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# Estimating higher-order structure functions from geophysical turbulence time series: Confronting the curse of the limited sample size

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# Estimating Higher-Order Structure Functions from Geophysical Turbulence Time-Series: Confronting the Curse of the Limited Sample Size

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Utilizing synthetically-generated random variates and laboratory measurements, we document the inherent limitations of the conventional structure function approach in limited sample size settings. We demonstrate that an alternative approach, based on the principle of maximum likelihood, can provide nearly unbiased structure function estimates with far less uncertainty under such unfavorable conditions. The superiority of this approach over the conventional approach does not diminish even in the case of strongly correlated samples. Two entirely different types of probability distributions, which have been reported in the turbulence literature, are found to be compatible with the proposed approach.

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## I. INTRODUCTION

Characterization of small-scale turbulence by higher-order statistical moments has a long and rich history in both laboratory and geophysical settings. Dating back nearly half-a-century, Van Atta and Chen [1] conducted an extensive atmospheric boundary layer (ABL) experiment to measure up to fourth-order moments of atmospheric velocity fluctuations over the ocean. Their study revealed some intriguing similarities, and differences, between what was observed and the existing turbulence hypotheses (e.g., Kolmogorov/Obukhov 1941 - KO41, [2, 3]). These findings led to increased efforts ([4–10], just to name a few) to acquire extensive measurements of ABL flows in order to further explore the statistical and dynamical features of turbulence (e.g., power-law scaling, nonlinearity in energy cascade). At the same time, researchers in a myriad of other geophysical disciplines, from oceanography (e.g., phytoplankton biomass distribution in turbulent coast waters [11, 12]) to magnetohydrodynamics (e.g., intermittency in solar wind fluctuations [13–17]), initiated their own investigations in this intriguing research arena. Due to the lack of modern instrumentation, the majority of the initial studies were conducted solely within the Eulerian framework (by invoking the so-called Taylor’s hypothesis). Fortunately, several recent contributions have attempted to fill the void in the Lagrangian framework [please refer to 18–21, and references therein].

Over the years, the utilization of higher-order statistics not only became common practice for (in)validating various hypotheses against experimental findings, but it also enabled the research community to gain a better understanding of different types of turbulent flows. For

example, many studies have been conducted which strive to make a distinction between active and passive scalars [22–24] as well as contrasting atmospheric convection [25, 26] from Rayleigh-Bénard convection [27–31]. For other illustrative examples, please refer to the outstanding books by Frisch [32] and Tsinober [33].

In parallel to the analysis and characterization studies, a handful of pioneering works focused on the development of cascade models with the inherent ability to capture the observed higher-order scaling behaviors. These models ranged from a simplistic  $\beta$ -model which seeks to resemble the intermittent behavior of turbulent cascade from a geometric point-of-view [34, 35] to a more complex probabilistic model, which describes the energy cascade (multiplicative) process within the inertial-range in a multifractal framework [36–38]. Likewise, a number of other simplified dynamical models (e.g., shell models, stochastic Burgers equation) [39–43] were developed to mimic a number of intrinsic traits of three-dimensional turbulence. From our perspective, this line of research is still far from being matured.

It is important to acknowledge that the aforementioned higher-order characterization and related modeling activities are not only of importance from a pedagogical point-of-view, but they are also beginning to make impacts in diverse practical applications, including (but not limited to): combustion [44, 45]; wind energy [46], and atmospheric modeling [47]. We strongly believe that the gamut of applications can be significantly broadened with further analyses of various geophysical datasets. Unfortunately, the typical sample size of such datasets is orders of magnitude fewer than their laboratory counterparts. This disparity in sample size poses a serious challenge for higher-order statistical analyses using the traditional sample moments. In this paper, we advocate an alternative approach to confront this challenge.

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## II. LIMITED SAMPLE SIZE PROBLEM

It is common knowledge in the turbulence research community that capturing higher-order moments of turbulent variables can be rather difficult without a substantial sample size of experimental data [8, 32, 48–55]. In particular, the ability to accurately estimate the moments can be directly related to the tails of the underlying probability density function (pdf), which signify rare events [56].

Thus, in laboratory settings, it is customary to measure turbulence with upwards of  $10^7$  samples using hot-wire anemometry (sampling rate on the order of several kHz). However, acquisition of hot-wire data in a natural geophysical setting is quite challenging. For example, in the case of ABL field experiments, one needs to perform meticulous hot-wire calibration at short regular intervals in order to account for the ever-changing, diurnally varying ABL flow parameters [57, 58]. As a viable alternative, the ABL community widely uses sonic anemometers (sampling rate of  $\sim 20$  Hz) for measuring turbulent velocity fields. In contrast to hot-wires, these sensors require much less periodic calibration and maintenance. However, these instruments can only collect  $O(20\text{--}40)$  thousand samples during a measurement time window of 15–30 min. Publications, from as early as the 1970s, pointed out that such short time-series are not adequate for estimating moments beyond fourth-order [1, 8]. Unfortunately, one cannot circumvent this problem by simply using longer time-records owing to the frequent interference of non-stationary and non-turbulent motions (aka mesoscale motions). An earlier work attempted to tackle this problem using cumulants [59]. It was demonstrated that a cumulant-based approach can reliably estimate the so-called intermittency exponent [32] from short ABL time-series. However, the cumulants involve logarithmic functions of the velocity increments; as such, they are more influenced by the peak of the pdf rather than its tails. Thus, their usage in the estimation of higher-order moments is questionable. As an alternative, in this paper, we illustrate a maximum likelihood-based moment estimation technique which can provide statistically accurate higher-order moments from relatively short geophysical series.

## III. QUANTIFYING UNCERTAINTY IN STRUCTURE FUNCTION ESTIMATES

It is customary to quantify the behavior of fine-scale fully developed turbulence, using structure function (SF) analysis:

$$S_p = \langle |u(x+r) - u(r)|^p \rangle = \langle |\delta u|^p \rangle \sim r^{\zeta_p} \quad (1)$$

where  $S_p$  is the  $p^{\text{th}}$ -order SF with respect to the spatial separation (or increment),  $r$ . The angular brackets here indicate spatial averaging;  $|\delta u|^p$  is the  $p^{\text{th}}$  order absolute

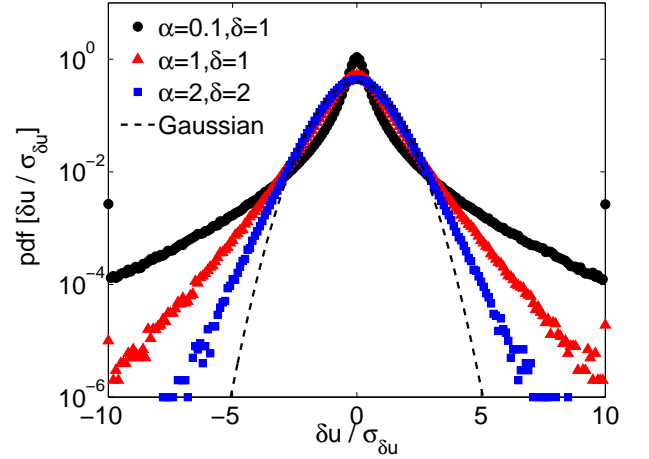


FIG. 1. NIG distributed variates with three different parameter combinations: (a)  $\alpha = 0.1, \delta = 1$ , (b)  $\alpha = 1, \delta = 1$ , and (c)  $\alpha = 2, \delta = 2$ . For all these cases, the parameters  $\mu$  and  $\beta$  are assumed to be equal to zero. Please refer to Appendix A for a detailed description of the NIG parameters. For each case,  $10^7$  samples were generated using Rydberg’s algorithm [60]. The distributions were normalized by the standard deviation  $\sigma_{\delta u}$ . A Gaussian pdf is overlaid (dashed line) as a reference.

moment of the velocity increments; and  $\zeta_p$  is the scaling exponent.

