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Mapping current fluctuations of stochastic pumps to nonequilibrium steady states

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We show that current fluctuations in a stochastic pump can be robustly mapped to fluctuations in a corresponding time-independent nonequilibrium steady state. We thus refine a recently proposed mapping so that it ensures equivalence of not only the averages, but also optimal representation of fluctuations in currents and density. Our mapping leads to a natural decomposition of the entropy production in stochastic pumps similar to the “housekeeping” heat. As a consequence of the decomposition of entropy production, the current fluctuations in weakly perturbed stochastic pumps are shown to satisfy a universal bound determined by the steady state entropy production.

Nonequilibrium steady states are an essential paradigm for describing nanoscale biological machines, such as molecular motors that extract work from chemical gradients [1]. When a system is coupled to reservoirs with different chemical potentials, the dynamics breaks detailed balance and persistent, directed motion can be used to perform mechanical work. Such a system is typically described as a Markov process with time-independent rates that depend both on the external chemical gradient and internal dynamics.

Promising applications across many disciplines have motivated efforts to design artificial molecular machines that behave like those in biological settings. Nonequilibrium steady states, however, have proved difficult to engineer [2]. Time-dependent external perturbations offer an alternative route to breaking detailed balance. Indeed, many synthetic nanoscale machines are implemented as “stochastic pumps,” in which currents are generated by periodically varying an external potential [3–7]. A stochastic pump can be modeled as a non-homogeneous Markov jump process with instantaneous Arrhenius rates that are determined by time-dependent energy levels and barrier heights [8–10].

Recently, Raz *et al.* [10] proposed a mapping between time-independent steady states and periodically driven stochastic pumps that offers a set of design principles for engineering biomimetic nanodevices. While the mapping ensures that the average properties are asymptotically equivalent in both representations, it makes no guarantees about the fluctuations. At the nanoscale, however, fluctuations play a crucial role in determining characteristics like work and efficiency in finite-time measurements [11, 12]. Indeed, fluctuations in both efficiency and current have become a central focus in nonequilibrium statistical mechanics: theoretic-

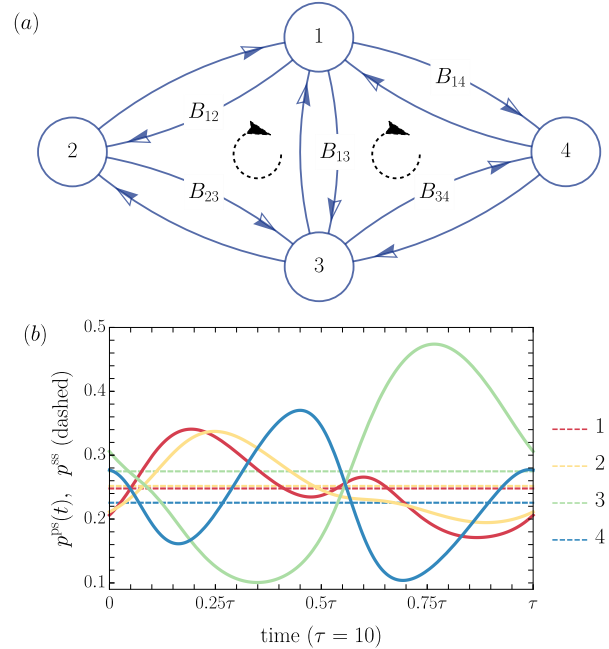


FIG. 1. (a) A schematic of the stochastic pump under consideration. Symmetric barriers B_{ij} and energy levels E_i parametrize Arrhenius rates and are varied periodically in time to generate a current. The corresponding nonequilibrium steady state representation of the pump has no time-dependence, but rather rates that break detailed balance. (b) The time periodic steady state probabilities for each site on the graph are shown over an entire period τ . The solid lines show the time-dependent occupation of the pump. The dashed lines show the average occupancy per period, a property matched by the corresponding steady state.

cal developments have predicted universal properties of fluctuating nanoscale machines [11, 13–15] and experimental realizations of nanoscale engines have drawn particular attention to the impact of fluctuations on measurements of efficiency [7, 16].

