and at a radial distance $r = 700\ \mu\text{m}$. These profiles clearly indicate the difference between the value $\Delta T^{m,s}$ and the external value $T_H - T_C$.

In situ measurements of the pattern wavelengths and growth times were obtained by optical microscopy (Zeiss Axiovert 200 MAT) and white light interferometry, respectively. Images were captured from two distinct regions: that beneath the SU-8 mesa characterized by d_o^m , ΔT^m , and λ_{max}^m , and that beneath the sapphire window (and away from the mesa, spacers and top copper sheet) characterized by d_o^s , ΔT^s , and λ_{max}^s . Altogether, these experiments span a wide parameter range, namely $81\ \text{nm} \leq h_o \leq 204\ \text{nm}$, $600\ \text{nm} \leq d_o \leq 2000\ \text{nm}$, $3 \leq d_o/h_o \leq 23.5$ and $13^\circ\text{C}/\mu\text{m} \lesssim \Delta T^{m,s}/d_o^{m,s} \lesssim 43^\circ\text{C}/\mu\text{m}$.

Figs. 2(a)–(b) show representative images of structure formation beneath the cooled mesa at (a) early times and (b) after contact by several nanopillars. Here, the mesa perimeter triggered axisymmetric undulations in film thickness which grew to touch the colder substrate. Approximately 18 protrusions formed along the outer ridge before contact [Fig. 2(a)]; approximately 31 were observed after contact [Fig. 2(b)]. The smaller wavelength after contact resulted from rapid fluid rearrangement against the silanized (mesa) substrate. Figs. 2(c)–(d) show corresponding images in the exterior region away from the mesa at (c) early times and (d) late times. Here, taller protrusions sometimes

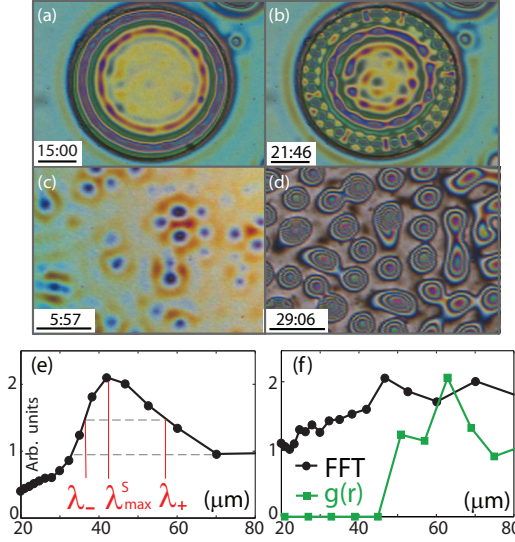


FIG. 2. (color online) Film deformation and growth beneath a 400 μm diameter mesa (a) at early times and (b) after contact for $h_o = 160$ nm, $d_o = 630$ nm and $\Delta T^m = 17^\circ\text{C}$. See Supplementary Material for movie of this process. Corresponding images in exterior region away from mesa at (c) early times and (d) late times for $h_o = 160$ nm, $d_o = 1900$ nm and $\Delta T^s = 45^\circ\text{C}$. Latter images show significant film depletion - pink regions in interstitial areas $\approx \text{O}(10\text{nm})$. (e) Fourier transform of blue channel of image (c) with $\lambda_{\text{max}}^s = 42.2$ μm and bandwidth spread (full width half-maximum) $\lambda_- = 36.8$ μm and $\lambda_+ = 56.1$ μm . (f) Comparison of pair correlation function $g(r)$ with Fourier transform (blue channel) of image (d). Time stamp = hours : minutes; scale bar = 100 μm . Color levels in (a) – (d) adjusted for enhanced contrast.

underwent coalescence, which resulted in larger values of λ_{max}^s , or film depletion, which eventually hindered growth. All data for comparison to linear stability theory was therefore restricted to protrusions which neither touched the cooler substrate nor underwent coalescence or film depletion.

Fourier transforms of images to extract λ_{max} were obtained from the color channel that exhibited highest contrast. The first circular ridge to form beneath the edge of the mesa was also excluded from analysis to minimize edge effects. Measurements of λ_{max} versus radial distance were conducted to rule out finite size effects. Fig. 2(e) is a sample Fourier transform of the blue channel for image (c). For structures containing many interference fringes, the quality of the Fourier transform was diminished, as shown in Fig. 2(f). In such cases, λ_{max} was instead extracted from the peak in the pair correlation function $g(r)$.