Many laboratory and geophysical turbulence studies have shown that the pdfs of velocity increments,  $\text{pdf}[\delta u]$ , are scale-dependent and change steadily within the inertial sub-range. Specifically, these distributions have shown to exhibit strong non-Gaussian behavior at small increments, then become more Gaussian as separation increases [15, 56, 61–65]. A few years ago, Barndorff-Nielsen et al. [56] demonstrated that the normal inverse Gaussian (NIG) distribution has the inherent ability to capture such scale-dependent traits in a parsimonious manner. An illustrative example is shown in Fig. 1. Here, following the approach by Rydberg [60], we have numerically generated three NIG distributed variates with different parameter settings. This figure clearly attests to the fact that the NIG distribution can indeed capture heavy-tailed ( $\bullet$ ), moderate-tailed ( $\blacktriangle$ ), and near-Gaussian ( $\blacksquare$ ) distributions with appropriate choice of parameters. More details regarding the NIG distribution are provided in Appendix A.

Next, using the NIG distributed variates, we quantify the impacts of pdf shapes and sample sizes on the uncertainty of the SF estimates. We consider a wide range of sample sizes ( $N$ ) from  $10^3$  to  $10^7$  for each of the three pdfs shown in Fig. 1. In order to obtain reliable statistics, we generate one hundred realizations for each case. Based on the numerically generated variates, we compute SF using Eq. (1). Without loss of generality, we focus on the 6<sup>th</sup>-order SF ( $S_6$ ).

The decision to consider  $S_6$  as a test statistic was not arbitrary. In turbulence literature, there is considerable

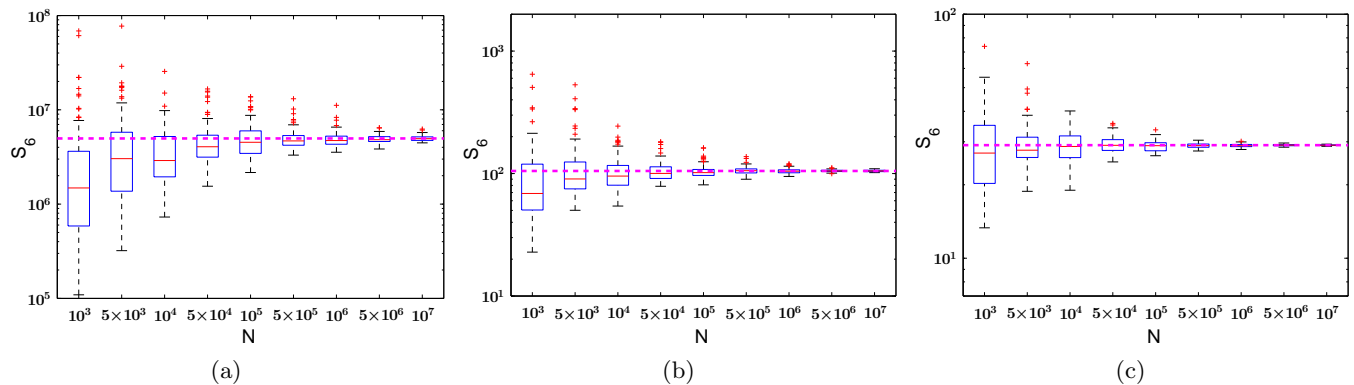


FIG. 2. “Empirical”  $S_6$  box-plots for three different NIG distributions with parameter combinations: (a)  $\alpha = 0.1, \delta = 1$ , (b)  $\alpha = 1, \delta = 1$ , and (c)  $\alpha = 2, \delta = 2$ . The parameters  $\mu$  and  $\beta$  are assumed to be equal to zero. The sample sizes ( $N$ ) are varied from  $10^3$  to  $10^7$ . One hundred realizations are used for the construction of the box-plots. The dashed magenta lines represent the true  $S_6$  values based on Eq. (A4).

interest in the accurate estimation of  $S_6$ , since its scaling exponent is directly used to determine the intermittency exponent,  $\mu^* \equiv 2 - \zeta_6$ , which relates to the behavior of the underlying non-Gaussian distributions.

The estimated (henceforth “empirical”)  $S_6$  values are shown in Fig. 2 utilizing a standard box-plot notation where 50 percent of the data lie within the blue “box” and the red line segment within the “box” is the median value of the data. The “whiskers” (i.e., the vertical dashed line segments) correspond to  $\pm 2.7\sigma$ , while the  $+$  are the outliers. The following observations can be made based on this figure:

- For all the cases, with increasing sample size the  $S_6$  estimates converge towards the true values as would be expected.
- For comparable sample size, the uncertainty of the  $S_6$  estimate is much higher for the heavy-tailed case than the near-Gaussian case; the moderate-tailed case falls in between.
- For small sizes, the  $S_6$  estimates are strongly biased for the heavy-tailed case. The bias decreases for the moderately-tailed case; while for the near-Gaussian case, the estimates are close to unbiased.

These findings have significant implication on geophysical data analyses and require scrutiny in to whether a collection of samples are robust enough to provide an accurate estimation of a specific higher-order moment. In a recent paper, Dudok de Wit [66] made an interesting contribution in this arena by borrowing ideas from the Extreme Value (EV) theory. He proposed a simple approach to compute the maximum moment order ( $p_{max}$ ) for which reliable estimation of structure function ( $S_{p_{max}}$ ) is feasible for a given spatial/time series. In the following section, using the aforementioned NIG distributed variates, we elaborate on Dudok de Wit’s approach followed by a recommendation for certain improvement.

#### IV. ESTIMATING $p_{max}$ FROM LIMITED DATA

Let us denote the rank-ordered (in decreasing order) absolute value of the velocity increments as:  $\Phi_k = |\delta u|_k$ , where  $k = 1, \dots, N$ . Dudok de Wit [66] showed that for small values of  $k$ ,  $\Phi_k$  versus  $k$  follows the well-known Zipf power-law behavior:

$$\Phi_k \propto \left(\frac{k}{N}\right)^{-\gamma^*} \quad (2)$$

where,  $\gamma^*$  is known as the tail index (aka shape parameter). Via analytical derivations (with one minor approximation), Dudok de Wit [66] related  $\gamma^*$  to  $p_{max}$  as follows:

$$p_{max} = \left\lfloor \frac{1}{\gamma^*} \right\rfloor - 1 \quad (3)$$

where the floor bracket denotes the integer part.

In Fig. 3, the rank-ordered plots for three NIG distributed variates are shown. In these log-log plots, the power-law behavior is clearly discernible for small values of  $k$ . Following Dudok de Wit’s approach,  $\gamma^*$  values are estimated using ordinary linear regression over the range of  $10 \leq k \leq 1000$ . These values along with the estimated  $p_{max}$  values are reported in Table I.