Translating between nonequilibrium steady states

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and stochastic pumps relies on the so-called “dynamical equivalence principle” of Zia and Schmittmann [17]. This principle stipulates that nonequilibrium steady states are characterized by the average currents and the average density. For Markov jump processes, the asymptotic fluctuations of a nonequilibrium steady state, however, are not dictated by these average properties alone.

Developments in large deviation theory, in particular the Level-2.5 formalism, have provided a general characterization of fluctuations away from the average behavior in Markov jump processes and diffusions [18–20]. In this framework, both the average currents and their fluctuations are uniquely determined by the empirical density,

$$\rho_x = \frac{1}{t_{\text{obs}}} \int_0^{t_{\text{obs}}} dt \delta_{z(t),x}, \quad (1)$$

with $z(t)$ denoting the state at time t , and the empirical flow,

$$q_{yx} = \frac{1}{t_{\text{obs}}} \int_0^{t_{\text{obs}}} dt \delta_{z(t^-),x} \delta_{z(t^+),y}, \quad (2)$$

which, roughly, counts the number hops from state x to y . It is important to note that the empirical flow contains more information than the empirical current; the latter specifies only the difference between the flow in the forward and reverse directions $j_{xy} = q_{xy} - q_{yx}$. For example, the empirical current would not distinguish between a trajectory in which there are 100 $x \rightarrow y$ hops and 80 $y \rightarrow x$ hops from one in which there are 20 $x \rightarrow y$ hops and 0 in the opposite direction, while the flows would be dramatically different. The large deviation rate function, $I(\rho, q)$, quantifies the rate of decay of probability of a joint observation of density and flow,

$$P(\rho, q) \asymp \exp(-t_{\text{obs}} I(\rho, q)). \quad (3)$$

The symbol \asymp indicates a logarithmic equivalence between $I(\rho, q)$ and $\lim_{t_{\text{obs}} \rightarrow \infty} -1/t_{\text{obs}} \ln P(\rho, q)$. For both jump processes and diffusions, the rate function I can be calculated explicitly [18, 19]. Once the joint rate function for empirical density and empirical flow is known, fluctuations in currents can be computed via the contraction principle [21].

The large deviation formalism suggests a stricter requirement for dynamical equivalence among jump processes: if the asymptotic form of the fluctuations is to be accurately captured, then it is not the average currents, but rather the average flows that must be used to describe the dynamics of a nonequilibrium steady state; a detailed discussion is provided in the Supplemental Material [22]. This is a more rigid prescription, as detailed below. Further, these insights

motivate a solution to the mapping problem between stochastic pumps and nonequilibrium steady states that preserves the fluctuations. Interestingly, in order to optimally describe current fluctuations of a stochastic pump, the corresponding nonequilibrium steady state must have a lower average entropy production rate than that of the pump. The origin of this “excess” entropy production can be explained with a simple decomposition of the entropy production of the stochastic pump [23–25].

The nonequilibrium steady state representation of the pump satisfies a universal lower bound on the magnitude of its current fluctuations, dictated by the total entropy production less the excess [14, 15, 26]. As a consequence of this splitting, we demonstrate that, in a perturbative limit, stochastic pumps satisfy a universal bound on their current fluctuations, dictated by the entropy production of the corresponding steady state. We also probe the breakdown of this limit under strong driving, as discussed further in the Supplemental Material [22]. Taken together, these insights offer a powerful set of design principles for translating between stochastic pumps and steady states as well as a potentially useful technique for theoretical analysis of systems under time-dependent driving.

