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## Prediction and measurement of leaky dielectric drop interactions

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# Prediction and measurement of leaky dielectric drop interactions

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Application of an electric field across the curved interface of two fluids of low but non-zero conductivities, or ‘leaky dielectrics,’ can give rise to electric stresses that drive sustained fluid flow. In a uniform DC electric field of sufficiently weak magnitude, the electric and velocity fields around an isolated, neutrally buoyant leaky dielectric drop at zero Reynolds number are fore-aft and azimuthally symmetric about the applied field axis. Consequently, the drop remains stationary. The presence of a second drop breaks these symmetries, resulting in relative motion of the drop pair. Recently, Sorgentone *et al.* derived an analytical expression for the relative velocity of a pair of widely separated drops of identical constitution, asymptotic in the inverse separation distance between the drop centroids [C. Sorgentone, J. I. Kach, A. S. Khair, L. M. Walker, and P. M. Vlahovska, “Numerical and asymptotic analysis of the three-dimensional electrohydrodynamic interactions of drop pairs,” *J. Fluid Mech.*, 914, A24 (2021)]. In the present work, we generalize the theory of Sorgentone *et al.* to interactions of dissimilar drops (of different size or constitution), and the pairwise additive interactions of three or more drops. We perform experiments on silicone oil drops suspended in castor oil and compare to asymptotic predictions of the drop pair trajectories. Experimental trajectories of drops with their line of centers initially at an arbitrary angle to the field direction are shown to be qualitatively predicted by our theory. We show results of experiments of dissimilar drops and of three and four drops, again observing qualitative agreement with our theoretical predictions.

## I. INTRODUCTION

The application of an electric field across the interface between low-conductivity (leaky dielectric) fluids gives rise to stresses that can deform the interface and drive electrohydro-

dynamic (EHD) flows [1, 2]. EHD flows find applications in electrosprays [3, 4], electrocoalescence [5, 6], electrorheology [7, 8], microfluidics [9, 10], the formation of Janus capsules [11], and have shown promise in improving existing methods of inkjet printing [12–14]. Much of the literature on electrohydrodynamics has focused on the deformation and breakup of drops [4, 15–26]. In particular, the dynamics of drops that deform to an oblate shape has garnered recent interest [27–30]. While the dynamics of a single drop is well understood [26], many applications involve multiple drops. In electrocoalescence, for example, it is important to predict the behavior of multiple drops in electric fields weak enough to avoid breakup. To this end, the electrohydrodynamic interactions between drops must be determined.

Due to the non-zero electrical conductivities of leaky dielectrics, a drop interface polarizes in an electric field due to both free-charge accumulation and the permittivity mismatch between drop and suspending phases. The resulting surface charge profile induces an electrical stress both normal and tangential to the local interface, thus shearing the interface and driving flow in and outside of the drop. Here, by a “weak” electric field it is meant that the capillary number,  $Ca = \mu_s U_{EHD} / \gamma = \varepsilon_s E_\infty^2 a / \gamma \ll 1$ , where  $\mu_s$  is the viscosity of the suspending fluid,  $U_{EHD} = \varepsilon_s E_\infty^2 a / \mu_s$  is the velocity scale of the EHD flow,  $E_\infty$  is the strength of the applied field,  $\varepsilon_s$  is the absolute electrical permittivity of the suspending phase,  $a$  is the undeformed drop radius, and  $\gamma$  is the surface tension of the interface. Since  $U_{EHD}$  depends inversely on viscosity  $Ca$  is independent of viscosity, unlike for a drop in an externally imposed flow field where the capillary number is inversely proportional to viscosity. A neutrally buoyant drop at zero Reynolds number remains nearly spherical, deforming to a spheroidal shape to leading order in  $Ca$ . Ignoring surface charge convection, the deformation of a single drop can be described to leading order in  $Ca$  using the material property ratios of viscosity  $M = \mu_d / \mu_s$ , conductivity  $R = \sigma_s / \sigma_d$ , and permittivity  $S = \varepsilon_d / \varepsilon_s$ , where subscripts  $d$  and  $s$  denote the drop and suspending phases, respectively. The deformation parameter, a function of the length of the major and minor axes of the drop ( $L_\parallel$  and  $L_\perp$ , respectively), is given by the following expression derived by Taylor [15]

$$D_T \equiv \frac{L_\parallel - L_\perp}{L_\parallel + L_\perp} = \frac{9 Ca}{16(1 + 2R^2)} \left[ \frac{3(2 + 3M)}{5(1 + M)} R(1 - RS) + R^2(1 - 2S) + 1 \right] + \mathcal{O}(Ca^2). \quad (1)$$

Thus, drops can either deform to a prolate ( $D_T > 0$ ) or an oblate ( $D_T < 0$ ) spheroid,

depending solely on the properties of the fluids. An example of the steady deformation and electric and velocity fields around a single leaky dielectric drop for  $M = 2$ ,  $R = 1/5$ ,  $S = 1/3$  is shown in figure 1.

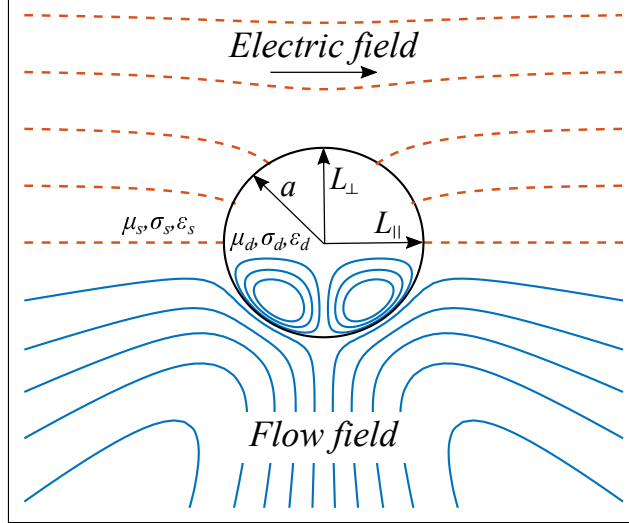


FIG. 1. Example steady electric and velocity fields around a leaky dielectric drop in a uniform electric field, where  $M = 2$ ,  $R = 1/5$ ,  $S = 1/3$ . In this example, the drop is slightly deformed to a prolate spheroid with undeformed radius  $a$ , major axis  $L_{\parallel}$ , and minor axis  $L_{\perp}$  with respect to the applied field direction. The viscosity  $\mu$ , conductivity  $\sigma$ , and permittivity  $\epsilon$  of the drop phase are denoted with subscript  $d$  and the suspending phase properties are denoted with subscript  $s$ . Both the electric and flow fields have fore-aft symmetry about the drop equator perpendicular to the applied field direction and axially symmetric about the poles in parallel to the applied field direction. Internal electric field lines are omitted, however the internal field is uniform and parallel to the applied field direction.

Due to the fore-aft and axial symmetry of the electric and flow fields in and outside a drop, a single, freely suspended drop remains stationary. In the presence of a second drop, however, those symmetries are broken, and the drops translate by action of the flow and non-uniform electric field due to the presence of the other drop. When perfectly dielectric or conducting drops are suspended in a dielectric medium, they interact only through dielectrophoresis (DEP), *i.e.* the force on a body residing in an electric field gradient [31, 32]. The electrostatic interaction of two dielectric spheres arbitrarily placed in an electric field was calculated using a multipole re-expansion by Washizu and Jones [33], who found that the interaction of widely separated spheres matches closely with a point dipole approximation [34]. In both cases, there is a critical angle between the line of centers connecting the drops and the applied field direction,  $\Theta = 54.7^\circ$ , below which the spheres will attract and above which they

will repel. This is the basis for electrocoalescence, where these interactions are exploited to augment the rates of collision and coalescence of water drops in oil [35, 36]. When the drop and suspending fluids are leaky dielectrics, the drops interact through EHD as well. This was first addressed by Sozou [37], who calculated that the flow field around two drops can be modified considerably depending on the drops' separation distance using a multipole expansion in bispherical coordinates; however, this calculation was restricted to the case of two identical, spherical drops with the line connecting their centers aligned in the direction of the applied field. Baygents, Rivette, and Stone [38] then demonstrated that leaky dielectric drops interact through a combination of EHD and DEP. They employed a boundary integral method, which considered the relative motion and deformation of identical drops aligned in the field direction. Their analysis showed that for widely separated drops, the DEP force scales to leading order as  $\mathcal{O}(a^4/d^4)$  while the EHD flow scales to leading order as  $\mathcal{O}(a^2/d^2)$ , where  $a$  is the radius of the drops and  $d$  is the separation distance of their centroids. Recently, Zabarankin [39] derived an analytical expression via a multipole re-expansion for the velocities of nearly spherical but non-identical drops aligned in the direction of the electric field. This theory matched observations by Baygents *et al.* that prolate-deforming drops may attract when drops are close and DEP dominates, yet repel at larger separations where the EHD flow dominates. Furthermore, Zabarankin's work introduced the possibility that oblate-deforming drops with dissimilar permittivities and conductivities in an inviscid suspending fluid could have a repulsive interaction, a behavior not reported in previous studies.

In order to study the EHD interactions of drops in two dimensions, Dong & Sau [40] performed lattice Boltzmann computations, using a point-dipole approximation for the DEP interaction. At a separation of  $d/a = 5$  and  $Ca = 0.18$ , they noted that the critical angle of the EHD flow for circular drops is similar to that of the point-dipole approximation for DEP. Mhatre *et al.* [41] compared boundary integral simulations to experimental drop trajectories for two drops aligned parallel to the field. Although they did not compare their simulations to experiments for drops misaligned with the field, they did experimentally observe the existence of a critical  $\Theta$ , above which drops did not attract each other. More recently, Sorgentone *et al.* [42] considered three dimensional EHD drop interactions via asymptotic theory and boundary integral simulations. Accurate to  $\mathcal{O}(a^5/d^5)$ , their asymptotic theory

showed that leaky dielectric drops initially at an angle to the field may align either parallel or perpendicular to the field direction depending only on the material properties of the drop and suspending phase. An expression, denoted by  $\Phi$ , was derived that quantifies the competition between EHD and DEP. This expression, given again in equation 14, can be used to determine the long-term behavior of the drop pair. Additionally, a derived expression for a critical separation distance further quantified the competition between the DEP and EHD effects driving the interaction.

In the present work, we first extend the theory of Sargentone *et al.* to consider non-identical and multiple, widely separated. We then compare our calculations to experiments of two or more drops, showing in particular that a pairwise additive approximation is capable of qualitatively predicting the trajectories of multiple leaky dielectric drops. In section II, we formulate the problem of interest. In section III, the asymptotic theory for drop interactions is generalized to include dissimilar drops and multiple drops. In section IV, we outline the experimental method and discuss the implications of the parameter  $\Phi$  on practical systems. In section V, we compare the theory to experimental measurements of drop trajectories. We first compare the theory to measurements of drop pair trajectories for identical drops, which qualitatively validate the calculations and illustrate the importance of considering the combined effects of DEP and EHD in drop interactions. We then compare the theory to experimental measurements of the trajectories of drops of different size and discuss the dynamics of electrically dissimilar drops. Finally, we compare the theory to experimental measurements of the interactions of three and four drops. In section VI, we provide the conclusions of our work.