As shown in [66], and illustrated here in Table I, there is a clear dependence on  $p_{max}$  values for the various sample sizes. Additionally, we also notice that the shape of the pdfs directly influences  $p_{max}$ . For instance, in the case of the heavy-tailed distribution ( $\alpha = 0.1$  and  $\delta = 1$ ), a minimum sample size of  $10^7$  is required in order to provide a reliable estimate of  $S_6$ . However, for a near-Gaussian distribution ( $\alpha = 2$  and  $\delta = 2$ ), only  $10^5$  samples will suffice. We would like to note that these results are in complete agreement with the ones reported earlier in Fig. 2.

Even though the overall approach of Dudok de Wit [66] is quite elegant and powerful, the tail index estimation

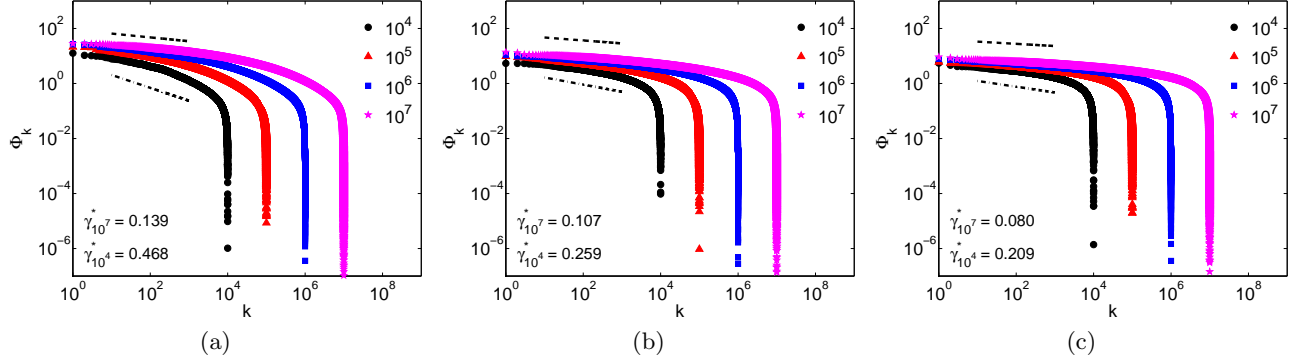


FIG. 3. Rank-order (aka Zipf) plots for NIG distributed variates with three different parameter combinations: (a)  $\alpha = 0.1, \delta = 1$ , (b)  $\alpha = 1, \delta = 1$ , and (c)  $\alpha = 2, \delta = 2$ . The parameters  $\mu$  and  $\beta$  are assumed to be equal to zero. The sample sizes ( $N$ ) are varied from  $10^4$  to  $10^7$ . The tail-indices ( $\gamma^*$ ) are estimated for  $N = 10^4$  (dot-dashed) and  $N = 10^7$  (dashed) and reported in the bottom-left corner of the plots.

component is rather subjective and not statistically robust. It can be significantly improved by employing one of the well-tested estimators from the field of EV theory [67] instead of using linear regression. Over the years, several estimators for  $\gamma^*$  have been proposed in the literature, including (but not limited to): Pickands estimator [68], Hill estimator [69], and the Dekkers-Einmahl-de Haan estimator [70]. In this work, we use the popular Hill estimator:

$$\gamma^* = \left( \frac{1}{k} \sum_{i=1}^k \log \left( \frac{\Phi_i}{\Phi_{k+1}} \right) \right)^{-1} \quad (4)$$

where  $k = 1, \dots, N - 1$ . It is customary to estimate  $\gamma^*$  value through a graphical representation called a Hill plot. This type of depiction is formed by plotting  $\gamma^*$  versus  $k$  [71]. For EV distributions (e.g., Pareto), estimated  $\gamma^*$  (or, related  $p_{max}$  via Eq. (3)) are expected to stabilize (i.e., exhibit non-fluctuating behavior) with increasing values of  $k$ .

To illustrate this technique, we present, in Fig. 4, Hill plots using the same three NIG distributed variates and range of sample sizes as in Fig. 3. Even though it captures heavy tails [72], NIG distribution is not formally an

EV distribution. Thus, perfect stabilization of the Hill plots are not anticipated. Nonetheless, Fig. 4(a), shows that all four curves smoothly and slowly decrease below the dashed line, representing  $p_{max} = 6$ . This behavior indicates that, for this particular heavy-tailed distribution, even with  $10^7$  samples we cannot provide an accurate estimation of  $S_6$ . However, as the pdf shapes are modified and tend to become more Gaussian, the Hill plots [Figs. 4(b) and 4(c)] reveal that higher order moments are achievable for smaller sample sizes. Another important feature that Fig. 4 portrays is that 6<sup>th</sup>-order moment estimations pose issues with sample size less than  $10^5$  irrespective of the shape of the distribution. In fact, this characteristic can also be seen through the “empirical” 6<sup>th</sup>-order SF calculations displayed in Fig. 2.

In summary, the approach proposed by Dudok de Wit [66] and our suggested modification provide guidelines into the  $p_{max}$  values attainable by the conventional structure function analysis. In the next section, we advocate an alternative approach, based on maximum likelihood estimation (MLE), which has the ability to reliably compute structure functions well beyond  $p_{max}$ . However, to employ such an approach, one needs to make an assumption about the underlying pdf of the velocity increments. In the present work, we assume it to be following the NIG distribution [56].

## V. MAXIMUM LIKELIHOOD-BASED STRUCTURE FUNCTION ESTIMATION

If the velocity increments follow the NIG distribution, the structure functions can be re-written as:

$$S_p = E(|x^p|) = \int_{-\infty}^{\infty} |x|^p f_{NIG}(x; \alpha, \beta, \mu, \delta) dx \quad (5)$$

In this case,  $x$  equals  $\delta u$ . If the parameters of the NIG distribution are known (or estimated), one can simply use a numerical integration approach to compute the integral.

TABLE I. Tail-index ( $\gamma^*$ ) and maximum moment order ( $p_{max}$ ) for NIG distributed variates of varying sample sizes and with three different parameter combinations.

	$\alpha = 0.1, \delta = 1$		$\alpha = 1, \delta = 1$		$\alpha = 2, \delta = 2$	
$N$	$\gamma^*$	$p_{max}$	$\gamma^*$	$p_{max}$	$\gamma^*$	$p_{max}$
$5 \times 10^3$	0.583	0	0.346	1	0.265	2
$1 \times 10^4$	0.468	1	0.259	2	0.209	3
$5 \times 10^4$	0.344	1	0.206	3	0.157	5
$1 \times 10^5$	0.294	2	0.185	4	0.140	6
$5 \times 10^5$	0.213	3	0.146	5	0.117	7
$1 \times 10^6$	0.204	3	0.130	6	0.109	8
$5 \times 10^6$	0.155	5	0.109	8	0.088	10
$1 \times 10^7$	0.139	6	0.107	8	0.080	11