The wavelength of the fastest growing mode in the limit $(h_o/\lambda_{\text{max}})^2 \ll 1$ for the three models discussed above [2, 3, 8] is given by:

$$\frac{\lambda_{\text{max}}^{\text{SC}}}{2\pi h_o} = \sqrt{\frac{2\varepsilon_o \varepsilon_p^2 \gamma h_o}{\sigma^2 d_o^2}} \left(\frac{d_o}{h_o} + \frac{1}{\varepsilon_p} - 1 \right)^{3/2}, \quad (1a)$$

$$\frac{\lambda_{\text{max}}^{\text{AP}}}{2\pi h_o} = \sqrt{\frac{\gamma u_p}{Q(1-\kappa)k_{\text{air}}\Delta T}} \left(\frac{d_o}{h_o} + \kappa - 1 \right), \quad (1b)$$

$$\frac{\lambda_{\text{max}}^{\text{TC}}}{2\pi h_o} = \sqrt{\frac{4\gamma h_o}{3\kappa d_o \gamma_T \Delta T}} \left(\frac{d_o}{h_o} + \kappa - 1 \right). \quad (1c)$$

Here, σ denotes the polymer surface charge density, ε_o is the vacuum permittivity, Q is the nanofilm acoustic quality factor [3], and $\kappa = k_{\text{air}}/k_p$, which represents the thermal conductivity ratio of air to polymer film. Remaining variables are defined in Fig. 1 and Table I. The AP and TC models both predict that λ_{max} scales as $(\Delta T)^{-1/2}$; the SC model contains no temperature dependence.

Fig. 3(a) shows the dependence of λ_{max} on ΔT i.e. ΔT^m or ΔT^s as computed from FEM simulations. Least squares fits to the power law $\lambda_{\text{max}} \propto (\Delta T)^\zeta$ resulted in an average value $\zeta = -0.47$, close to the predicted value - 1/2. The measured exponent is consistent with the AP and TC models but not the SC model. Shown in Fig. 3(b) is a least squares fit to the SC model as a function of d_o with $\sigma = 0.24$ mC/m². Not only is the agreement poor but the fit constant σ is one to two orders of magnitude larger than reported in the literature [16]. These results indicate that

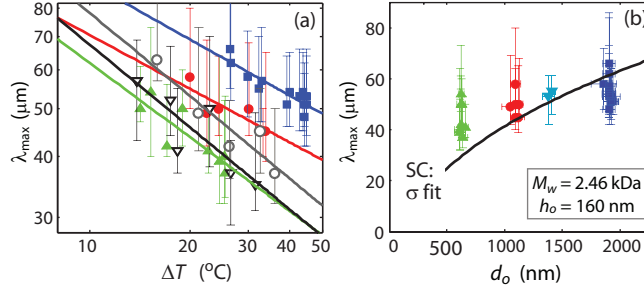


FIG. 3. (color online) (a) Least squares fit (solid lines) to power law $\lambda_{\max} \propto (\Delta T)^\zeta$. Error bars denote bandwidth spread λ_+ to λ_- defined in Fig. 2(e). Fits are based on λ_{\max} values (excluding error bars). Parameter values for lines shown: solid (blue) squares: $M_w = 2.46$ kg/mol, $h_o = 160 \pm 10$ nm, $d_o = 1900 \pm 100$ nm, $\zeta = -0.38 \pm 0.13$; solid (red) circles: $M_w = 2.46$ kg/mol, $h_o = 160 \pm 10$ nm, $d_o = 1100 \pm 50$ nm, $\zeta = -0.36 \pm 0.31$; open (grey) circles: $M_w = 1.3$ kg/mol, $h_o = 186 \pm 5$ nm, $d_o = 873 \pm 45$ nm, $\zeta = -0.56 \pm 0.42$; open (black) triangles: $M_w = 1.3$ kg/mol, $h_o = 186 \pm 5$ nm, $d_o = 655 \pm 45$ nm, $\zeta = -0.56 \pm 0.50$; and solid (green) triangles: $M_w = 2.46$ kg/mol, $h_o = 160 \pm 10$ nm, $d_o = 630 \pm 30$ nm, $\zeta = -0.50 \pm 0.31$. (b) Least squares fit (solid line) to SC model for 2.46k PS [Eq.(1a)] for $\sigma = 0.24$ mC/m².