## II. PROBLEM FORMULATION

Consider two spherical, leaky dielectric drops suspended in an unbounded, density matched fluid and subject to a uniform DC electric field  $\mathbf{E}_\infty$  pointing in direction  $\hat{\mathbf{E}}_\infty = \mathbf{E}_\infty/E_\infty$ . We introduce the subscripts  $i$  and  $j$  to identify the drops, where  $i = 1, 2$ ,  $j = 1, 2$ , and  $j \neq i$ . The drop phases (denoted by subscript  $d$ ) and suspending medium (denoted by subscript  $s$ ) have constant and homogeneous properties of conductivity, permittivity, viscosity,, with ratios of material properties  $M_i = \mu_{d,i}/\mu_s$ ,  $R_i = \sigma_{s,i}/\sigma_d$ , and  $S_i = \varepsilon_{d,i}/\varepsilon_s$ ,

respectively. The positions of the drops evolve on the timescale  $\tau_c = a/U_{EHD} = \mu_s/\varepsilon_s E_\infty^2$ . A schematic of the two drop system is shown in Figure 2, where the centers of each drop, relative to an arbitrary origin, are denoted as  $\mathbf{x}_1$  and  $\mathbf{x}_2$ .

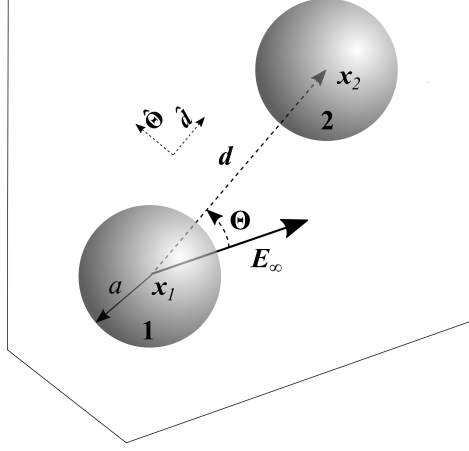


FIG. 2. Depiction of coordinate system for two spherical drops of radius  $a$ . The centers of the drops are separated by a distance  $d$ , with the angle between the line of centers and the applied field denoted as  $\Theta$ .

The vector  $\mathbf{d} = \mathbf{x}_2 - \mathbf{x}_1$  points from the center of drop 1 to the center of drop 2 with associated unit vector  $\hat{\mathbf{d}}$ . A second, right-handed unit vector  $\hat{\Theta}$  is introduced to denote rotations of  $\hat{\mathbf{d}}$ . In effect,  $\hat{\Theta}$  describes rotations of the drop pair, where a positive  $\Theta$  indicates a counter-clockwise rotation of drop 2 about drop 1.

We describe the combined electrostatic and hydrodynamic problems using the approach of Melcher and Taylor [1]. We assume no free charge in the bulk, such that the potential inside and outside the drops satisfies Laplace's equation

$$\nabla^2 \phi_i = 0, \quad \nabla^2 \phi_s = 0. \quad (2)$$

The electric field is expressed as the negative gradient of the potential,  $\mathbf{E} = -\nabla\phi$ . Far from the drops, the electric field approaches the imposed field,  $\mathbf{E}_\infty$ , and the field is bounded at the centroid of each drop. The capillary number is taken to be small,  $Ca \ll 1$ , such that the interface of the drops can be assumed to be spherical. The potential is continuous across the surface of the drops, and the surface charge density is given as

$$\varepsilon_s (\nabla\phi_s \cdot \mathbf{n}_i - S\nabla\phi_i \cdot \mathbf{n}_i) = q \quad \text{at} \quad r_i = |\mathbf{x} - \mathbf{x}_i| = a \quad (3)$$

where  $\mathbf{n}_i$  is the outward pointing unit normal vector of the drops. Neglecting surface charge convection and charge relaxation, current across the interface is conserved, satisfying

$$\nabla\phi_i = R\nabla\phi_s \text{ at } r_i = a. \quad (4)$$

The assumption of no surface charge convection requires the electric Reynolds number,  $Re_E = \varepsilon_s^2 E_\infty^2 / \sigma_s \mu_s \ll 1$ . The charge relaxation timescales in and outside the drop are assumed to be small,  $\varepsilon_{d,s} / \sigma_{d,s} \ll 1$ .

Assuming creeping flow of incompressible fluids, the velocity and pressure inside and outside the drops are governed by the Stokes equations

$$\nabla \cdot \boldsymbol{\sigma}_i = \mu_i \nabla^2 \mathbf{u}_i - \nabla p_i = 0, \quad \nabla \cdot \boldsymbol{\sigma}_s = \mu_s \nabla^2 \mathbf{u}_s - \nabla p_s = 0, \quad (5)$$

where  $\boldsymbol{\sigma} = -p\mathbf{I} + \mu(\nabla\mathbf{u} + (\nabla\mathbf{u})^T)$  is the hydrodynamic stress tensor and  $\mathbf{I}$  is the identity tensor. The flow is quiescent far from the drops and bounded within. The velocity is continuous across the interface, with no penetration of fluid across the boundary. The electric field acting on the developed surface charge induces a tangential Maxwell stress at the surface, which drives the EHD flow. The tangential stress balance is given as

$$[\boldsymbol{\sigma}_s \cdot \mathbf{n}_i - \boldsymbol{\sigma}_i \cdot \mathbf{n}_i] \times \mathbf{n}_i = q \nabla\phi_i \times \mathbf{n}_i, \quad r_i = a, \quad (6)$$

where  $\nabla\phi_i \times \mathbf{n}_i$  is the tangential component of the electric field, which is continuous across the interface. Solution of the above equations and boundary conditions gives the electric and flow fields around each drop individually, which are then used with the method of reflections to determine the interaction of widely separated drops.

### III. ASYMPTOTIC APPROXIMATION OF PAIR INTERACTION

We generalize the methodology of Sorgentone *et al.* [42] to determine the interaction between two widely separated, dissimilar, leaky dielectric drops. Via the method of reflections, a single reflection of the electric and velocity fields around drop  $i$  as seen by drop  $j$  a distance



$d$  away are [43],

$$\mathbf{E}_i = \mathbf{E}_\infty - \frac{1 - R_i}{1 + 2R_i} \mathbf{E}_\infty \cdot (\mathbf{I} - 3\hat{\mathbf{d}}\hat{\mathbf{d}}) \left(\frac{a_i}{d}\right)^3 + \mathcal{O}\left(\left(\frac{a_i}{d}\right)^6\right), \quad (7)$$

$$\begin{aligned} \mathbf{u}_i = & \frac{9}{10} \frac{\varepsilon_s E_\infty^2 a_i}{\mu_s} \frac{R_i(1 - R_i S_i)}{(1 + 2R_i)^2(1 + M_i)} \hat{\mathbf{E}}_\infty \hat{\mathbf{E}}_\infty \\ & : \left[ (\mathbf{I} - 3\hat{\mathbf{d}}\hat{\mathbf{d}}) \left(\frac{a_i}{d}\right)^2 \hat{\mathbf{d}} + \frac{1}{3} \nabla \left( \mathbf{I} \left(\frac{a_i}{d}\right)^3 - 3\hat{\mathbf{d}}\hat{\mathbf{d}} \left(\frac{a_i}{d}\right)^3 \right) \right] + \mathcal{O}\left(\left(\frac{a_i}{d}\right)^5\right). \end{aligned} \quad (8)$$

The electric and flow fields have fore-aft about the equator and axial symmetry about the field direction, illustrated by the field lines and streamlines in figure 1, and a single drop undergoes no translational motion. Upon addition of a second drop, that symmetry is broken. The disturbance electric and velocity fields from one drop act on the other, and vice versa, resulting in translational motion of the drops.

To describe the interactions between drops, we introduce the notation  $\mathbf{F}_{ji}$  and  $\mathbf{U}_{ji}$ , where the subscripts denotes the force or velocity on drop  $j$  due to its interaction with drop  $i$ . Approximating each drop as a point dipole, the DEP force on drop  $j$  in the disturbance electric field of drop  $i$  is

$$\mathbf{F}_{ji} = \mathbf{P}_j \cdot \nabla \mathbf{E}_i|_{\mathbf{x}=\mathbf{x}_j}, \quad (9)$$

where  $\mathbf{P}_j$  is the polarizability of drop  $j$ ,  $\mathbf{P}_j = 4\pi\varepsilon_s a_j^3 \frac{1 - R_j}{1 + 2R_j} \mathbf{E}_\infty$ , and  $\nabla \mathbf{E}_i|_{\mathbf{x}=\mathbf{x}_j}$  is the gradient of the electric field around drop  $i$  evaluated at the center of drop  $j$ . The translational velocity of drop  $j$ , considering the EHD and DEP interactions with drop  $i$ , as well as the drag on drop  $j$ , is then, via Faxén's law for drops [44],

$$\mathbf{U}_{ji} = \left(1 + \frac{a_j^2 M_j}{2(2 + 3M_j)} \nabla^2\right) \mathbf{u}_i(\mathbf{x})|_{\mathbf{x}=\mathbf{x}_j} + \frac{1}{2\pi\mu_s a_j} \frac{1 + M_j}{2 + 3M_j} \mathbf{U}_{ji}. \quad (10)$$

Insertion of equations (8) and (9) into (10) returns the velocity of each drop

$$\begin{aligned}
\mathbf{U}_{ji} = & \frac{9 \varepsilon_s E_\infty^2 a_i}{5 \mu_s} \left[ \frac{R_i(1 - R_i S_i)}{(1 + 2R_i)^2(1 + M_i)} P_2(\cos \Theta) \left(\frac{a_i}{d}\right)^2 \hat{\mathbf{d}} \right. \\
& - \frac{R_i(1 - R_i S_i)}{(1 + 2R_i)^2(1 + M_i)} \left( P_2(\cos \Theta) \hat{\mathbf{d}} + \frac{1}{2} \sin(2\Theta) \hat{\Theta} \right) \left(\frac{a_i}{d}\right)^4 \\
& - \left( \frac{3M_j}{(2 + 3M_j)} \frac{R_i(1 - S_i R_i)}{(1 + 2R_i)^2(1 + M_i)} + \frac{20}{3} \frac{(1 + M_j)}{(2 + 3M_j)} \frac{(1 - R_j)}{(1 + 2R_j)} \frac{(1 - R_i)}{(1 + 2R_i)} \right) \\
& \times \left. \left( P_2(\cos \Theta) \hat{\mathbf{d}} + \frac{1}{2} \sin(2\Theta) \hat{\Theta} \right) \left(\frac{a_i^2 a_j^2}{d^4}\right) \right] + \mathcal{O}\left(\frac{a_i^2 a_j^3}{d^5}\right), \tag{11}
\end{aligned}$$

where  $P_2(\cos \Theta)$  is the second Legendre polynomial. Clearly, for nonidentical drops,  $\mathbf{U}_d = \mathbf{U}_{ji} - \mathbf{U}_{ij} \neq 2\mathbf{U}_{ji}$ , analogous to non-reciprocal interactions of phoretic particles with different interaction potentials [45, 46]. For dissimilar drops, the higher order, i.e.  $\mathcal{O}(a^4/d^4)$ , interactions depend on properties from both drops  $i$  and  $j$ , as seen in equation (11). This is a generalization of equation 4.8 in Sorgentone *et al.* [42], from which the orientation of an identical drop pair can be predicted based solely on the material properties of the system. The expression presented here, namely the second and third terms in equation (11), show that the interactions of dissimilar drops are more complex. When one drop is much larger than the other, equation (11) reduces to the EHD flow profile around the larger drop, with the smaller drop effectively acting as a tracer in the EHD flow of the larger drop. For drops of equal size but different constitution, the expression governing the  $\mathcal{O}(a^4/d^4)$  interactions of the drops becomes