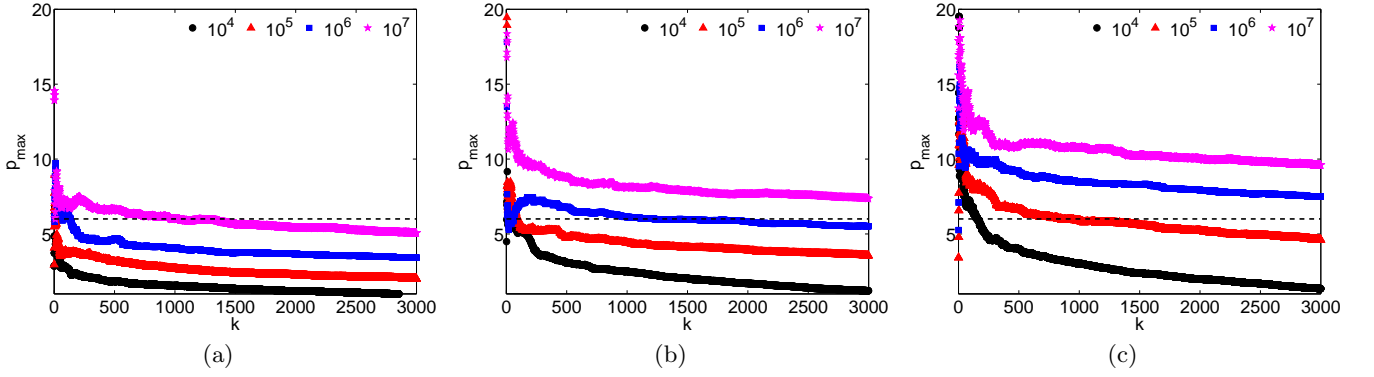


FIG. 4. Hill plots for NIG distributed variates with three different parameter combinations: (a)  $\alpha = 0.1, \delta = 1$ , (b)  $\alpha = 1, \delta = 1$ , and (c)  $\alpha = 2, \delta = 2$ . The parameters  $\mu$  and  $\beta$  are assumed to be equal to zero. The sample sizes ( $N$ ) are varied from  $10^4$  to  $10^7$ . The dashed black lines represent  $p_{max} = 6$ .

However, in a typical laboratory/geophysical setting, these NIG parameters are not known *a priori*. One can then use the method of moments approach (see Appendix A) to estimate them; but this technique has been shown to be unstable [73]. A more robust approach would be to use the maximum likelihood estimator (MLE; [74, 75]), for details see Appendix B. Since, MLE is a computationally very expensive technique and occasionally requires numerous iterations for convergence, in this work, we make use of the MME-based estimates as the initial conditions for the MLE computations.

In order to illustrate the superiority of MLE over MME, we make use of the Kolmogorov-Smirnov (K-S) statistic based on the empirical distribution function (EDF; [76]):

$$D = \sup_x |F_{EMP}(x) - F_{NIG}(x)| \quad (6)$$

where  $F_{EMP}$  and  $F_{NIG}$  are the empirical and estimated NIG distribution functions, respectively. The results associated with a heavy-tail distribution ( $\alpha = 0.1, \delta = 1$ ) are shown in Fig. 5. Without any doubt, for all sample sizes, MLE outperforms MME by having (i) lower (median) values of  $D$  and (ii) reduced uncertainty bounds of  $D$ . Similar comparative results were obtained for moderate-tail and near-Gaussian pdfs as well (not shown here for brevity).

Within the MLE computation, we explored two types of numerical algorithms: Expectation-Maximization (E-M) [77] and Nelder-Mead method [78]. Both these approaches produced near-identical results (up to the fourth decimal points). Our implementation of the E-M algorithm follows [74]. We chose this specific approach due to its simplicity and robustness for the NIG distribution. A pseudo-code is included in Appendix B. For the Nelder-Mead method, we used a commercial MLE function from MATLAB<sup>TM</sup>. Further details regarding this approach can be found in [79].

Using the idealized NIG distributed variates generated in Fig. 2, we now apply the MLE approach to find out if an improvement over the conventional approach is feasi-

ble. The MLE-based  $S_6$  estimates are displayed in Fig. 6 using the standard box-plot notation as before. Of note, the sample size range is reduced from  $10^7$  in Fig. 2 to  $10^6$  in Fig. 6 since MLE provides converged statistics with far less data samples.

There are distinct differences in results between Fig. 2 and Fig. 6. First of all, for all sample sizes and pdf shapes, the estimated  $S_6$  values are nearly unbiased in Fig. 6. Second, the uncertainty bounds are significantly reduced in Fig. 6 in comparison to the corresponding box-plots in Fig. 2. In other words, the MLE-based structure function approach is much more robust and more reliable in comparison to the conventional structure function approach, especially in a small sample setting.

In the following section, we will investigate if this conclusion also holds in the case of correlated and real-data samples.

## VI. EFFECTS OF CORRELATION

To this point, our analysis has been focused on independent and identically distributed (i.i.d) random NIG variates. However, in practice, the samples may be correlated. For example, in the case of velocity increments, Anselmet et al. [49] and Huang et al. [80] reported scale-dependent temporal correlations. In order to quantify the impact of correlation on higher-order moment estimation, we synthetically generated one hundred realizations of correlated NIG variates. Each realization is created via the following steps:

1. As before, generate i.i.d NIG variates (sample size of one million) using the approach by Rydberg [60]. We assumed a moderate-tailed distribution ( $\alpha=1, \beta=0, \mu=0$ , and  $\delta=1$ ).
2. Generate a red-noise series (sample size of one million) with a spectral slope between zero and minus 1. The magnitude of this slope is randomly selected from a uniform distribution.

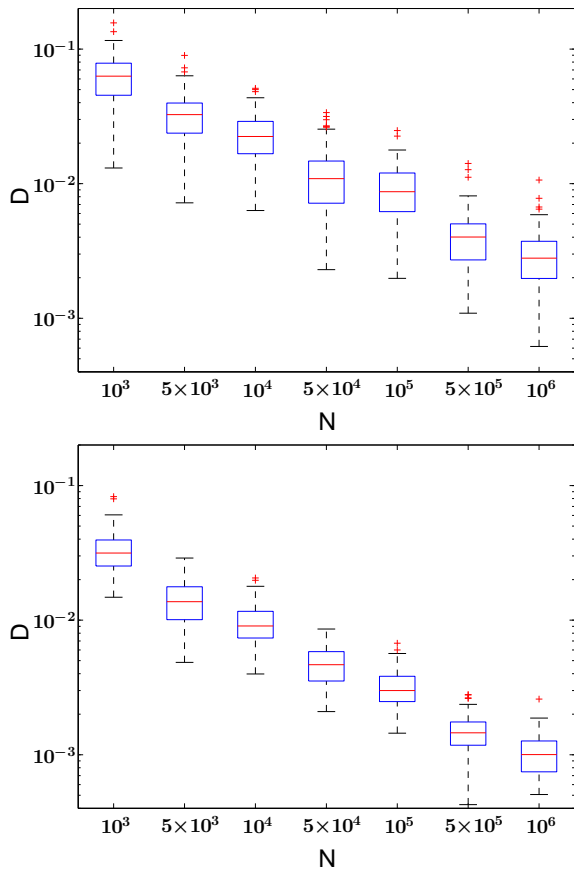


FIG. 5. Box-plots of K-S test statistic ( $D$ ) comparing MME (top panel) versus MLE (bottom panel) results. The following parameters are utilized to generate the random variates:  $\alpha = 0.1$ ,  $\beta = 0$ ,  $\mu = 0$ , and  $\delta = 1$  (heavy-tailed). The sample sizes ( $N$ ) are varied from  $10^3$  to  $10^6$ . As before, one hundred realizations are used for the construction of the box-plots.

3. Perform simple histogram matching between the i.i.d NIG series and the red-noise series. The resultant series preserves the NIG pdf accurately and it is correlated. Albeit, it does not follow the exact correlation structure of the red-noise.