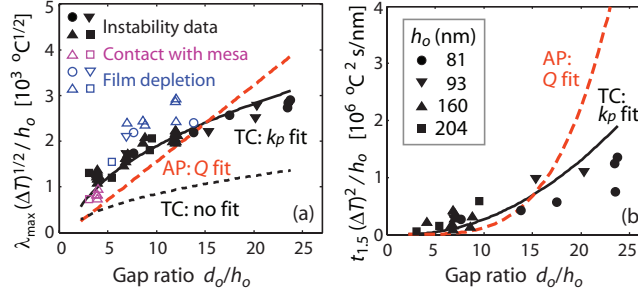


FIG. 4. (color online) (a) Comparison of measured (scaled) wavelength versus gap ratio d_o/h_o for 2.46 kg/mol PS samples. Superimposed curves represent (i) TC model [Eq. (1c)] with no fitting parameter i.e. only the material constants given in Table I; (ii) least squares fit to AP model with fit constant $Q = 2.3$ [Eq. (1b)]; and (iii) least squares fit to TC model with fit constant $k_p = 0.68$ W/m-K. Only data prior to contact with mesa or film depletion is included in fitting procedure. Icons shown in (b) denote initial film thickness. Error bars (not shown for clarity) extend $\pm 500^\circ\text{C}^{1/2}$ along the vertical axis and ± 0.5 along the horizontal axis. See Supplementary Material for results with 1.3 kg/mol PS films. (b) Comparison of data in (a) with predictions of AP and TC models for growth amplitude to achieve a value $h/h_o = 1.5$.

the SC mechanism is likely not the primary cause of instability.

To differentiate between the AP and TC mechanisms, we examined the behavior of λ_{\max} as a function of gap ratio d_o/h_o i.e. d_o^m/h_o or d_o^s/h_o . Superimposed on the data in Fig. 4(a) are the theoretical predictions of Eqs. (1b) and (1c). The (black) dashed line is the TC model with bulk material constants from Table I, which yields an unacceptable fit. The (orange) dashed curve is the AP model with fitting constant $Q = 2.3$ (cf. $Q = 6.2$ for PS between two Si wafers [3]). The linear increase with d_o/h_o is not supported by the data. A two parameter fit to Eq. (1b) yielded better agreement but unphysical constants, namely $Q = -0.56$ (positive value required for low frequency phonon model [3]) and $k = 0.0026$ W/m-K (value must exceed $k_{\text{air}} = 0.033$ W/m-K). The solid (black) curve is the TC model with fitting constant $k_p = 0.68$ W/m-K, which produces excellent agreement. (The value of k_p is not expected to change significantly over the film thickness and temperature ranges used in this study [17].) Similar fits for 1.3 kg/mol PS films can be found in the supplementary section.

This five fold increase in the out-of-plane thermal conductivity is suggestive of polymer chain alignment. Birefringence measurements of spun coat and annealed PS films (150 kg/mol, 2.3 μm) have established out-of-plane alignment on oxide coated wafers [18]. Additional studies have shown that the thermal conductivity of polymer microscale films can increase by a factor 4 – 8 in the direction of alignment [17]. Chain alignment is also observed to increase with decreasing molecular weight and decreasing film thickness [19]. Simultaneous adjustment of other material constants

in Eq. (1c) was also tested, but only an increase in k_p captures the correct dependence of $\lambda_{\max}^{\text{TC}}$ with d_o/h_o .

The time for protrusions to reach a normalized height h/h_o can also be estimated from linear stability theory [8]:

$$t_{h/h_o} = \frac{3\eta h_o}{\gamma} \left(\frac{\lambda_{\max}}{2\pi h_o} \right)^4 \log \left(\frac{h/h_o - 1}{R/h_o} \right). \quad (2)$$

Here, R/h_o denotes the normalized initial film roughness, estimated to be 10^{-2} from atomic force microscopy. The average (scaled) value of $t_{1.5}$ is shown in Fig. 4(b) using the best fit values for λ_{\max} from Fig. 4(a). Variations in film thickness were obtained from interference color mapping. As evident, the TC model for 2.46 kg/mol PS with fitting parameter $k_p = 0.68$ W/m-K yields a closer fit to the experimental data than the AP model.

In summary, these experiments establish that thermocapillary forces along the free surface of the nanofilm generate a long wavelength thermocapillary instability primarily responsible for the formation and growth of nanopillar arrays. Excellent agreement with theory is obtained for a value of the melt out-of-plane thermal conductivity several times larger than bulk. This is suggestive of polymer chain alignment in the vertical direction. Studies of the degree of alignment as a function of chain length are currently underway. We are hopeful that the excellent correspondence between experiment and theory will lead to further reduction in the pitch and higher spatial resolution for fabrication of optical and photonic arrays.

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