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Asymmetric crystallization during cooling and heating in model glass-forming systems

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We perform molecular dynamics (MD) simulations of the crystallization process in binary Lennard-Jones systems during heating and cooling to investigate atomistic-scale crystallization kinetics in glass-forming materials. For the cooling protocol, we prepared equilibrated liquids above the liquidus temperature \(T_l\) and cooled each sample to zero temperature at rate \(R_c\). For the heating protocol, we first cooled equilibrated liquids to zero temperature at rate \(R_h\) and then heated the samples to temperature \(T > T_l\) at rate \(R_h\). We measured the critical heating and cooling rates \(R_h^*\) and \(R_c^*\), below which the systems begin to form a substantial fraction of crystalline clusters during the heating and cooling protocols. We show that \(R_h^* > R_c^*\) and that the asymmetry ratio \(R_h^*/R_c^*\) includes an intrinsic contribution that increases with the glass-forming ability (GFA) of the system and a preparation-rate dependent contribution that increases strongly as \(R_p \to R_c^*\) from above. We also show that the predictions from classical nucleation theory (CNT) can qualitatively describe the dependence of the asymmetry ratio on the GFA and preparation rate \(R_p\) from the MD simulations and results for the asymmetry ratio measured in Zr- and Au-based bulk metallic glasses (BMG).

This work emphasizes the need for and benefits of an improved understanding of crystallization processes in BMGs and other glass-forming systems.

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I. INTRODUCTION

Crystallization, during which a material transforms from a dense, amorphous liquid to a crystalline solid, occurs via the nucleation and subsequent growth of small crystalline domains [1]. Crystallization in metals has been intensely studied over the past several decades with the goal of developing the ability to tune the microstructure to optimize the mechanical properties of metal alloys [2–4]. However, in-situ observation of crystallization in metallic melts is limited due to the rapid crystallization kinetics of metals [5–7].

In contrast, bulk metallic glasses (BMGs), which are amorphous metal alloys, can be supercooled to temperatures below the solidus temperature \(T_s\) and persist in a dense, amorphous liquid state over more than 12 orders of magnitude in time scales or viscosity [8]. Deep supercooling of BMGs provides the ability to study crystallization on time scales that are accessible to experiments [9–12].

These prior experimental studies have uncovered fundamental questions concerning crystallization kinetics in BMGs. For example, when a BMG in the glass state is heated to a temperature \(T_f < T_s\) in the supercooled liquid region, crystallization is much faster than crystallization that occurs when the metastable melt is cooled to the same temperature \(T_f\) [13, 14]. Asymmetries in the crystallization time scales upon heating versus cooling of up to two orders of magnitude have been reported in experiments [15, 16]. The asymmetry impacts industrial applications of BMGs because rapid crystallization upon heating limits the thermoplastic forming processing time window for BMGs [17–20].

Recent studies have suggested that the asymmetry in the crystallization time scales originates from the temperature dependence of the nucleation and growth rates [15], i.e. that the nucleation rate is maximal at a temperature below that at which the growth rate is maximal. According to this argument, crystallization upon heating is faster because of the growth of the nascent crystal nuclei that formed during the thermal quench to the glass. In contrast, crystallization is slower upon cooling since crystal nuclei are not able to form at high temperatures in the melt. However, there has been no direct visualization of the crystallization process in BMGs, and it is not yet understood why the asymmetry varies from one BMG to another [21] and how sensitively the asymmetry depends on the cooling rate \(R_p\) used to prepare the glass. An improved, predictive understanding of the crystallization process in BMGs will aid the design of new BMG-forming alloys with small crystallization asymmetry ratios and large thermoplastic processing time windows.