Illustrative examples of i.i.d and correlated NIG variates are shown in Fig. 7. Even though they look distinctly different (due to correlation structure), both realizations follow an identical pdf.

Let us denote each of the one hundred correlated NIG realizations as:  $\delta u_1^{(k)}, \dots, \delta u_M^{(k)}$ ; where  $M = 10^6$  and  $k$  varies from 1 to 100. From each realization, we extract a contiguous subset  $\delta u_i^{(k)}, \dots, \delta u_{i+N-1}^{(k)}$ ; where  $i \geq 1$  and  $i + N - 1 \leq M$ . We vary the subsample size  $N$  from  $10^3$  to  $10^6$ . Since we have a total of one hundred realizations, for a specific value of  $N$ , we also get one hundred subsamples. These subsamples are used to estimate  $S_6$  using the aforementioned “empirical” and MLE approaches. These results are shown in Fig. 8.

Comparing the results from Fig. 8 to the corresponding box-plots in Fig. 2, it is clear that the uncertainty bounds

have significantly increased for the correlated samples. Also, the number of outliers have increased substantially. Still, for this difficult scenario, the MLE-based estimates outperforms the “empirical” ones in terms of bias and uncertainty bounds. It is quite remarkable that for all sample sizes, the MLE-based estimates are unbiased. It is needless to say that both the estimates do converge to the true  $S_6$  value for large sample sizes; albeit, the convergence is slower than the i.i.d scenario.

## VII. WIND TUNNEL DATA

To further showcase the strength of the MLE approach, we utilize laboratory data from the Office National d’Etudes et de Recherches Aéronautiques (ONERA) S1 wind tunnel. These velocity measurements were obtained with a DISA 55M01 constant temperature system with Wollaston wire (3 mm diameter and 0.35 mm length for all the air flows). The sample size for this data is approximately ( $\sim 13 \times 10^6$ ) long with a sampling rate of 25 kHz. Following the conventional turbulence analysis techniques, we have invoked Taylor’s hypothesis to convert this time series to a spatial series and normalized the original series to have zero mean and unit standard deviation. For further details on this dataset and past ONERA S1 wind tunnel experiments, please refer to [81–83].

Figs. 9a and 10a depict pdfs of velocity increments for two specific  $\Delta t$  values:  $4 \times 10^{-4}$  sec and  $1.35 \times 10^{-2}$  sec, respectively. Given their distinctly different tail behavior, we utilize them to evaluate the strengths (weaknesses) of the proposed MLE-based structure function estimation approach. As before, we randomly selected one hundred subsets of varying sample sizes for both empirical and MLE-based moment estimations. We consider the  $S_6$  values based on Eq. (1) using the entire dataset as the “truth”.

For small sample sizes, the conventional estimates are quite uncertain (middle panels of Figs. 9 and 10). In addition, for such cases, the median  $S_6$  estimates are significantly outside the  $\pm 10$  percent uncertainty bound. In contrast, the MLE-based estimates offer low uncertainty for all sample sizes (right panels of Figs. 9 and 10). For the large  $\Delta t$  case, the MLE-based median estimates are almost identical to the “true” value for all sample sizes. The performance is somewhat poorer for small  $\Delta t$ . In this case, the MLE-based median values are approximately  $\pm 10$  percent lower than the “truth” for all sample sizes. For small sample sizes ( $N \leq 10^4$ ), the MLE-based approach unequivocally outperforms the conventional approach. Based on these results, we strongly recommend the geophysical community to utilize the proposed MLE-based approach for analyzing datasets with limited sample size.

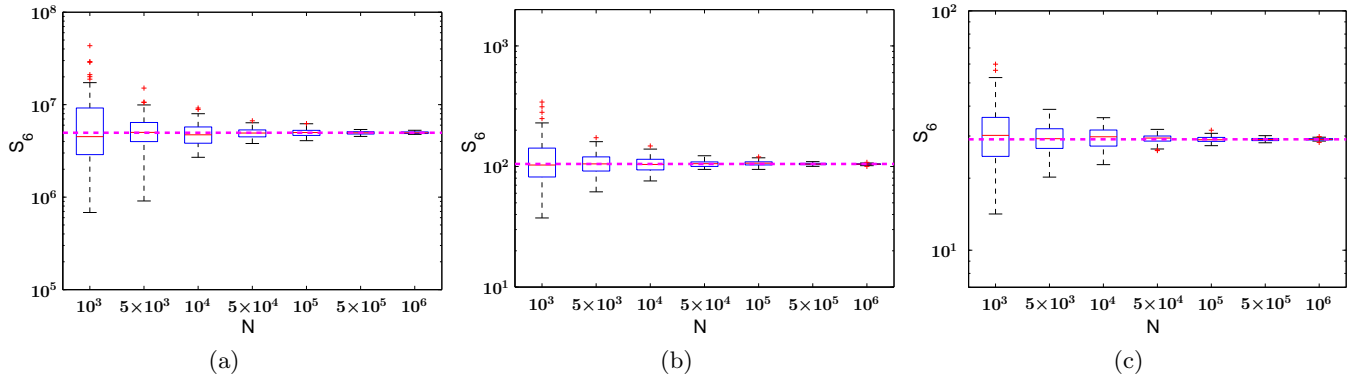


FIG. 6. MLE-based  $S_6$  box-plots for three NIG distributions with parameter combinations: (a)  $\alpha = 0.1, \delta = 1$ , (b)  $\alpha = 1, \delta = 1$ , and (c)  $\alpha = 2, \delta = 2$ . The parameters  $\mu$  and  $\beta$  are assumed to be equal to zero. The sample sizes ( $N$ ) are varied from  $10^3$  to  $10^6$ . One hundred realizations are used for the construction of the box-plots. The dashed magenta lines represent the true  $S_6$  values based on Eq. (A4).

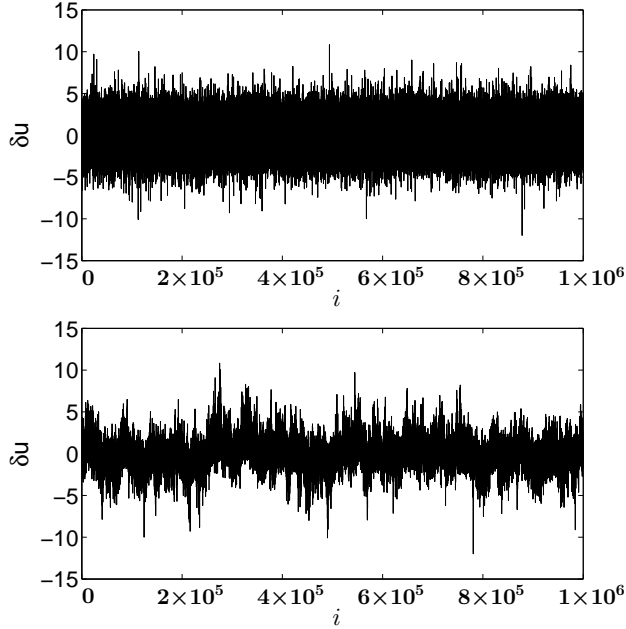


FIG. 7. Realizations of i.i.d (top panel) and correlated (bottom panel) NIG variates. Both the realizations follow the same NIG distribution with prescribed parameters:  $\alpha=1, \beta=0, \mu=0$ , and  $\delta=1$ .