To illustrate our mapping, we consider a simple model of a stochastic pump: a single particle hopping with Arrhenius rates on a four state graph. We vary two energy levels and one barrier periodically in time, which provides a time-dependent perturbation that generates a non-vanishing current, as permitted by the no-pumping theorem [4–6]. This setup is depicted in Fig. 1 (a).

The pump achieves a periodic steady state, which can be calculated numerically by integrating,

$$p_i^{\text{ps}}(t+s) = \int_t^s W_{ij}(t+t') p_j^{\text{ps}}(t+t') dt'. \quad (4)$$

Here $p_i^{\text{ps}}(t)$ is the probability of being in state i at time t and $W(t)$ is the continuous time rate matrix for the dynamics at time t . The periodic steady state satisfies

$$p_i^{\text{ps}}(t+\tau) = p_i^{\text{ps}}(t), \quad (5)$$

where τ is the period of the pumping protocol. Note that, by construction, $W(t)$ satisfies detailed balance at each point in time. The Arrhenius rates determine the instantaneous rate matrix

$$W_{ij}(t) = e^{-\beta(B_{ij}(t)-E_j(t))} \quad \text{for } i \neq j$$

$$W_{ii}(t) = -\sum_{j \neq i} W_{ij}(t)$$

where $E_j(t)$ denotes the energy level of state j and $B_{ij}(t) = B_{ji}(t)$ is the barrier height. In our example,

the only time-dependent quantities are

$$\begin{aligned} E_3(t) &= \sin(2\pi t/\tau) + 1, \\ E_4(t) &= \sin(4\pi t/\tau), \\ B_{13}(t) &= \sin(2\pi t/\tau). \end{aligned} \quad (6)$$

The periodic solution is plotted in Fig. 1 (b).

We aim to find a time-independent rate matrix W^{ss} that mimics the stochastic pump and matches its fluctuations. Following [17], we let $\bar{W}_{ij} = W_{ij}^{\text{ss}} \hat{p}_j$ where \hat{p}_j is the average occupancy in the periodic steady state and write

$$\bar{W}_{ij} = \mathcal{S}_{ij} + \mathcal{A}_{ij}, \quad (7)$$

where \mathcal{S} is a symmetric, stochastic matrix and \mathcal{A} is an antisymmetric matrix. The symmetric part of this decomposition is related to the “activity” of a trajectory [27, 28]. The continuous time rate matrix for the dynamics is then given by

$$W^{\text{ss}} = (\mathcal{S} + \mathcal{A}) \mathcal{P}^{-1}, \quad (8)$$

where \mathcal{P} is a diagonal matrix with $\mathcal{P}_{ii} = \hat{p}_i$, the steady state probability of site i . If we further impose the constraint that the steady state currents agree with the periodic average current along each edge,

$$\hat{j}_{ij} = \int_0^\tau dt W_{ij}(t) p_j^{\text{ps}}(t) - W_{ji}(t) p_i^{\text{ps}}(t), \quad (9)$$

then the antisymmetric part of the rate matrix is uniquely identified,

$$\mathcal{A}_{ij} = \frac{1}{2} \hat{j}_{ij}. \quad (10)$$

The rate matrix W^{ss} describes a probability conserving stochastic process, and, as a result, the form of \mathcal{S} is constrained, but only weakly. In particular, it must be the case that

$$\mathcal{S}_{ij} \geq |\mathcal{A}_{ij}| \quad (11)$$

and

$$\sum_j \mathcal{S}_{ij} = 0, \quad (12)$$

which ensures that W^{ss} is a stochastic matrix.