$$\Phi_{ji} = \frac{1}{(2 + 3M_j)} \left( \frac{2(1 + 3M_j)R_i(1 - R_i S_i)}{(1 + M_i)(1 + 2R_i)^2} + \frac{20}{3}(1 + M_j) \frac{(1 - R_j)(1 - R_i)}{(1 + 2R_j)(1 + 2R_i)} \right), \tag{12}$$

where  $\Phi_{ji}$  denotes the  $\mathcal{O}(a^4/d^4)$  contribution to the velocity of drop  $j$  due to its interaction with drop  $i$ . Equation (12) shows that two drops may align perpendicular to the electric field direction if their conductivities are larger and smaller, respectively, than the suspending phase (*i.e.*  $R_i < 1 < R_j$ ). Thus,  $\Phi_{ji}$ , and therefore the total interaction of the drop pair, cannot be described using  $\Phi_i$  and  $\Phi_j$  for interactions of identical drops of type  $i$  and  $j$ . For drops of identical size and constitution (*i.e.* when  $M_j = M_i$ ,  $R_j = R_i$ ,  $S_j = S_i$ , and  $a_j = a_i$ ),  $\mathbf{U}_d = 2\mathbf{U}_{ji}$ , and equations (11) and (12) reduce to equations 4.7 and 4.8 for identical drops

given by Sorgentone *et al.* [42]

$$\begin{aligned} \mathbf{U}_d = & \frac{18 \varepsilon_s E_\infty^2 a}{5 \mu_s} \left[ \frac{R(1-RS)}{(1+2R)^2(1+M)} P_2(\cos \Theta) \left(\frac{a}{d}\right)^2 \hat{\mathbf{d}} \right. \\ & \left. - \Phi \left( P_2(\cos \Theta) \hat{\mathbf{d}} + \frac{1}{2} \sin(2\Theta) \hat{\Theta} \right) \left(\frac{a}{d}\right)^4 \right] + \mathcal{O} \left( \left(\frac{a}{d}\right)^5 \right), \end{aligned} \quad (13)$$

and

$$\Phi = \frac{1}{(2+3M)(1+2R)^2} \left( \frac{2(1+3M)R(1-RS)}{(1+M)} + \frac{20}{3}(1+M)(1-R)^2 \right). \quad (14)$$

Equations (11) and (13) can be reduced to pure dielectrophoresis of conducting drops by setting  $S = 1/R$ , where the EHD interaction of  $\mathcal{O}(a^2/d^2)$  is absent and the weaker DEP governs the interaction of the drops to leading order of  $\mathcal{O}(a^4/d^4)$ . In this case, the charging timescales of the drop and suspending phases match ( $\varepsilon_d/\sigma_d = \varepsilon_s/\sigma_s$ , or  $RS = 1$ ) and the tangential electric stress on each side of the interface balance, eliminating the driving force for the interface to shear and resulting in the EHD flow vanishing, exemplified by  $\mathbf{u}_i = 0$  when  $RS = 1$  in equation (8).

The relative velocity of the drop pair can be used to determine the trajectory of the drop pair via the relations

$$\frac{dd}{dt} = \mathbf{U}_d \cdot \hat{\mathbf{d}}, \quad \text{and} \quad d \frac{d\Theta}{dt} = \mathbf{U}_d \cdot \hat{\Theta}, \quad (15)$$

where  $d$  is the separation distance between the centroids of the drops and  $\Theta$  is the angle between the drops' line of centers and the electric field direction, equal to  $\arccos(\mathbf{E}_\infty \cdot \hat{\mathbf{d}})$ . The unit vectors  $\hat{\mathbf{d}}$  and  $\hat{\Theta}$  are those pointing along the line of centers of the drops and perpendicular to the drops' line of centers. Additionally, the position of each drop can be tracked individually as

$$\frac{d\mathbf{x}_j}{dt} = \mathbf{U}_{ji}, \quad (16)$$

which, while a trivial result, can be extended to predict the behavior of multiple drops, as follows. When there are multiple drops, it is assumed that each drop moves due to pairwise interactions with every other drop. The position of each drop can then be predicted by summing over the interactions of that drop with all other drops. This yields the same expression as equation (16), but now including a sum over  $i$ . The positions of the entire

collection of drops can then be described as

$$\frac{d\mathbf{x}_j}{dt} = \sum_{i \neq j}^N \mathbf{U}_{ji}, \text{ for } j = 1, 2, \dots, N, \quad (17)$$

where  $\mathbf{x}_j$  is the position of the  $j$ th drop,  $\mathbf{U}_{ji}$  is the velocity of drop  $j$  due to its interaction with drop  $i$ , and  $N$  is the total number of drops in the system.

The trajectories of a set of two or more drops can be predicted via integration of equation (17). The positions of the drops in time are hence calculated by numerically integrating equation (17) using a forward Euler scheme with time step  $0.001t_c$ , where  $t_c = \mu_s/\varepsilon_s E_\infty^2$  is the characteristic timescale of the EHD flow. In the next sections, these calculated trajectories are compared to experimental results in various scenarios, and theoretical results for other scenarios are shown as well.

#### IV. MATERIALS AND METHODS

Experiments were performed in a 3D-printed acrylic cell 2.8cm width  $\times$  3.6cm length  $\times$  7cm height developed by Sengupta *et al* [47]. Two stainless steel electrodes 35 mm wide are set 28 mm apart. Voltages of 2, 3, 4, and 5 kV are applied to one electrode from a high-voltage power supply (Gamma High Voltage Research, Inc.) with the other grounded, resulting in calculated electric field strengths of 0.714 kV/cm, 1.07 kV/cm, 1.43 kV/cm, and 1.79 kV/cm, respectively, in the cell. A foot switch connected to the voltage supply circuit allows for rapid and safe activation/deactivation of the electric field. Drops of volume 1  $\mu$ L (620  $\mu$ m radius) are administered using a 25  $\mu$ L glass syringe with a grounded 22s gauge stainless steel needle (Hamilton). After insertion into the cell, drops are then placed in their initial positions by moving nearby fluid using the grounded needle. The two walls adjacent to the electrodes have circular windows, where drops are imaged using a camera (Point Grey Grasshopper) with a 10 $\times$  objective lens (Nikon) and a fiber optic back light (QVABL, Dolan-Jenner). The drops are initially placed in the same focal plane. Via equation (11), drops positioned in the plane made by the field direction and the line connecting their centers will only move within that plane. Visual observations made during the experiments indicate that out-of-plane motion is small compared to that in-plane. A schematic of the setup is shown

in figure 3. Images are recorded at 7 frames per second with LabView. Drop positions and trajectories are analyzed in MATLAB with the function *imfindcircles*; the data is smoothed for clarity by taking a moving average of the previous 7 data points and data points spaced one second apart are shown.

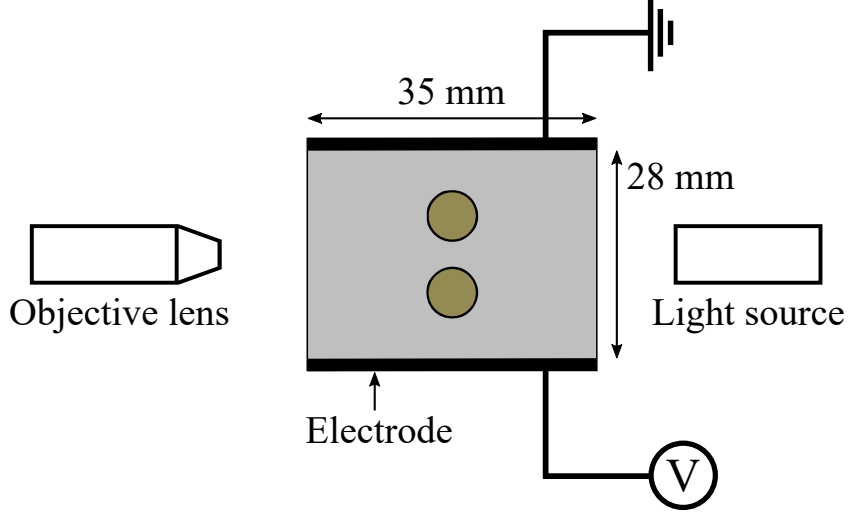


FIG. 3. Schematic of experimental setup. Drops are initially placed in the same focal plane, where they tend to remain throughout the experiment.

The oils used are 350 cSt silicone oil (Sigma-Aldrich) and castor oil (Sigma-Aldrich). Prediction of the interaction between drops requires accurate knowledge of the drop and suspending phase fluid and electrical properties. Electrical properties are taken from Lanauze *et al.* [23], wherein electrical impedance spectroscopy was used [48] and the viscosities of the fluids are measured using a concentric cylinder rheometer (DH-2, TA Instruments) at 20°C. The densities are considered as given by the supplier. These material properties are given in Table I.

Fluid	$\varepsilon$	$\sigma$ (S/m)	$\mu$ (Pa s)	$\rho$ (kg/m <sup>3</sup> )
Castor oil	4.9	$5.8 \times 10^{-11}$	0.99	961
Silicone oil	2.8	$2.0 \times 10^{-12}$	0.39	970

TABLE I. Material properties for a silicone oil drop suspended in castor oil. Here,  $\varepsilon$  denotes the relative permittivity.

For identical drops, the quantity  $1 - RS$  and the expression for  $\Phi$  in equation (14) are enough to qualitatively predict how a given pair of drops will behave. The leading order

term in equation (13) determines the relative velocity of the drop pair at large separation distances. This term is purely electrohydrodynamic, since it vanishes if  $1 - RS = 0$ . The sign of  $1 - RS$  determines the direction of this EHD interaction, where if  $1 - RS > 0$  ( $< 0$ ),  $U_d > 0$  ( $< 0$ ), and widely separated drops will repel (attract) when  $P_2(\cos \Theta) > 0$ , or  $\Theta < 54.7^\circ$ , and attract (repel) when  $\Theta > 54.7^\circ$ . The shorter range  $\mathcal{O}(a^4/d^4)$  contribution to the relative velocity is due to a combination of both EHD and DEP. The expression  $\Phi$  quantifies the interplay between EHD and DEP interactions, and can be used with the sign of  $1 - RS$  to predict whether or not a drop pair will come together or drift apart. From equation (13), the only contribution to the drop pair orientation relative to the field is scaled by  $-\Phi$ . As indicated in figure 2, positive motion in the  $\hat{\Theta}$  direction constitutes a rotation toward a perpendicular alignment relative to the field. Thus, just by knowing the sign of  $\Phi$ , the direction the drop pair aligns can be predicted. Finally, to qualitatively approximate the dependence of the pair interaction on separation distance, Sorgentone *et al.* introduced a critical separation distance,  $d_c$ , solved by setting  $U_d = 0$  and  $\Theta = 0$  or  $\pi/2$ . From Sorgentone [42] *et al.*,

$$\frac{d_c}{a} = \sqrt{\frac{(1 + 2R)^2(1 + M)}{R(1 - RS)}}\Phi. \quad (18)$$

The critical separation distance  $d_c$  gives the centroid separation where the effects of EHD and DEP balance, and is an equilibrium point where the drops do not move relative to each other. Above this separation distance, long range EHD interactions will dominate, and below this separation distance the drop motion will be dominated by DEP. The combined use of  $1 - RS$ ,  $\Phi$ , and  $d_c$  to predict the long-time behavior of a leaky dielectric drop pair can be visualized as a phase diagram for a chosen value of one of the three material property ratios. For  $M = 1$ , the associated phase diagram is shown in figure 4. For systems where  $\Phi < 0$ , drop pairs rotate toward a perpendicular alignment with the field. The line  $\Phi = 0$  never crosses  $RS = 1$ , thus systems where  $\Phi < 0$  will always have  $RS > 1$  and will repel when aligned perpendicular to the field. In these cases,  $d_c/a$  is never greater than 2, and drops will repel, however the error in prediction grows as drop separation decreases. In the region where  $\Phi > 0$  and  $RS > 1$ , drops align parallel to the field and attract along their alignment. Here, since  $1 - RS < 0$  while  $\Phi$  is positive,  $d_c$  is imaginary, and the interaction behavior is directionally identical to pure DEP. When  $RS < 1$ ,  $\Phi$  is always positive and drops