### VIII. ALTERNATIVE PDF

Throughout this paper, we have demonstrated the strengths of the MLE-based approach to estimate higher-order moments. For this purpose, we needed to make an assumption about the underlying pdf of increments. Given its versatility in capturing pdfs of different shapes and forms [84], we opted to use the NIG pdf.

We acknowledge that the NIG pdf has not been fully vetted by the turbulence research community at large. Thus, its appropriateness to represent velocity and/or scalar increments for diverse types of flows remains to be

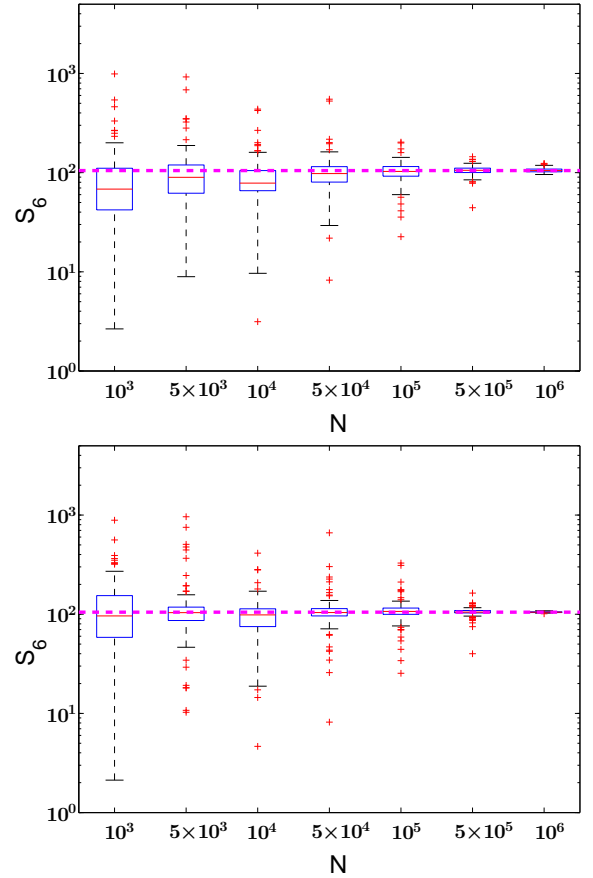


FIG. 8. “Empirical” (top panel) and MLE-based (bottom panel)  $S_6$  box-plots for correlated NIG variates. The following parameters are utilized to generate the random variates:  $\alpha = 1, \beta = 0, \mu = 0$ , and  $\delta = 1$ . The sample sizes ( $N$ ) are varied from  $10^3$  to  $10^6$ . One hundred realizations are used for the construction of the box-plots. The dashed magenta lines represent the true  $S_6$  value based on Eq. (A4).



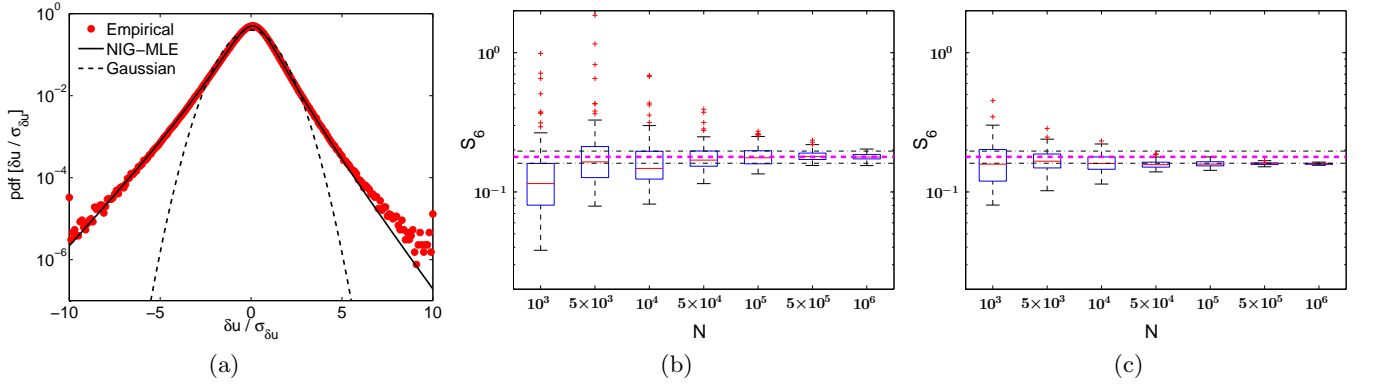


FIG. 9. Analyses of ONERA S1 wind tunnel data. Selected increment:  $r = 8.2$  mm or  $\Delta t = 4 \times 10^{-4}$  sec, a) corresponding PDF with NIG-MLE fit, b) “Empirical”  $S_6$  box-plots, c) NIG-MLE  $S_6$  box-plots. One hundred realizations are used for the construction of the box-plots. The dashed magenta line represent the  $S_6$  values based on Eq. (1) using the entire dataset. The dot-dashed lines represent an uncertainty of  $\pm 10\%$  around the magenta line.

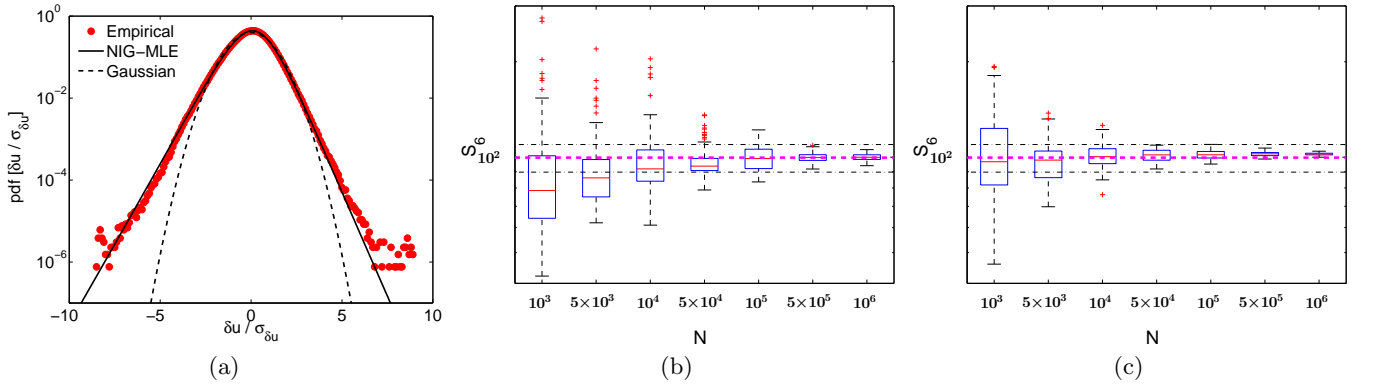


FIG. 10. Same as Fig. 9, except for  $r = 277.8$  mm or  $\Delta t = 1.35 \times 10^{-2}$  sec.

confirmed. In the recent past, other types of pdfs have been proposed (e.g., [85–87]) and some of them have already gained popularity. In this section, we would like to find out if our MLE-based moment estimation approach can be utilized in conjunction with another type of pdf.