Though the rate matrix is not uniquely specified, any valid choice of \mathcal{S} results in a stochastic process with identical average currents and average occupancy statistics. The same cannot be said for the fluctuations. The freedom in \mathcal{S} can be directly represented by noting that any valid off-diagonal entry in the matrix can be written,

$$\mathcal{S}_{ij} = c_{ij} |\mathcal{A}_{ij}|, \quad c_{ij} > 1. \quad (13)$$

Due to symmetry, there are $N(N-1)/2$ choices to make. Indeed, the rate matrices resulting from different choices of \mathcal{S} yield different average entropy production rates, given by,

$$\hat{\sigma}_{ij} = \hat{j}_{ij} \ln \frac{c_{ij} |\hat{j}_{ij}| + \hat{j}_{ij}}{c_{ij} |\hat{j}_{ij}| - \hat{j}_{ij}}. \quad (14)$$

The c_{ij} values can be varied independently so long as they meet the constraint $c_{ij} \geq 1$, meaning that the total entropy production can be made arbitrarily small by taking c_{ij} large.

Raz *et al.* [10] suggest choosing \mathcal{S} so that the average entropy production rate along each edge is the same in the stochastic pump and the nonequilibrium steady state representations. This choice, which we denote $\mathcal{S}_{\langle \sigma \rangle}$ uniquely specifies a rate matrix and also guarantees that the average current, occupancy, and entropy production rates are preserved by the map. However, the asymptotic fluctuations in entropy production and current are dramatically different.

To demonstrate this, we computed the entropy production and current large deviation rate functions for both the stochastic pump and the nonequilibrium steady state representation, shown in Fig. 2. To calculate the rate functions, we first compute the scaled cumulant generating functions for entropy production ω and current j ,

$$\psi_\omega(\lambda) = \lim_{t \rightarrow \infty} \frac{1}{t} \ln \langle e^{-\lambda \omega} \rangle, \quad \psi_j(s) = \lim_{t \rightarrow \infty} \frac{1}{t} \ln \langle e^{-s j} \rangle. \quad (15)$$

For the nonequilibrium steady state representation, the cumulant generating functions can be calculated exactly by Cramér tilting [21]. In the case of the stochastic pump, the averages in (15) can be directly evaluated in the time-periodic steady state, meaning that the cumulant generating function can be numerically computed as,

$$\psi_\omega(\lambda) = \frac{1}{\tau} \ln \sum_j \int_0^\tau W_{ij}(t; \lambda) p_j^{\text{ps}}(t), \quad (16)$$

where $W(t; \lambda)$ is the tilted rate matrix for entropy production [29]. We use the Gärtner-Ellis theorem to compute the large deviation rate functions by first computing the scaled cumulant generating function and then performing a Legendre-Fenchel transform [21].

Fig. 2 (b) shows the entropy production rate function with $W^{\text{ss}} = (\mathcal{S}_{\langle \sigma \rangle} + \mathcal{A}) \mathcal{P}^{-1}$. Note that, while the averages agree, the nature of the entropy production fluctuations is quite different. The steady state with the matching average entropy production has a notably fatter tail for large entropy production rates.