We employ molecular dynamics (MD) simulations of bidisperse spheres interacting via Lennard-Jones potentials [22–24] to visualize directly the crystallization process upon heating and cooling in model metallic glass-
forming systems. We perform thermal quenches of the system from a high temperature $T_i$ in the equilibrated liquid regime to a glass at $T_f = 0$ and vary the cooling rate $R_c$ by several orders of magnitude. For cooling rates below the critical cooling rate $R_c < R_c^*$, the system begins to crystallize, whereas for $R_c > R_c^*$, the system remains amorphous. We also performed MD simulations in which we heat the zero-temperature glassy states (prepared at cooling rate $R_p > R_c^*$) through the supercooled liquid regime to $T_f = T_i$ over a range of heating rates $R_h$. For heating rates $R_h < R_h^*$, the system begins to crystallize, whereas for $R_h > R_h^*$, it remains amorphous. We also find that the critical heating rate has an intrinsic contribution $R_h^*(\infty)$ and an $R_p$-dependent contribution $R_h^*(R_p) - R_h^*(\infty)$ that increases with decreasing $R_p$. We measured the asymmetry ratio $R_h^*/R_c^*$ as a function of the glass-forming ability (GFA) and $R_p$ for several binary Lennard-Jones mixtures and find that $R_h^*/R_c^* > 1$ and the ratio grows with increasing GFA and decreasing $R_p$. We show that these results are consistent with predictions from classical nucleation theory (CNT) that the maximal growth rate occurs at a higher temperature than the maximal nucleation rate and that the separation between the nucleation and growth peaks increases with the GFA. Further, CNT is able to qualitatively re-capitulate the dependence of the asymmetry ratio on the GFA as measured through $R_h^*$ for both our MD simulations and recent experiments on BMGs as well as on $R_p$ for the MD simulations [25].

The remainder of the manuscript is organized into three sections: Sec. II: Methods, Sec. III: Results, and Sec. IV: Conclusion. In Sec. II, we describe the MD simulations of binary Lennard-Jones mixtures, the computational methods to detect and structurally characterize crystal nuclei, and measurements of the critical cooling and heating rates, $R_c^*$ and $R_h^*$. In Sec. III, we show results from MD simulations for the time-temperature transformation diagram [26] and the asymmetry ratio $R_h^*/R_c^*$ as a function of the glass-forming ability as measured by the critical cooling rate $R_c^*$ and the cooling rate used to prepare the zero-temperature glasses $R_c$. We also compare our simulation results for the asymmetry ratio to experimental measurements of the ratio for two BMGs and to predictions of the ratio from classical nucleation theory. In Sec. IV, we briefly summarize our results and put forward our conclusions.

II. METHODS

We performed MD simulations of binary Lennard-Jones (LJ) mixtures of $N = N_A + N_B$ spheres with mass $m$ at constant volume $V = L^3$ in a cubic simulation box with side length $L$ and periodic boundary conditions. We studied mixtures with $N_A = N_B$ and diameter ratio $\alpha = \sigma_B/\sigma_A < 1$. We employed the LJ pairwise interaction potential between spheres $i$ and $j$:

$$u(r_{ij}) = 4\epsilon[(\sigma_{ij}/r_{ij})^{12} - (\sigma_{ij}/r_{ij})^{6}],$$

where $r_{ij}$ is their center-to-center separation, $\epsilon$ is the depth of the minimum in the potential energy $u(r_{ij})$, $\sigma_{ij} = (\sigma_i + \sigma_j)/2$, and $u(r_{ij})$ has been truncated and shifted so that the potential energy and force vanish for separations $r_{ij} \geq 3.5\sigma_{ij}$ [27]. We varied the system volume $V$ to fix the packing fraction $\phi = \pi\sigma_A^3(N_A + \alpha^3 N_B)/6V = 0.5236$ [28] at each diameter ratio $\alpha$. For most simulations, we considered $N = 1372$ spheres, but we also studied $N = 4000$ and 8788 to assess finite-size
effects. Below, energy, length, time, and temperature scales are expressed in units of $\epsilon$, $\sigma_A$, $\sigma_A \sqrt{m/\epsilon}$, and $\epsilon/k_B$, respectively, where the Boltzmann constant $k_B$ has been set to be unity.

A. Cooling and Heating Protocols

For each particle diameter ratio, which yield different glass-forming abilities, we performed MD simulations to cool metastable liquids to zero temperature and heat zero-temperature glasses into the metastable liquid regime to measure $R^c_*$ and $R^b_*$ at which the systems begin to crystallize. To measure $R^c_*$, we first equilibrate the system at high temperature $T_i = 2.0$ using a Gaussian constraint thermostat [27]. We then cool the system by decreasing the temperature linearly at rate $R_c$ from $T_i$ to $T_f = 0$:

$$T(t) = T_i - R_c t. \quad (2)$$

To measure the critical heating rate $R_h^b(R_p)$ at finite rate $R_p$, we first prepare the systems in a glass state by cooling them from the high temperature liquid state to zero-temperature at rate $R_p > R^c_*$. To measure the intrinsic critical heating rate $R_h^b(\infty)$, we quench the systems infinitely fast to zero temperature using conjugate gradient energy minimization. For both cases, we heat the zero-temperature glasses using a linear ramp

$$T(t) = R_h t \quad (3)$$

until $T_f = 2.0$. For both heating and cooling protocols, we carried out $N_{\text{tot}} = 1000$ independent trajectories and averaged the results.