In this proof-of-concept exercise, we choose to use the log-normal superstatistics (LNSS) pdf [64, 87, 88] given its strikingly different form compared to the NIG pdf (please refer to Appendix C). First, we generate i.i.d. NIG variates ( $\alpha = 1$ ,  $\beta = 0$ ,  $\mu = 0$ ,  $\delta = 1$ ) of different sample sizes. We then estimate  $S_6$  by utilizing the MLE approach. However, unlike before, we make an (incorrect) assumption that the underlying distribution is governed by the LNSS pdf. The results are shown in Fig. 11. The top-panel plot shows that the difference between the NIG and LNSS pdfs are remarkably small (except near the tails). Visually (without using any metrics), both the pdfs appear to be equally representative of the generated random variates. To magnify the tail estimation, the middle panel shows the pdf multiplied by  $\delta u^6$ , which highlights the differences in two estimations. More surprisingly, the LNSS-MLE approach overestimates the true  $S_6$  value only by a small margin (see bottom panel of Fig. 11). Undoubtedly, the most impor-

tant finding is that the estimation bias remains independent of sample size. This result re-confirms the strength of the proposed MLE approach for small sample setting.

## IX. CONCLUDING REMARKS

Maximum likelihood estimation (MLE) is an age-old technique and is utilized in countless disciplines. For reasons unknown, the turbulence community has not leveraged on this statistically robust approach for the estimation of higher-order structure functions. In this work, we demonstrate that unbiased estimation of 6<sup>th</sup>-order structure function with relatively small samples (less than  $10^5$ ) is feasible with MLE; whereas, the conventional approach fails under these circumstances. Moreover, the unbiasedness of the MLE approach is not affected by correlation within the samples. Last, this approach performs remarkably well for two entirely different types of pdfs: normal inverse Gaussian and log-normal superstatistics. In our future work, we will continue to investigate the prowess of the MLE-based higher-order moment estimation approach by systematically us-

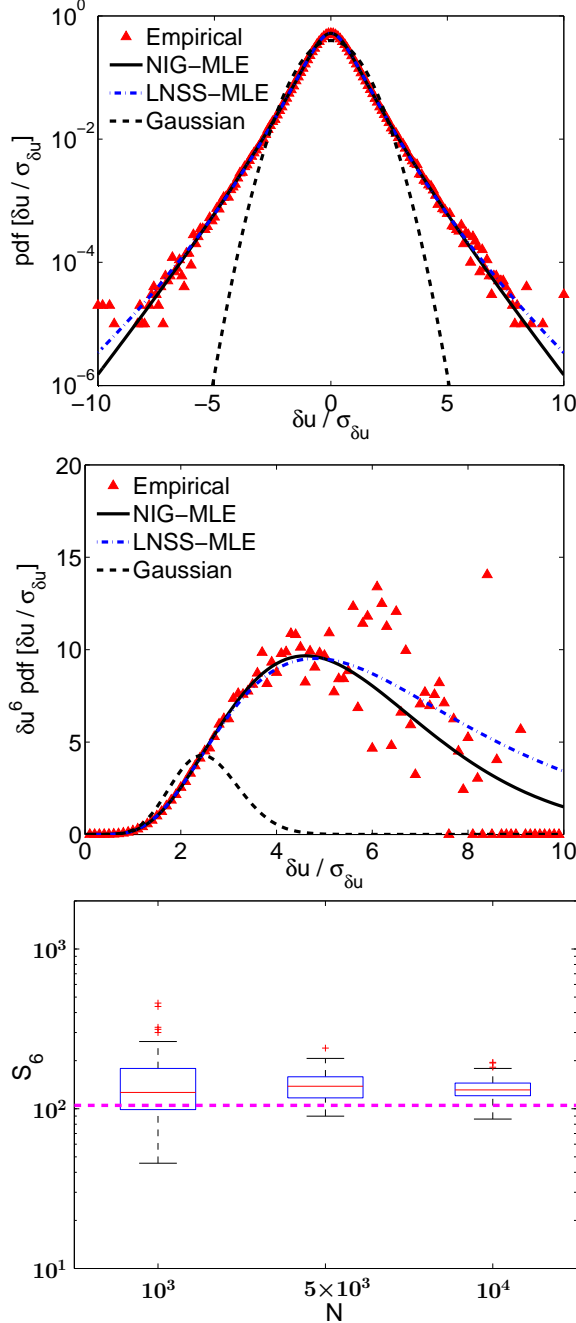


FIG. 11. Top panel: comparison of fitted NIG and LNSS pdfs for i.i.d. NIG variates. The sample size is  $10^6$ . Middle panel: magnifies the right-tail estimation by multiplying the pdf by  $\delta u^6$ . Bottom panel: MLE-based  $S_6$  box-plot for i.i.d. NIG variates with the (incorrect) assumption of LNSS as the underlying pdf. Due to high computational costs associated with numerical integration of the LNSS pdf, the sample sizes ( $N$ ) are only limited to  $10^4$  in this example. The following parameters are utilized to generate the random variates:  $\alpha = 1$ ,  $\beta = 0$ ,  $\mu = 0$ , and  $\delta = 1$ . One hundred realizations are used for the construction of the box-plot. The dashed magenta line represents the true  $S_6$  value based on Eq. (A4).

ing other observed datasets from turbulence to larger-scales motions. Additionally, we will inter-compare various potential pdf candidates using rigorous metrics (e.g., Kolmogorov-Smirnov and Anderson-Darling).

### Appendix A: Normal Inverse Gaussian Distribution

The one-dimensional normal inverse Gaussian (NIG) pdf contains four-parameters ( $\alpha$ ,  $\beta$ ,  $\delta$ , and  $\mu$ ) and is defined as follows [89–91]:

$$f_{NIG}(x; \alpha, \beta, \mu, \delta) = \frac{\alpha}{\pi} \exp\left(\delta\sqrt{\alpha^2 - \beta^2} - \beta\mu\right) \frac{1}{\sqrt{\phi(x)}} \times \exp(\beta x) K_1\left(\delta\alpha\sqrt{\phi(x)}\right) \quad (\text{A1})$$

where

$$\phi(x) = 1 + \left[\frac{x - \mu}{\delta}\right]^2 \quad (\text{A2})$$

The parameter  $\alpha$  controls the steepness of the pdf, where a small  $\alpha$  signifies a heavy tail.  $\beta$  is the skewness parameter, such that a negative  $\beta$  indicates that the pdf is skewed to the left.  $\mu$  is the centrality or translation parameter and is slightly different from the arithmetic mean of the distribution.  $\delta$  is a scale or peakedness parameter and it controls the shape of the pdf near its mode.  $\alpha$  and  $\delta$  are always positive and  $K_1$  is the modified Bessel function of third kind of order one [92].

The parameters of the NIG distribution are explicitly related to the first four central moments [56, 74]. Let us denote the sample mean, standard deviation, skewness, and kurtosis by  $m_1$ ,  $m_2$ ,  $m_3$ , and  $m_4$ , respectively. Further define:  $\gamma = \frac{3}{m_2\sqrt{(3m_4 - 5m_3^2)}}$ . Subsequently, the pdf parameters can be estimated, via the method of moments approach, as follows [74]:

$$\alpha = \sqrt{\beta^2 + \gamma^2}; \quad (\text{A3a})$$

$$\beta = \frac{(m_2 m_3 \gamma^2)}{3}; \quad (\text{A3b})$$

$$\delta = \frac{m_2^2 \gamma^3}{\beta^2 + \gamma^2}; \quad (\text{A3c})$$

$$\mu = m_1 - \frac{\beta\delta}{\gamma}. \quad (\text{A3d})$$

In this work, without loss of generality, we generated NIG distributed variates with  $\mu = 0$  and  $\beta = 0$ . This choice was made so that Eq. (5) becomes analytically tractable [93] and reduces to:

$$S_p = E(|x|^p) = \frac{2^{\frac{p+1}{2}} \delta^p}{\pi (\alpha\delta)^{\frac{p-1}{2}}} \exp(\alpha\delta) \Gamma\left(\frac{p+1}{2}\right) K_{\frac{p-1}{2}}(\alpha\delta) \quad (\text{A4})$$

For  $\alpha = 0.1$ ,  $\delta = 1$ , it is easy to show that  $S_6 = 4.965 \times 10^6$ . This true value is represented as dashed magenta lines in the left panels of Fig. 2 and Fig. 6. True  $S_6$  values using other parameter combinations are also shown in middle and right panels of Fig. 2 and Fig. 6.