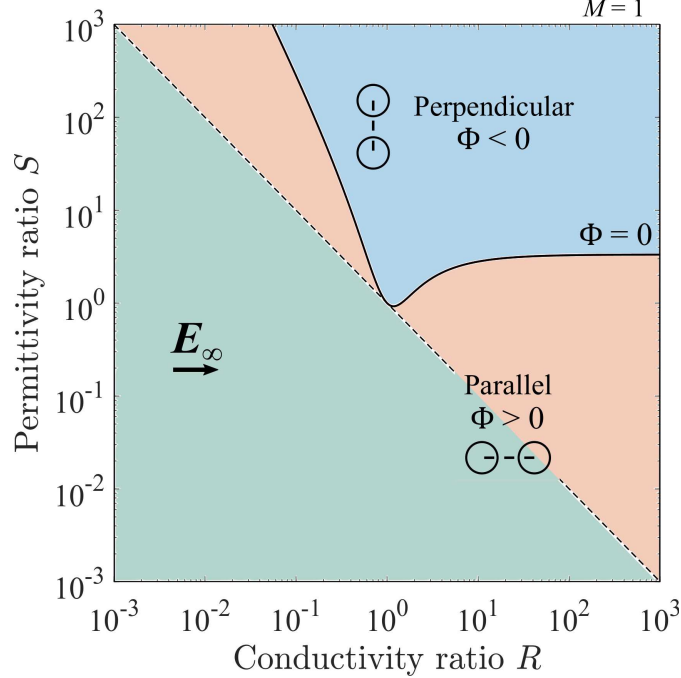


FIG. 4. Phase diagram for behavior of a pair of equiviscous ( $M = 1$ ), identical, leaky dielectric drops with permittivity ratio  $S$  and conductivity ratio  $R$ , based on equation 4.8 from Sorgentone *et al* [42].

The solid black line denotes combinations of  $S$  and  $R$  for which  $\Phi = 0$  and the orientation of the drops is steady in time. In the (blue) region above the black line,  $\Phi < 0$ , such that material systems in that region will show drop pair rotation toward  $\Theta = \pi/2$ . Below the black line,  $\Phi > 0$ . In the (orange) region between the lines of  $\Phi = 0$  and  $RS = 1$  drop pairs will rotate toward parallel and attract when  $\Theta < 54.7^\circ$ . In the green region below  $RS = 1$ , drop pairs will rotate toward parallel, however whether they attract or repel at  $\Theta < 54.7^\circ$  depends on the separation distance relative to  $d_c$  for the given  $M$ ,  $S$ , and  $R$ .

align along the field direction. In this region, whether the drops repel or attract in the field direction depends on their separation distance relative to  $d_c$ . At separations above  $d_c$  drops will repel in the field direction, while below  $d_c$  they will attract, making  $d_c$  in this case an unstable equilibrium position. Therefore the quantity  $1 - RS$ , equation (14), and equation (18) can be used to determine how a pair of identical drops will qualitatively behave under an electric field. For the system given in table I,  $M = 0.39$ ,  $R = 29$ , and  $S = 0.57$ . Although the phase diagram in figure 4 is for  $M = 1$ , not much change is observed when  $M = 0.39$ , placing the system of silicone oil drops suspending in castor oil in the orange region of figure 4. Here, the product  $RS = 17 > 1$  and  $\Phi = 0.53 > 0$ . Thus, these drops are predicted to align parallel to the field and attract one another.

In practicality, the material properties of systems where  $\Phi < 0$  are heavily constrained.

As  $M$  increases from unity for figure 4, the line for  $\Phi = 0$  on the right side of the diagram increases in slope, making the region of  $S$  and  $R$  for which  $\Phi < 0$  narrow quickly. In the EHD literature, the maximum value of  $S$  is around 40, corresponding to water ( $\varepsilon \approx 80$ ) in oil ( $\varepsilon \gtrsim 2$ ) [16, 49–51], thus narrowing the accessible zone of the phase diagram in real systems. The dip at  $S = R = 1$ , remains unchanged with  $M$ . Thus, fluid combinations with similar conductivities are seemingly feasible systems to have  $\Phi < 0$ . These systems, however, clearly must be immiscible, with distinct permittivities, as well as low capillary numbers and matched densities, such that the drops will not break up at field strengths needed to observe their interaction, or settle on a timescale faster than their interaction. These conditions are not wholly exclusive, however experimental evidence of interactions for drops with  $\Phi < 0$  has not been reported as of this writing.

The theory presented in Section III relies on the assumptions that the capillary number, Reynolds number, and electric Reynolds number are small. A typical capillary number in our experiments is calculated to be  $Ca = 0.19$ , using an initial drop radius of  $620 \mu\text{m}$  and a surface tension value for castor oil and silicone oil of  $4.5 \text{ mN/m}$  from Salipante & Vlahovska [22]. Using outer phase properties of castor oil, the Reynolds number  $Re = 5.24 \times 10^{-4}$ , and the electric Reynolds number  $Re_E = 1.05$ . An electric Reynolds number of 1.05 indicates the effect of surface charge convection may not be negligible, however for the sake of qualitatively predicting drop interactions, we will show that use of this assumption is reasonable, and in fact variation of  $Re_E$  will be shown to have little impact on the interaction dynamics in Section V A.

## V. RESULTS AND DISCUSSION

### A. Interaction of identical drops

Results are presented of two identical silicone oil drops suspended in castor oil subject to a uniform electric field. Via table I, the material property ratios for this system are  $M = 0.39$ ,  $R = 29$ , and  $S = 0.57$ , thus equation (1) dictates that these drops will deform into oblate spheroids, where the major axis is perpendicular to the field direction. Here, the product  $RS > 1$ , therefore drops aligned at angles  $\Theta < 54.7^\circ$  to the field should attract and drops at angles  $\Theta > 54.7^\circ$  to the field should repel. In the first set of experiments, drops



are initially aligned parallel ( $\Theta = 0^\circ$ ) or perpendicular ( $\Theta = 90^\circ$ ) to the field direction. The relative velocity and trajectory of the drop pair should then only be a function of the centroid separation  $d$  of the drops. Figures 5a and 5b show the separation distance of parallel and

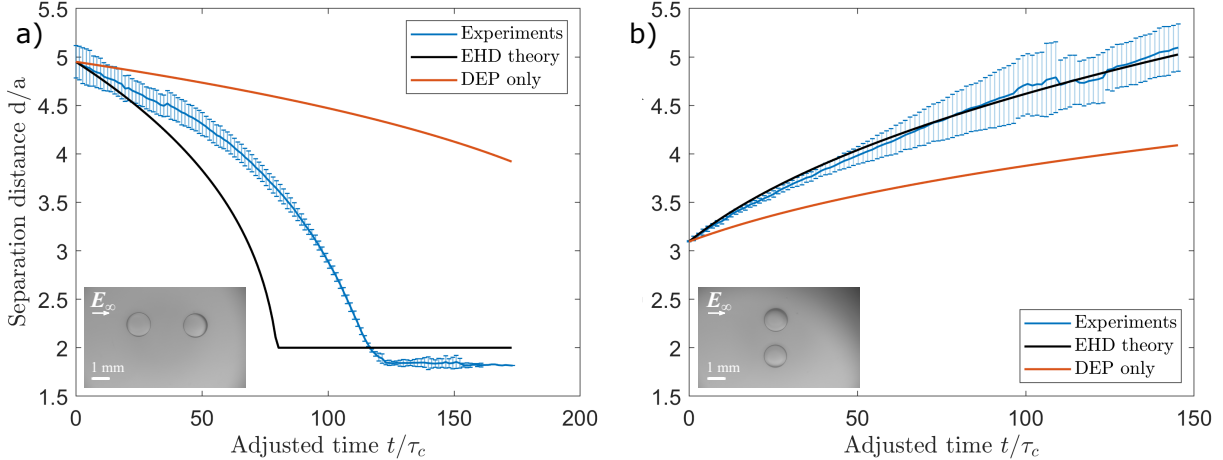


FIG. 5. (a) Centroid separation between two 350 cSt silicone oil drops in castor oil aligned parallel to the field. (b) Centroid separation between two drops aligned perpendicular to the field. Error bars represent a standard deviation of interpolated and time-averaged experiments. In both cases,  $\sin(2\Theta) = 0$  and minimal rotation of the drop pair is observed.  $E_\infty = 1.79$  kV/cm and  $a = 620$   $\mu\text{m}$ .

perpendicular aligned drops as a function of dimensionless time, respectively, where time is nondimensionalized with  $\tau_c = \mu_s/\varepsilon_s E_\infty^2$ . Insets in the bottom corners are pictures of the initial positions of the drops in one of the experiments included in each of the presented datasets. In these experiments, precise repeated placement of the drops in the same initial position is difficult. To analyze the data from experiments started at the same initial angle but varying separation distances, we consider the fact that the interactions between the drops are strongest (and therefore the most reproducible) the closer the drops are together. Since  $Re \ll 1$ , the flow is reversible, therefore the time axis of each experiment is shifted (without changing the time increment between the data points) such that the slope of separation distance versus time for each experiment reaches a minimum value at the same time, allowing a clear comparison of the trajectories between experiments. These experimental trajectories are shown with the EHD theory of equation (13) and the case of pure DEP ( $S = 1/R$ ). The theoretical trajectories include a cut off at  $d/a = 2$ , where a hard sphere interaction is imposed. Clearly, considering only DEP results in a drastic under-prediction of the rate of

approach of the drop pair, which strongly suggests that EHD interactions are present. When drops are attracting (figure 5a), a faster approach is predicted compared to the experiments when starting at a separation distance  $d/a \approx 5$ . Additionally, the drops attain a minimum centroid separation of 1.8, which can be attributed to the oblate deformation of the drops, whereas perfect spheres will reach a minimum separation of 2. Prediction of the repulsive interaction between the drops, on the other hand, matches quite well with the measured trajectories. The asymptotic theory here is accurate through  $\mathcal{O}(a^4/d^4)$ , and is therefore restricted to descriptions of widely separated drops, so predicted and measured trajectories should become increasingly disparate as drops come closer together. A comparison can be made to figures 7 and 8 in Sargentone *et al.*, which show the asymptotic theory for identical drops along with boundary integral computations. At separations as low  $d/a = 3.5$ , the theory and computations are nearly identical, yet diverge as separation distance decreases. The same divergence between the asymptotic method of reflections and a more rigorous approach like the twin multipole re-expansion can be seen in similar systems of conducting spheres in electrolyte [52]. While the asymptotic theory loses accuracy with decreasing separation distance, the error in the measured trajectories is observed to increase when drops are further apart. This is attributed to the fact that when the drops are relatively close together, their interaction velocity is strong compared to any interfering effects, such as gravity, migrations due to field distorting impurities and charge carriers, or triboelectric charge. When the drops are further apart, the relative strength of interaction is abated compared to the uncontrolled effects just stated, hence the widening of error bars at larger  $d/a$  in figure 5. Evidently, then, there is then a desirable experimental range for attractive interactions around  $d/a = 4-4.5$ , where the pair interactions dominate in the system and the drops are separated enough for the theory to be qualitatively relevant. In light of this fact, the asymptotic theory qualitatively predicts the observed experimental trajectories quite well.