B. Identification of Crystal Nuclei

To detect the onset of crystallization in our simulations [15], we differentiate ‘crystal-like’ versus ‘liquid-like’ particles based on the value of the area-weighted bond orientational order parameter for each particle [29, 30]. We define the complex-valued bond orientational order parameter for particle $i$:

$$q_{lm}(i) = \frac{\sum_{j=1}^{N_h} A_{ij} Y_{lm}(\theta(\vec{r}_{ij}), \phi(\vec{r}_{ij}))}{\sum_{j=1}^{N_h} A_{ij}}, \quad (4)$$

where $Y_{lm}(\theta(\vec{r}_{ij}), \phi(\vec{r}_{ij}))$ is the spherical harmonic of degree $l$ and order $m$, $\theta(\vec{r}_{ij})$ and $\phi(\vec{r}_{ij})$ are the polar and azimuthal angles for the vector $\vec{r}_{ij}$, $j = 1, \ldots, N_h$ gives the index of the Voronoi neighbors of particle $i$, and $A_{ij}$ is the area of the face of the Voronoi polyhedral common to particles $i$ and $j$. The correlation coefficient [29] between the bond orientational order parameters $q_{lm}(i)$ and $q_{lm}(j)$, where particle $j$ is a Voronoi neighbor of $i$, is sensitive to face-centered-cubic (FCC) order. When $S_{ij} > 0.7$, $i$ and $j$ are considered ‘connected’. If particle $i$ has more than 10 connected Voronoi neighbors, it is defined as ‘crystal-like’. The ratio $N_{cr}/N$ gives the fraction of crystal-like particles in a given configuration. In addition, we also define a crystal cluster as the set of crystal-like particles that possess mutual Voronoi neighbors. Distinct crystal clusters that nucleate and grow upon heating and cooling are shown in Fig. 1.

This general scheme for identifying crystal-like particle clusters has been implemented in prior studies [39–41], however, we made two improvements [42]. First, we defined nearest-neighbor particles by Voronoi tessellation to remove the arbitrariness associated with defining neighbors using a cutoff distance. Second, the definition of the bond orientational order parameter $q_{lm}$ weights each bond between the central particle and its nearest neighbors by the area of the associated Voronoi polyhedral face, such that $q_{lm}$ is a continuous function of particle coordinates.

C. Probability for Crystallization

For each diameter ratio and rate, we measure the probability for crystallization $P(R_{h,c}) = N_X/N_{\text{tot}}$, where $N_X$ is the number of trajectories that crystallized with $N_{cr}/N > 0.5$ during the heating or cooling protocol and $N_{\text{tot}}$ is the total number of trajectories (cf. insets to Fig. 2). We find that the data for $P(R_{h,c})$ collapses onto a sigmoidal scaling function as shown in Fig. 2:

$$\frac{P(R_{h,c}) - P_{h,c}^{\infty}}{P_{h,c}^0 - P_{h,c}^{\infty}} = \frac{1}{2} \left[ 1 - \tanh \left( \log_{10} \left( \frac{R_{h,c}}{R_{h,c}^M} \right)^{1/\kappa_{h,c}} \right) \right], \quad (6)$$

where $P_{h,c}^{\infty}$ is the probability for crystallization in the limit of infinitely fast rates $R_{h,c} \to \infty$, $P_{h,c}^0$ is the probability for crystallization in the $R_{h,c} \to 0$ limit, $R_{h,c}^M$ is the rate at which $P(R_{h,c}) = (P_{h,c}^0 + P_{h,c}^{\infty})/2$, and $\kappa_{h,c}$ is the stretching factor. We find that $\kappa_c \approx 0.25$ and $\kappa_h \approx 0.2$ for $\alpha = 1.0$, and these factors increase by only a few percent over the range in $\alpha$ that we consider. We define the critical heating and cooling rates $R^c_*$ and $R^b_*$ by the rates at which $P(R_{h,c}) = 0.5$, i.e.