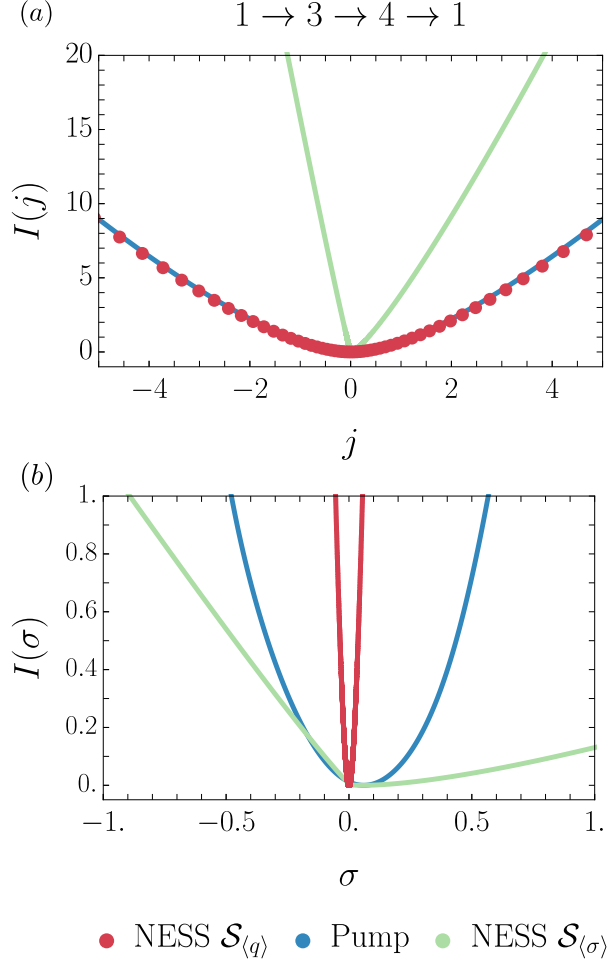


FIG. 2. (a) The large deviation rate function for the current around the upper cycle (see Fig. 1) $1 \rightarrow 3 \rightarrow 4 \rightarrow 1$ is shown for the stochastic pump (blue / dark gray) the nonequilibrium steady state with the same average entropy production along each edge as the pump (green / light gray), and the nonequilibrium steady state with the same average flow along each edge as the pump (red dots). While the nonequilibrium steady state with $\mathcal{S}_{\langle\sigma\rangle}$ has the same average current, the character and extent of its fluctuations are extremely different. Choosing $\mathcal{S}_{\langle q \rangle}$ preserves even very rare fluctuations in current. (b) The large deviation rate functions for entropy production reveal that the steady state that recapitulates the current fluctuations has a smaller average entropy production. Furthermore, the extent of entropy production fluctuations in the corresponding steady state is much less pronounced (red innermost curve). The pump is shown in blue (dark gray) and has fluctuations that are intermediate in magnitude between the two representations. $\mathcal{S}_{\langle\sigma\rangle}$, on the other hand, leads to greatly enhanced entropy production fluctuations, as shown in the green / light gray outermost curve.

Excess entropy production.— In order to match

the fluctuations in current, we instead choose \mathcal{S} so that the average empirical flows are accurately captured by the dynamics. In particular, we let

$$\mathcal{S}_{\langle q \rangle} = \hat{q}_{ij} - \frac{1}{2} \hat{j}_{ij} \iff \bar{W}_{ij} = \hat{q}_{ij}, \quad (17)$$

where \hat{q}_{ij} denotes the average flow along edge ij in the periodic steady state. This choice has the additional advantage of simplicity: the dynamics produces the correct average number of hops in both directions along each edge of the network. We note that for high-dimensional networks, measuring all of the detailed edge currents or flows could be a formidable challenge. Nevertheless, biological motors have been successfully modeled as Markov jump processes with a small number of distinct ligation states [30] and engineered nanodevices typically have only a few states [31]. Because \mathcal{S} does not affect the antisymmetric part of the rate matrix, the average currents along each edge are equivalent in both the stochastic pump and the nonequilibrium steady state. As illustrated by Fig. 2 (a), choosing $\mathcal{S}_{\langle q \rangle}$ leads to striking agreement between the current fluctuations of the stochastic pump and the corresponding steady state.

However, with the choice of $\mathcal{S}_{\langle q \rangle}$, both the average entropy production rate and its fluctuations in the nonequilibrium steady state representation differ markedly from the corresponding stochastic pump, as shown in Fig. 2 (b). The “excess” entropy production has a physical origin and can be explained with a natural decomposition of the stochastic pump entropy production. Unlike nonequilibrium steady states, which can only produce entropy around closed cycles, stochastic pumps can produce entropy without completing a cycle [32]. We decompose the total stochastic pump entropy production rate into a contribution from the steady state, akin to the “housekeeping heat”, and the excess associated with the pumping protocol [23, 24],

$$\sigma^{\text{pump}} = \sigma^{\text{ss}} + \sigma^{\text{ex}}, \quad (18)$$

where,

$$\sigma_{ij}^{\text{ss}} = \hat{j}_{ij} \ln \frac{\hat{q}_{ij}}{\hat{q}_{ji}}, \quad (19)$$

and,

$$\sigma_{ij}^{\text{ex}} = \frac{1}{\tau} \int_0^\tau j_{ij} \left(\ln \frac{q_{ij}}{q_{ji}} - \ln \frac{\hat{q}_{ij}}{\hat{q}_{ji}} \right). \quad (20)$$