Admittedly, the electric Reynolds number of the suspending phase,  $Re_{E_s} = 1.05$ , is not small. The drop phase value,  $Re_{E_d} = 25.52$ , is even larger, clearly in violation of the assumption that  $Re_E \ll 1$ . To determine the impact of  $Re_E$  and surface charge convection on the drop trajectories, experiments of parallel- and perpendicular- aligned drops were performed at various electric field strengths. The effect of surface charge convection on the interac-

tion velocities of the drops can be visualized by normalizing the time over which the drops interact by  $\tau_c$ , where  $E_\infty$ , and thus  $\tau_c$ , now varies between experiments. Results for drops with  $\Theta = 0^\circ$  are plotted in figure 6a and 6b, and with  $\Theta = 90^\circ$  in 6c and 6d. Normalization of time by  $\tau_c$  collapses the trajectories together, indicating that the role of surface charge convection either has a small influence on the interactions at the separation distances shown, or the effect similarly scales with  $E_\infty^2$ . It should be noted as well that  $Ca$  similarly scales with  $E_\infty^2$ , however the maximum  $Ca$  achieved is 0.19, and as seen in the insets of figure 5 the drops remain nearly spherical. Therefore, the collapse of the trajectories in figure 6 justifies the choice of a 5 kV applied voltage, where the strongest possible interactions between drops can be induced without observing a change in the dynamics of their interaction. Included in figure 6b and 6d are dimensionless theoretical trajectories for attracting and repelling drops, respectively. There is a slight over-prediction of the perpendicular drop separations, however this is consistent with figure 5b. In both cases, the asymptotic theory performs reasonably well in predicting the normalized behavior of the drops, demonstrating that the physics inherent in these pairwise interactions are captured, and that using the largest voltage difference of 5 kV to conduct the experiments does not appreciably impact the dynamics of the drops.

We now consider drops unaligned with the electric field direction. Drops with an angle  $\Theta \neq 0$  and  $\Theta \neq 90^\circ$  will rotate due to the  $\mathcal{O}(a^4/d^4)$  EHD and DEP interactions of the drops, described by the  $\hat{\Theta}$  term in equation (13). The direction of the pair rotation can be predicted based on the discussion of  $\Phi$  in section IV, and here the dynamics of drop pair rotations are shown experimentally. In performing these experiments, similarly as discussed with figure 5, the drop interactions were stronger the closer the drops started together, while more variability was observed at larger separation distances. Like the experiments shown thus far, precisely matching initial conditions for the sake of comparison between trials is difficult. Additionally, unlike with drops aligned parallel or perpendicular to the field direction, normalizing the data between experiments starting at different initial positions proves infeasible, since the velocities of drop pairs at similar separation distances but different angles to the field (and vice versa) are not the same. In other words, drop pairs starting further apart may not “pass through” the same position as drops starting at a similar angle to the field but closer together, rendering comparison of their trajectories impossible. Consider

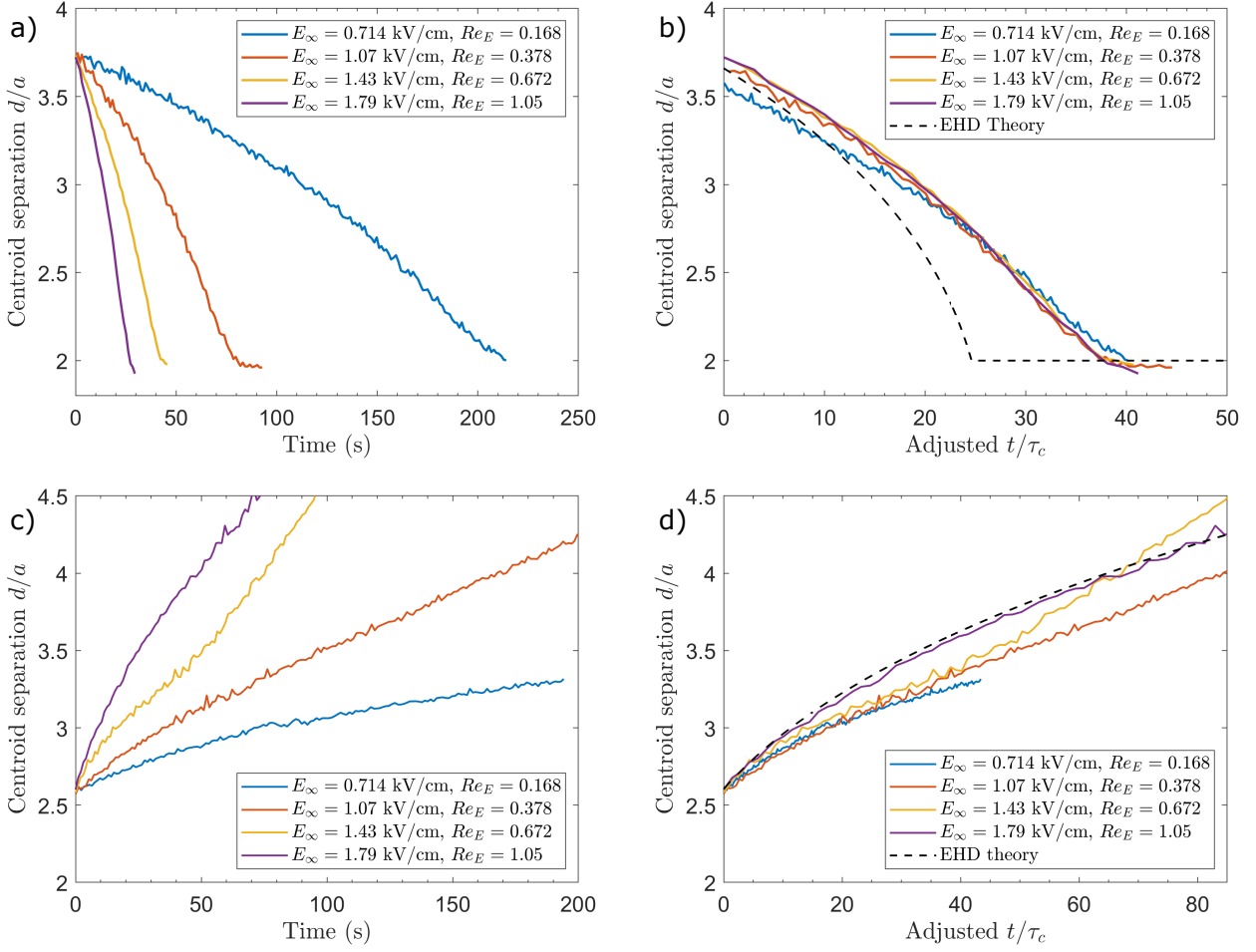


FIG. 6. Parallel and perpendicular drop trajectories for various applied voltages, with  $Re_E = \varepsilon_s^2 E_\infty^2 / \sigma_s \mu_s$ . (a) Drops are aligned parallel to the field direction. (b) Same trajectories as (a), with time normalized by  $\tau_c$ . (c) Drops are aligned perpendicular to the field. (d) Same trajectories as (c), with time normalized by  $\tau_c$ . Trajectories collapse upon normalization of time by  $\tau_c = \mu_s / \varepsilon_s E_\infty^2$ , indicating that the maximum voltage tested of 5 kV will not appreciably alter the dynamics of the drop interactions compared to lower voltages.

two experiments where drops start at the same  $d_0$  but differ in  $\Theta_0$  between runs. The two velocities scale with the same  $a/d_0$ , but values of the second Legendre polynomial, which also scale the interaction velocity, are different. Thus, the angle the drops' line of centers makes with the field can have noticeable effect on the drop pair dynamics, exemplified in figure 7. Figure 7a and 7b are the center to center and angular trajectories for a drop pair with  $d_0 = 4.7$  and  $\Theta_0 = 21^\circ$ , and figure 7c and 7d correspond to a drop pair with  $d_0 = 4.4$  and  $\Theta = 39^\circ$ . Even though the drop pair in figure 7a starts at a larger initial separation distance than in 7c, the drops closer together but starting at a larger  $\Theta$  attract each other more slowly.

The increased angle between the drop pair and the electric field results in a reduced initial relative velocity, as  $P_2(\cos(21^\circ)) = 0.80$ , while  $P_2(\cos(39^\circ)) = 0.41$ . Note that equation (13) is successful at predicting both the center-to-center and angular initial trajectories of the drop pairs in figure 7; although seemingly large, the early discrepancy in  $\Theta$  between the experimental and theoretical trajectories in figure 7b is only about  $3^\circ$ . The prediction of  $\Theta$  is seen to quickly diverge from the measured values at the same time that the predicted and measured separation distances split. The failure of equation (13) to quantitatively capture the dynamics of the drops at close distances is indicative of the method of reflections employed, and should not obfuscate the qualitative success of the theory in predicting drop pair behaviors. That the nature of interactions between arbitrarily positioned drops, and the timescale of their interaction, can be predicted underscores the power of the asymptotic method of reflections. Experiments are also performed of drops initially unaligned with the field at angles larger than  $\Theta = 54.7^\circ$ . At these angles, drop pairs will initially repel while still rotating toward the electric field direction and decreasing  $\Theta$ . Upon crossing  $\Theta = 54.7^\circ$ , the center-to-center interaction switches from repulsive to attractive, and the drops begin to approach each other. An example of this behavior is shown in figure 8. The initial separation  $d_0/a$  of the drops is just over 2, and the drops rotate toward parallel and repel to a maximum of 2.9 where they reach an angle of  $\Theta \approx 54.7^\circ$ . At this moment, the centerline velocity of the drops is no longer repulsive, and the drops approach each other until they are near contact. While these dynamics are captured with equation (13), the extent of repulsion and the timescale of the interaction are not in quantitative agreement. This is entirely expected to be the case with an asymptotic theory being only accurate through  $\mathcal{O}(a^4/d^4)$ . Over the course of the whole experiment, the drops never reach a separation distance large enough where the error from neglected terms can be accurately ignored, and thus comparison of the data shown in figure 8 to the EHD theory should only be for qualitative consideration. Nonetheless, the ability to capture qualitatively the dynamics of drop pairs unaligned with the electric field, even at small separation distances, with an asymptotic theory for widely separated drops is remarkable.