## Appendix B: Maximum Likelihood Estimation

Maximum likelihood estimation (MLE) is a well-established statistical method to estimate the parameters of a given model (say NIG) which make the sample data,  $x_i = x_1, x_2, \dots, x_N$ , the most probable outcome. Let  $f(x|\theta)$  denote the underlying NIG pdf of the sample data with parameters  $\theta$  ( $\theta_1 = \alpha$ ,  $\theta_2 = \beta$ ,  $\theta_3 = \mu$ , and  $\theta_4 = \delta$ ). In the case of independent, identically distributed NIG variates,  $f(x|\theta)$  can then be expressed as a joint probability function:

$$f(x|\theta) = f_1(x_1|\theta)f_2(x_2|\theta)\dots f_N(x_N|\theta) \quad (B1)$$

However, in order to determine the model parameters based on observed data, we have to solve an inverse problem. The first step is to define a likelihood function, where the parameters are a function of the fixed data, as follows:

$$L(\theta|x) = f(x|\theta) \quad (B2)$$

In the case of the NIG pdf, this likelihood function is simply a four dimensional surface sitting above a four-dimensional hyperplane covering the NIG parameters. For computational ease, it is customary to maximize the log-likelihood (instead of  $L$ ) to obtain the MLE estimates. The log-likelihood function for the NIG pdf can be written as:

$$\ln(L(\theta|x)) = -N \ln(\pi) + N \ln(\alpha) + N(\delta\gamma - \beta\mu) - \frac{1}{2} \sum_{i=1}^N \ln(\phi(x_i)) + \beta \sum_{i=1}^N x_i + \sum_{i=1}^N \ln \left[ K_1(\delta\alpha\sqrt{\phi(x_i)}) \right]; \quad (B3)$$

where  $N$  is the sample size. Next, to find the parametric values which “maximizes” the log-likelihood function, we impose:

$$\frac{\partial \ln(L(\theta|x))}{\partial \theta_k} = 0 \quad (B4)$$

$$\frac{\partial^2 \ln(L(\theta|x))}{\partial \theta_k^2} < 0 \quad (B5)$$

where  $k$  varies from 1 to 4.

Karlis [74] developed an expectation-maximization algorithm 1 to easily maximize Eq. (B3). He leveraged on the fact that the partial derivative of  $\ln(L)$  with respect

to  $\beta$  leads to a simple relationship connecting the sample mean ( $\bar{x}$ ) and some of the NIG parameters:

$$\bar{x} = \mu + \frac{\delta\beta}{\gamma} \quad (B6)$$

He also derived the relationships between the conditional expectations of the inverse Gaussian (IG) distribution and NIG parameters (see [74] for details). A pseudo-code for his approach is provided below:

---

### ALGORITHM 1: Expectation-Maximization for NIG pdf

---

**Initialize:**

NIG parameters ( $\alpha^{(1)}$ ,  $\beta^{(1)}$ ,  $\mu^{(1)}$ ,  $\delta^{(1)}$ ) using the MME approach

**Compute:**

$\ln(L^{(1)})$  using Eq. (B3) and initialized parameters

**for**  $k = 1$  to  $k_{max}$  **do**

**Compute:**

**E-Step** - The conditional expectations,  $s_i$  and  $w_i$

$$s_i \leftarrow \frac{\delta^{(k)} \sqrt{\phi^{(k)}(x_i)} K_0(\delta^{(k)} \alpha^{(k)} \sqrt{\phi^{(k)}(x_i)})}{\alpha^{(k)} K_1(\delta^{(k)} \alpha^{(k)} \sqrt{\phi^{(k)}(x_i)})}$$

$$w_i \leftarrow \frac{\alpha^{(k)} K_{-2}(\delta^{(k)} \alpha^{(k)} \sqrt{\phi^{(k)}(x_i)})}{\delta^{(k)} \sqrt{\phi^{(k)}(x_i)} K_{-1}(\delta^{(k)} \alpha^{(k)} \sqrt{\phi^{(k)}(x_i)})}$$

**Compute:**

**M-Step** - Update the parameters using  $s_i$  and  $w_i$  from previous step

$$\bar{s} \leftarrow \sum_{i=1}^N \frac{s_i}{N}$$

$$\widehat{M} \leftarrow \bar{s}$$

$$\widehat{\Lambda} \leftarrow \frac{N}{\sum_{i=1}^N \left( w_i - \frac{1}{M} \right)}$$

$$\delta^{(k+1)} \leftarrow \sqrt{\widehat{\Lambda}}$$

$$\gamma^{(k+1)} \leftarrow \frac{\delta^{(k+1)}}{\widehat{M}}$$

$$\beta^{(k+1)} \leftarrow \frac{\sum_{i=1}^N x_i w_i - \bar{x} \sum_{i=1}^N w_i}{N - \bar{s} \sum_{i=1}^N w_i}$$

$$\mu^{(k+1)} \leftarrow \bar{x} - \beta^{(k+1)} \bar{s}$$

$$\alpha^{(k+1)} \leftarrow \sqrt{(\gamma^{(k+1)})^2 + (\beta^{(k+1)})^2}$$

$i = 1, \dots, N$

---

**Compute:**  
 $\ln(L^{(k+1)})$  using Eq. (B3) with updated  
parameters  
**if**  $\left| \frac{\ln(L^{(k+1)}) - \ln(L^{(k)})}{\ln(L^{(k)})} \right| < 10^{-10}$  **then**  
    **break**  
**end if**  
**end for**

---

### Appendix C: Log-Normal Superstatistics

The concept of superstatistics (aka “statistics of a statistics”) was proposed by Beck and Cohen 2003 [87]. The log-normal superstatistics (LNSS) pdf can be written as:

$$f_{LNSS}(x; \mu, s) = \frac{1}{2\pi s} \int_0^\infty b^{-1/2} \exp \left\{ \frac{-(\ln(b/\mu))^2}{2s^2} \right\} e^{-(1/2)bx^2} db. \quad (C1)$$

The non-central second-order moment and the flatness of this distribution can be written as follows [64]:

$$\langle x^2 \rangle = \sqrt{w}/\mu \quad (C2a)$$

$$F_2 = \frac{\langle x^4 \rangle}{\langle x^2 \rangle^2} = 3w \quad (C2b)$$

where  $w = e^{s^2}$ . These equations are easily solved to estimate the unknown parameters  $\mu$  and  $s$ . In the present work, these method of moments-based estimates are used as initial conditions for the MLE computations. A commercial MLE function from MATLAB<sup>TM</sup>, employing the Nelder-Mead method, is utilized.

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