The Second Law of Thermodynamics ensures that both σ^{pump} and σ^{ss} are non-negative on average. This decomposition is analogous to the decomposition of entropy production used to describe the “housekeeping heat”, i.e., the amount of

heat required to maintain a nonequilibrium steady state [23–25].

The excess entropy produced by the stochastic pump, σ^{ex} is also non-negative. The inequality,

$$\frac{1}{\tau} \int_0^\tau j_{ij} \ln \frac{q_{ij}}{q_{ji}} \geq \hat{j}_{ij} \ln \frac{\hat{q}_{ij}}{\hat{q}_{ji}}. \quad (21)$$

is known as the log-sum inequality and follows directly from Jensen’s inequality, because $q_{ij}(t) > 0$ and $x \ln x$ is a convex function, as detailed in the supplementary information [33]. In the adiabatic limit, the system remains in the instantaneous equilibrium distribution and σ^{ex} vanishes. In this limiting case, $S_{\langle\sigma\rangle} = S_{\langle\omega\rangle}$. That is, for slow driving, entropy is only produced in the long time limit if probability is pumped through the network on average. While one might hope to match both the current and entropy production fluctuations when mapping a stochastic pump to a nonequilibrium steady state, or vice versa, this can only be achieved if the pumping protocol is adiabatic. As a consequence, in the inverse mapping problem, a pump protocol cannot generally be designed to mimic both current and entropy production fluctuations because the average entropy productions only agree in the adiabatic limit. Choosing the time-independent rate matrix so that it gives the steady state entropy production of the stochastic pump, that is, choosing \mathcal{S}_q , yields a coarse-graining that is consistent with the physical mechanism by which entropy is produced in the pump.

In a stochastic pump, the hopping statistics along each edge need not be Poissonian, even in the adiabatic limit [34]. Therefore, the instantaneous dynamics of the nonequilibrium steady state, for which all transitions are purely Poissonian, may not perfectly recapitulate the behavior of the pump. An effective dynamics can be constructed by a periodic solution via Floquet Theory, an analysis performed in the Supplemental Material [22]. In the limit that time-periodic perturbations to the hopping rates are

small, the nonequilibrium steady state representation describes the dynamics of the pump at all times, but for sufficiently strong driving the correspondence in fluctuations weakens. Numerical simulations using the kinetic Monte Carlo technique provide additional support that this correspondence is nevertheless robust, see the Supplemental Material [22], and emphasize that statistics converge to the large deviation form on timescales that can easily be accessed in simulations and experiments.

The mapping determined by the choice (17) yields a universal bound on current fluctuations in weakly driven stochastic pumps, akin to the thermodynamic uncertainty relations recently discovered for nonequilibrium steady states [14, 15, 26, 35, 36]. Distinct behavior can be achieved with random driving: Barato and Seifert recently showed that, through the use of a driving protocol that changes at stochastic times, current fluctuations can be suppressed without incurring significant dissipation [37]. For the deterministic protocols considered here, in the perturbative limit, the rate function for any generalized current j is subject to a quadratic bound determined by the steady state entropy production rate,

$$I^{\text{pump}}(j) \leq \frac{(j - \hat{j})^2}{4\hat{j}^2/\sigma^{\text{ss}}}. \quad (22)$$

The bound is maximally tight because incorporating the excess entropy production only reduces the curvature of the quadratic form. The lack of Poisson statistics for the pump suggests that the bound should not hold in full generality, but numerical evidence demonstrates that it is quite robust.

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