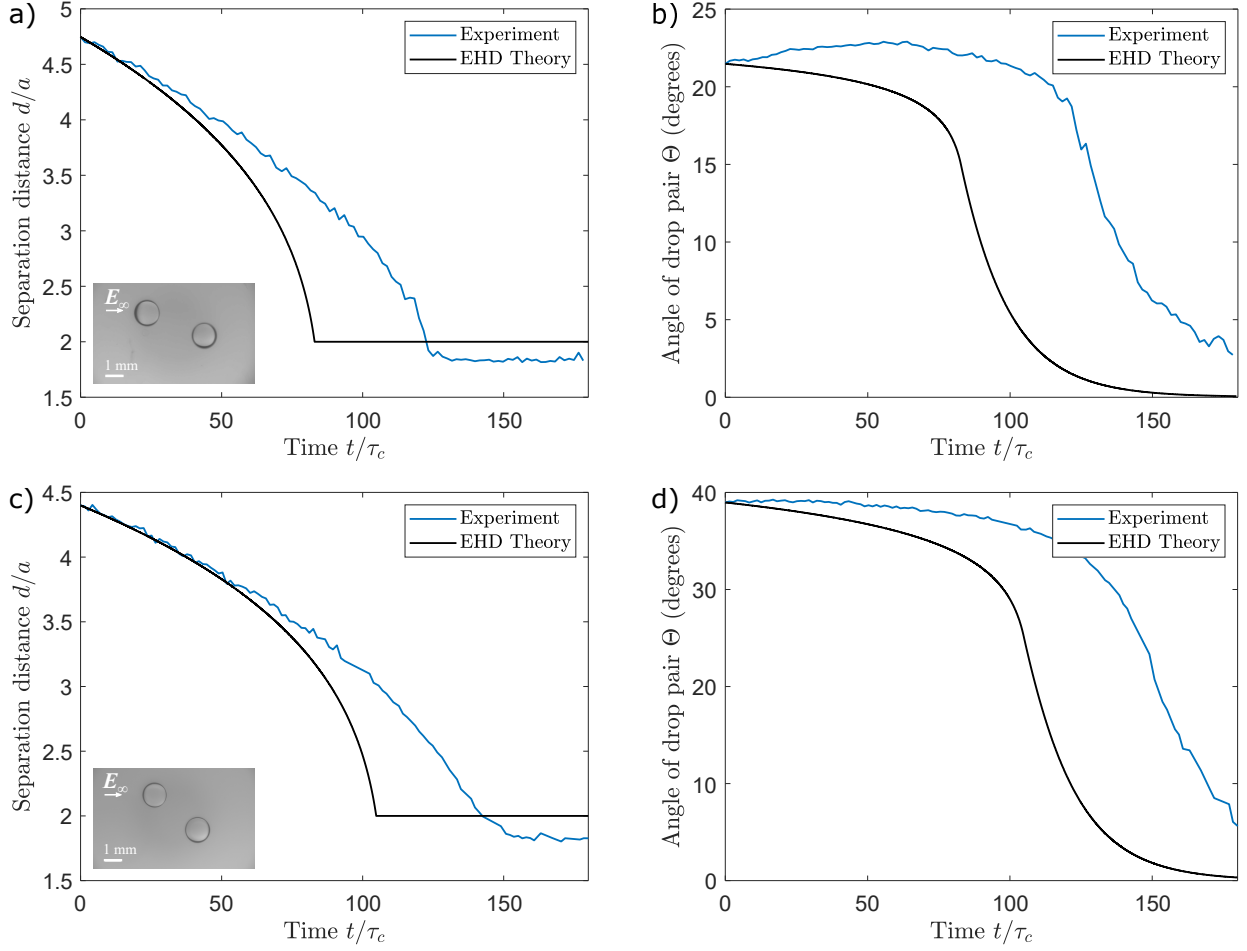


FIG. 7. (a) Separation distance between the centers of drops unaligned with the field direction and (b) angle between the line of centers of the drops and the field direction, for drops initially placed with  $d_0/a = 4.7$  and  $\Theta_0 = 21^\circ$ . (c) Separation distance and (d) angle between line of centers and field, for drops initially placed with  $d_0/a = 4.4$  and  $\Theta_0 = 39^\circ$ . The vector between the drops points from the drop on the left to the one on the right, and angles plotted are  $|\Theta|$  (therefore always between 0 and  $90^\circ$ ).

### B. Interaction of dissimilar drops

Here we consider the interaction of drops of different sizes and composition. When drops are differing in size, the strength of interaction of the smaller drop acting on the larger one is no longer the same as the larger drop acting on the smaller. This is evident in the velocity scale for drop  $j$  in the presence of drop  $i$ ,  $U = \varepsilon E_\infty a_i / \mu_s$ , scaling with the radius  $a_i$ . Due to these nonreciprocal interactions, the center of mass between the drops is not constant in time, and the relative velocity of the drop pair must be modeled with the more general expression  $\mathbf{U}_d = |\mathbf{U}_j - \mathbf{U}_i|$ , where  $\mathbf{U}_j$  and  $\mathbf{U}_i$  are found via equation (11).

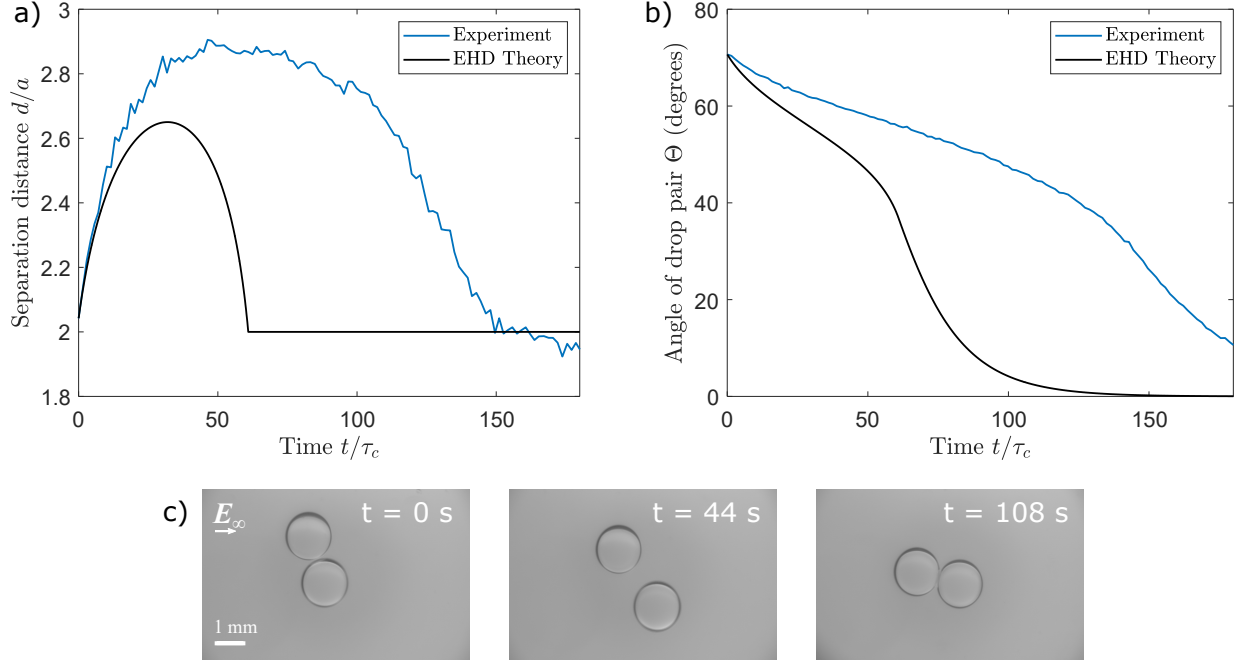


FIG. 8. (a) Separation distance between the centers of drops unaligned with the field direction and (b) angle between the drops' line of centers and the field direction. (c) Photos taken from the experiment showing the progression of drop positions in time. At the initial time  $\Theta_0 > 54.7^\circ$ , and drops initially repel. The vector between the drops points from the drop on the left to the one on the right, and angles plotted are  $|\Theta|$ .

We compare calculation of the trajectories using equation (11) for two drops, one of radius  $a_j = 620 \mu\text{m}$  (same size as the previous experiments) and the other  $a_i = 391 \mu\text{m}$  (a quarter the volume of drop  $j$ , or  $0.25 \mu\text{L}$ ), to that for identical drops using an average radius in equation (13) in figure 9. As shown similarly for identical drops, equation (11) predicts the interaction of the drops reasonably well at separation distances of around  $d/a_{avg} = 4$  and larger. For comparison, the trajectory is shown for identical drops using the mean size  $a_{avg} = 505.5 \mu\text{m}$  of the two dissimilar drops. Both equation (11) for dissimilar drops and equation (13) for identical, average-sized drops agree qualitatively with the experimental trajectory of the drops. Only a slight difference is observed between the two predictions, which is expected upon briefly comparing the differences in leading order  $\mathcal{O}(a^2/d^2)$  terms of the interaction velocities. With the drop sizes given above, the leading order terms can be used to estimate how different predictions from equation (13) for identical, average-sized drops will be compared to predictions for dissimilar drops using equation (11). The leading order relative velocity of identical, average-sized drops scales as  $2a_{avg}^3/d_0^2$ , while the leading

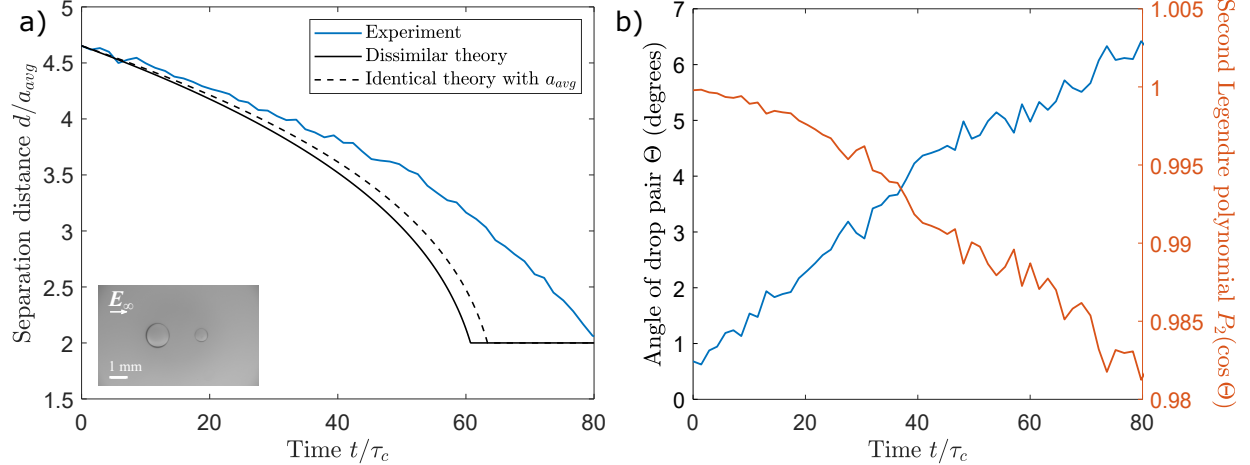


FIG. 9. (a) Normalized separation distance  $d/a_{avg}$  for drops of dissimilar size. Solid black line indicates theoretical prediction of the separation distance from equation (11); dotted black line indicates prediction for identical drops with equation (13) using an average radius of  $505.5 \mu\text{m}$ . Inset shows initial position of drops when electric field is applied. (b) Angle between line of centers and the field direction shown with corresponding values of the second Legendre polynomial. The largest angle observed between the line of centers and the applied field is  $\Theta \approx 0.11$ , which gives a value of 0.98 for the second Legendre polynomial.

order relative velocity of a dissimilar drop pair scales as  $a_i^3/d_0^2 + a_j^3/d_0^2$ , giving the ratio of the two relative velocities, respectively, as  $2a_{avg}^2/(a_i^3 + a_j^3)$ . From this expression, the predicted leading order velocity for identical, average-sized drops will always be slower than that predicted for dissimilar drops, which coincides with the faster predicted approach of dissimilar drops observed in figure 9. To highlight the non-reciprocal EHD interactions of the drop pair, a parallel initial configuration of the drops is chosen in order to minimize the effect of gravitational settling on the pair dynamics. We find that although there is some slight vertical misalignment of the drops, due to the larger drop settling faster than the smaller one, the drop pair only briefly reaches a maximum rotation of  $\Theta \approx 0.11$ , or  $6^\circ$ , shown in figure 9. Calculation of the reduction in the interaction velocity because of this brief off-parallel alignment shows only a 2 % difference in the calculated value ( $P_2(\cos(6.3^\circ)) = 0.98$  versus  $P_2(\cos(0)) = 1$ ), hence the effect of gravitational settling can be reasonably neglected. While a more precise calculation should include gravitational effects on the drop pair, figure 9 shows that the asymptotic theory is able to capture the EHD component of the interactions involved even when drops are of different sizes.

Unlike for differences in size shown above, small variations in material properties between



the drops can lead to starkly different pair interactions. As first noted by Zabarankin [39] for drops whose line of centers is parallel to the applied field, and here for drops in arbitrary orientations via equation (11), two oblatelly deforming drops may repel along the axis of the electric field if their conductivity ratios are larger and smaller than unity (*i.e.*  $R_i > 1 > R_j$ ). This counter-intuitive result is indicative of the fact that the interactions between materially dissimilar drops cannot simply be predicted by knowing the interactions for identical drops of each type. This repulsive interaction results from the direction of the polarizability of the drops, determined by the Clausius-Mossotti factor  $(1 - R)/(1 + 2R)$  [34]. For identical drops, the Clausius-Mossotti factors are the same, and thus the DEP force on each drop along the field axis is attractive. However, drops having Clausius-Mossotti factors of opposite sign will instead experience a repulsive DEP force along the field axis. For drops with high viscosity ratios (effectively rigid particles), or when the ratio  $RS \sim 1$ , the DEP interaction dominates and the drop pair will have a steady state configuration such that the drops are in contact and aligned perpendicular to the field direction.

The interactions between drops become more complex when EHD is accounted for. Unlike with DEP, the EHD interactions of the drops are non-reciprocal, such that the center of mass of the drop pair moves in time. Additionally, as with equation (18) for identical drops, a critical separation distance for dissimilar drops, where DEP and EHD balance, exists as well. This critical separation distance can be written as

$$d_c = \sqrt{\frac{(\alpha_{ji} + \alpha_{ij})a_i^2 a_j^2 + \beta_i a_i^4 + \beta_j a_j^4}{\beta_i a_i^2 + \beta_j a_j^2}}, \quad (19)$$

where

$$\alpha_{ji} = \frac{3M_j}{(2 + 3M_j)} \frac{R_i(1 - S_i R_i)}{(1 + 2R_i)^2(1 + M_i)} + \frac{20}{3} \frac{(1 + M_j)}{(2 + 3M_j)} \frac{(1 - R_j)}{(1 + 2R_j)} \frac{(1 - R_i)}{(1 + 2R_i)}$$

and

$$\beta_i = \frac{R_i(1 - R_i S_i)}{(1 + 2R_i)^2(1 + M_i)}. \quad (20)$$

Here,  $\alpha_{ji}$  denotes the prefactor for the  $a_i^2 a_j^2$  term in the velocity of drop  $j$  due to the presence of drop  $i$  given in equation (11), and  $\beta_i$  denotes the prefactor for the  $a_i^2$  and  $a_i^4$  terms in the velocity of drop  $j$  due to the presence of drop  $i$ . As with equation (18), for real values of

equation (19), the behavior of the drop pair will be drastically different depending on if  $d_0 < d_c$  or  $d_0 > d_c$ . The importance of considering EHD in the interactions of electrically dissimilar drops is showcased via simulations in figure 10. Figure 10 shows three cases

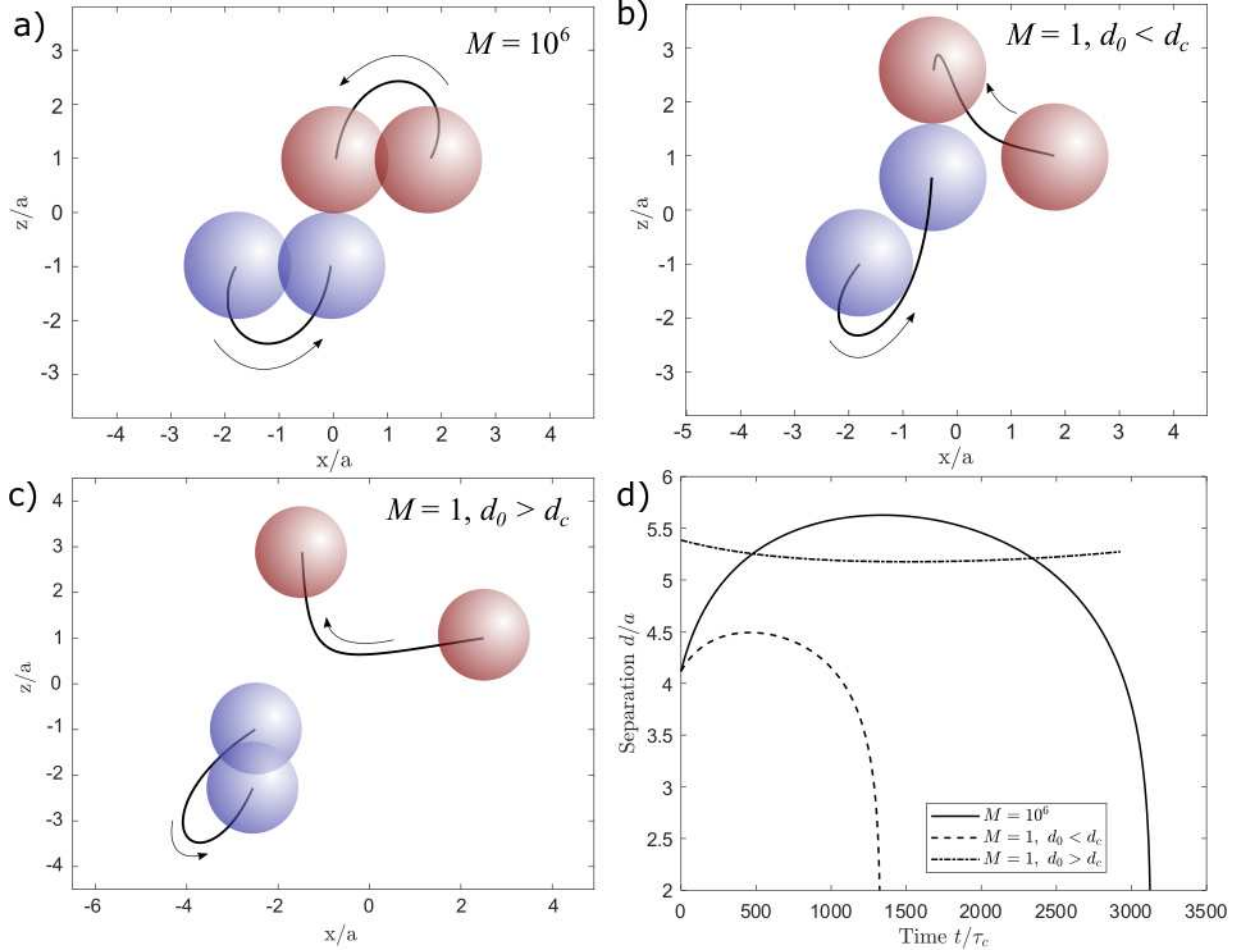


FIG. 10. Trajectories of drops in the plane made by the line connecting the centers of the drops and the field direction. In all cases,  $S_{blue} = S_{red} = 1$ ,  $R_{blue} = 10$ ,  $R_{red} = 0.1$ . a)  $M = M_{blue} = M_{red} = 10^6$ ,  $d_0/a = 4.1$ ,  $\Theta_0 = 29^\circ$ . b)  $M = 1$ ,  $d_0/a = 4.1$ ,  $\Theta_0 = 29^\circ$ . c)  $M = 1$ ,  $d_0 = 5.4$ ,  $\Theta_0 = 22^\circ$ . d) Plots of separation distance versus time for the cases a) (solid line), b) (dashed line), and c) (dot-dashed line). For cases b) and c),  $d_c/a = 5.1$ .

exemplifying the behavior described above. Here,  $S_i$  (blue) =  $S_j$  (red) = 1,  $R_i = 10$ , and  $R_j = 1$ . The viscosity ratio and the initial position of the drops is varied between cases. Figure 10a shows the spatial trajectories of the dissimilar drops just described, where both drops have a viscosity ratio of  $M = 10^6$ . Thus, DEP interactions dominate the behavior of the drop pair, and a symmetrical interaction where the drops eventually align perpendicular to the field direction and make contact at their equators is observed. In figure 10b, initial

conditions of the pair remain the same, however the drops are now equiviscous with the suspending phase and EHD plays a considerably larger role. While the ending configuration of the drop pair is the same as for the nearly rigid-particle case of figure 10a, the center of mass of the pair moves in time. The paths taken by the drops illustrates the non-reciprocity of their interaction. Importantly, the time required for the drop pair to reach its minimum separation distance is more than halved when EHD is present, as shown in figure 10d. Here, the DEP interaction of the drops drives the pair toward a perpendicular alignment with an initial repulsion, while the effect of the EHD interaction suppresses that initial repulsion, allowing the dynamics of the drop pair to occur at a closer separation distance where they will be stronger. The competition between EHD and DEP is made clear in figure 10c, where the initial separation of the drops  $d_0/a = 5.4$  is larger than the critical separation  $d_c/a = 5.1$ . Thus, the long range EHD interaction dominates, and the drops are driven toward a perpendicular alignment where they repel instead of attract. Hence, as shown in figure 10d, the drop pair will continue to repel after rotating above  $\Theta_c$  without making contact. Figure 10 exemplifies the complexity in dissimilar drop interactions under an applied field. The interplay between EHD and DEP effects results in dynamics of the drop pair that cannot simply be predicted based on the identical interactions of each drop phase.

### C. Interaction of multiple drops

Pairwise interaction calculations are commonly used to approximate behavior of large scale systems of drops or particles in various contexts [36, 46, 53–55]. In order to validate the use of a pairwise theory for systems of more than two drops, we compare the model to experiments of three and four identical drops. In figures 11 and 12, the center-to-center and angular components of equation (17) are shown alongside the trajectories of multiple drops. Qualitative agreement is observed between the pairwise theory and the 3-drop experiment shown in figure 11. The success in capturing the separation distances and angles of the vectors  $\mathbf{d}_{12}$ ,  $\mathbf{d}_{23}$ , and  $\mathbf{d}_{13}$  (indicated in figure 11c) shows that the evolution of the triangle made by the centers of the drops can be predicted up to around 48 seconds when a doublet between drops 2 and 3 is formed. After formation of the doublet, while still shown for the sake of comparison, the theory is inapplicable, as any lubrication effects that would arise

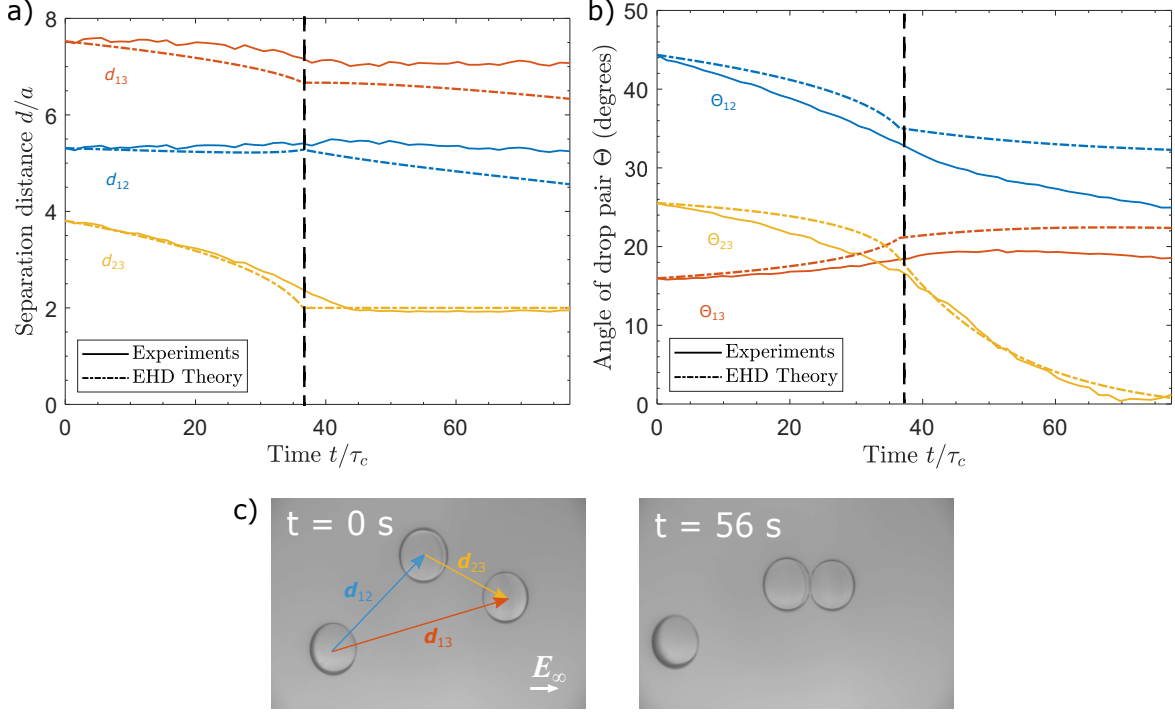


FIG. 11. (a) Separation distance between drop pairs for the three drop system. (b) Rotational dynamics between drop pairs for the three drop system. Angles plotted are  $|\Theta|$ . Vertical dotted line indicates moment drops 2 and 3 came together to form a doublet in the experiment, after which the theory is formally inapplicable. The kinks in the theoretical trajectories occur upon predicted formation of the doublet. (c) Photos of initial and final configuration of drops, with a schematic identifying the vectors plotted in (a) and (b).

upon near-contact of the drops are ignored, as well as higher order terms that would increase the accuracy of the model as the drops become close. In any case, the 3-body dynamics of this system are successfully captured. To explain this, it is noted that while equation (13) is valid for remote separations, higher order terms for both EHD and DEP come in  $O(a/d)^3$  smaller than the terms they are reflected from. Three-body interactions scale similarly, provided the drop sizes are similar, where a third drop of radius  $a_3$  would interact with drop 2 at leading order  $O(a_3/d)^2$ , which would then reflect to drop 1 at  $O(a_3^2 a_2^3/d^5)$  [43]. Thus, by only considering terms up to  $O(a/d)^4$ , three-body interactions can be ignored, and the pairwise theory of equation (17) is accurate to the same order for systems of 3 drops as it is for a drop pair.

Comparison of the pairwise additive theory to experiments of four drops, as shown in figure 12, also shows qualitative agreement. However, while the evolution of the system is

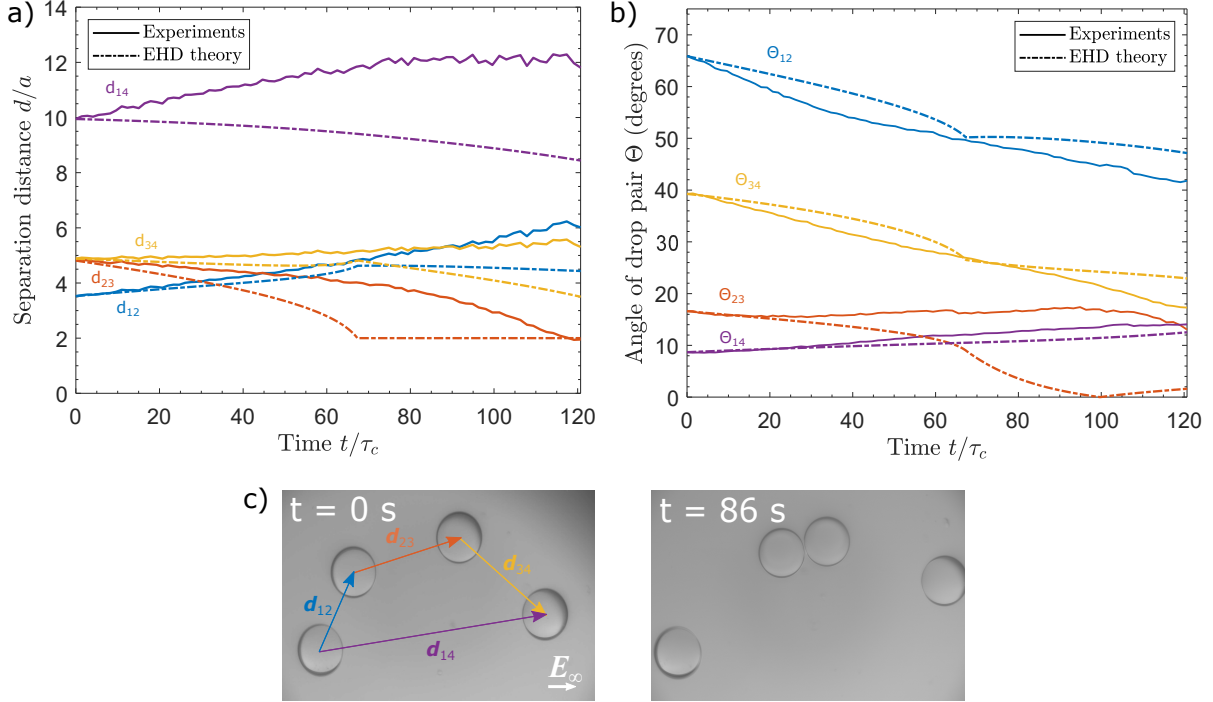


FIG. 12. (a) Separation distance between drop pairs within the four drop system. (b) Rotational dynamics between drop pairs within the four drop system. Angles plotted are  $|\Theta|$ . Here the experiment is stopped upon formation of the doublet between drops 2 and 3, however the theoretical prediction of doublet formation occurs at about 48 seconds. (c) Photos of initial and final configuration of drops, with a schematic identifying the vectors plotted in (a) and (b).

captured in this case, considerably faster dynamics are predicted compared to those observed experimentally. For instance, the formation of a drop 2-3 doublet is predicted to occur about twice as fast as seen in the experiment, and observe a similar difference in timescale between the theoretical predictions of the trajectories between the other drops. Considering the quality of agreement in figure 11, a likely source of the observed discrepancy in timescale is considered. Based on the observed increase in magnitude of the vector connecting drops 1 and 4, it is possible that the distances from drop 1 to drops 3 and 4, and likewise drop 4 to drops 1 and 2, are large enough such that the interaction along those vectors are small compared to noise from impurities or errant charge in the bulk. Thus, the interactions between drops 1 and 3, drops 1 and 4, and drops 2 and 4 that would in sum be attractive enough to pull drops 1 and 4 together are screened, and the pair of drops 1 and 2 initially repels with minimal interference from the other drops. Combined with the clockwise rotation of the pair of drops 1 and 2 and counterclockwise rotation of the pair of drops 3 and 4, respectively, drops 1 and

4 are driven apart. As a result, as the pair of drops 1 and 2 and the pair of drops 3 and 4 rotate toward parallel, their center-to-center attraction get stronger, slowing the time it would take for drops 2 and 3 to meet. Provided this is the case, the fact that the dynamics of four drops is qualitatively predicted bodes well for prediction of  $n$ -body systems of drops, which we plan to address in future work. These results thus show that equations (11), (13), and (17) provide a framework for the approximation of the behavior of large-scale systems of leaky dielectric drops using low cost simulations compared to more expensive boundary integral codes or multipole expansions incorporating large numbers of terms.

## VI. CONCLUSIONS

The three-dimensional interactions of leaky dielectric drops are analyzed using asymptotic analysis and experiments. The theory presented by Sargentone *et al.* [42] is generalized to consider dissimilar and multiple drops. The interaction parameter  $\Phi$  is examined, the sign of which is predictive of the direction that a drop pair will rotate relative to the field direction. In discussing the possibility of exploring the phase space of  $\Phi$  in practical systems, it is noted that inherent physical limits on  $S$  immediately reduce accessible regions of the  $\Phi$  phase diagram. Constraints of immiscibility, high surface tension, comparable densities, and similar conductivities in concert make practical realization of predicted yet so far experimentally unobserved drop pair behaviors unlikely in relevant applications.

The theory for identical drops of Sargentone *et al.* is compared to experiments of silicone oil drops suspended in castor oil, and it is shown that physics dominant in leaky dielectric drop interactions are captured. The theory is found to accurately predict the trajectories of drop pairs at separation distances as low as 3.5 radii; however, noise in experimental measurements of drop pair interactions may dominate over interaction dynamics at separations larger than 5 radii. Results are shown exemplifying the importance of the angle the drop pair makes with the field direction in determining how quickly drops will attract or repel. Drops are shown to not always interact in a monotonic manner, and the positions of drops at long times are heavily dependant on their initial placement. We find that the theory is successful in qualitatively predicting the dynamics observed in the experiments.

The theory of Sargentone *et al.* is generalized to consider the asymmetric interactions of

widely separated dissimilar drops, and systems of multiple drops through a pairwise additive approximation. Neglecting gravitational effects, it is shown that the theory is capable of predicting the trajectories of drops of different sizes. Simulated trajectories of drops of electrically dissimilar drops are also shown. These non-reciprocal interactions non-trivially impact the predicted trajectories of a drop pair. In cases of three and four drops, a summation of pairwise interactions between drops is shown to qualitatively predict the evolution of the many-body systems. The error in ignoring three-body interactions is of similar scale as the truncation error of  $\mathcal{O}(a^5/d^5)$  in the pairwise theory, allowing the use of the pairwise theory to predict the interactions of multiple drops. Although a more rigorous consideration of drop interactions via twin multipole re-expansions or boundary integral computations may provide more accurate resolution of drop interactions at close distances [39, 42, 52], the simple theory presented here provides a means for qualitatively accurate descriptions of drop interactions at comparatively minuscule computational cost.

While the theory was able to capture the qualitative behavior of drops, our methods can be improved and more accurate prediction of drop interactions can be made. Experimentally, we were unable to fully control for migration of the drops or be sure of no errant charges. In order to mitigate these issues, the needles and oil in the cell were grounded before the experiment and when the drops were inserted and moved, however this was not enough to fully eliminate these effects. It has been suggested that the migration of leaky dielectric drops in a steady field could be electrophoretic in nature [56], and thus could be avoided using an AC field. In terms of the model, we introduce inaccuracy by considering non-deforming drops and ignoring the possibility for charge convection, which we know is relevant at the field strengths used in this study. Additionally, emulsion surfaces are rarely clean, and the presence of surface active species can impact the EHD deformation and interactions of drops [57–59]. Nonetheless, in predicting the interactions of drops in various scenarios using a simple asymptotic theory, a considerable step is taken toward modeling more complex many-body systems. Analogies to our methodology exist in electrocoalescence [36], electrorheology [53], active matter [46, 55], and electrokinetics [54], where many-body simulations show a rich depth of behavior not yet quantified for leaky dielectric materials.

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