$$R^c_*= R_{h,c}^M \kappa_{h,c} \tanh^{-1} \left[ \frac{P_{h,c}^0 + P_{h,c}^{\infty}}{R_{h,c}^M} \right]. \quad (7)$$

As shown in the insets to Fig. 2, for $R_{h,c} \ll R^c_*$, most of the configurations crystallize during heating or cooling. In contrast, for $R_{h,c} \gg R^c_*$, none of the configurations crystallize.
FIG. 2: Shifted and normalized probability for crystallization $(P(R_{h,c}) - P_{\infty}^*(R_{h,c})/(P_{0}^*(R_{h,c}) - P_{\infty}^*(R_{h,c}))$ versus the scaled heating or cooling rate $\log_{10}(R_{h,c}/R_{h,c}^*\lambda_{h,c})$. Circles (squares) indicate data for cooling (heating) for diameter ratios $\alpha = 1.0$ (filled symbols) and 0.97 (open symbols). The insets show the fraction of crystal-like particles $N_{cr}/N$ as a function of temperature $T$ during cooling (lower left) and heating (upper right) for 12 configurations with $\alpha = 1.0$. The four solid, dashed, and dot-dashed curves in each inset correspond to cooling and heating trajectories with rates slower than $R_{h,c}^*$, near $R_{h,c}^*$, and faster than $R_{h,c}^*$, respectively. Trajectories for which $N_{cr}/N$ exceeds 0.5 (above the horizontal dashed line) are considered to have crystallized during the heating or cooling protocol.

III. RESULTS

An advantage of MD simulations is that they can provide atomic-level structural details of the crystallization dynamics that are often difficult to obtain in experiments. In Fig. 1, we visualize the nucleation and growth of clusters of crystal-like particles during the heating and cooling simulations. In both cases, the number of clusters reaches a maximum near $T \approx 0.5$. In Fig. 3, we show the maximum number of clusters $N_{max}$ (normalized by $L^3/\sigma^3$) that form during the heating and cooling protocols. We find that more crystal clusters form during the heating protocol compared to the cooling protocol for all particle diameter ratios studied, which is supported by the measured time-temperature-transformation (TTT) diagram. In addition, we will show below that the asymmetry ratio $R_{h}^*(\infty)/R_{c}^*$ for finite preparation rates $R_{p}$ will be considered in Sec. III C.) In Fig. 4, we plot $R_{h}^*(\infty)/R_{c}^*$ versus $R_{p}$ for diameter ratios $\alpha = 1.0, 0.97, 0.96, 0.95$ and 0.93. We find that $R_{h}^*(\infty) > R_{c}^*$ for all systems studied, which is consistent with classical nucleation theory (CNT). As shown in Fig. 1, more crystal nuclei form during the heating protocol than during the cooling protocol. In addition, CNT predicts that the growth rates for crystal nuclei are larger during heating compared to cooling. In Sec. III B, we will show that both factors contribute to an increased probability for crystallization during heating.

A. Intrinsic Asymmetry Ratio

The critical heating and cooling rates can be obtained by fitting the probability for crystallization $P(R_{h,c})$ as a function of $R_{h}$ or $R_{c}$ to the sigmoidal form in Eq. 6. We first investigate the minimum value for the asymmetry ratio $R_{h}^*(\infty)/R_{c}^*$, which is obtained by taking the $R_{p} \to \infty$ limit. (The asymmetry ratio $R_{h}^*(R_{p})/R_{c}^*$ for finite preparation rates $R_{p}$ will be considered in Sec. III C.) In Fig. 4, we plot $R_{h}^*(\infty)/R_{c}^*$ versus $R_{p}$ for diameter ratios $\alpha = 1.0, 0.97, 0.96, 0.95$ and 0.93. We find that $R_{h}^*(\infty) > R_{c}^*$ for all systems studied, which is consistent with classical nucleation theory (CNT). As shown in Fig. 1, more crystal nuclei form during the heating protocol than during the cooling protocol. In addition, CNT predicts that the growth rates for crystal nuclei are larger during heating compared to cooling. In Sec. III B, we will show that both factors contribute to an increased probability for crystallization during heating.

In Fig. 4, we also show that the asymmetry ratio $R_{h}^*(\infty)/R_{c}^*$ increases as the critical cooling rate $R_{c}^*$ decreases, or equivalently as the glass-forming ability increases. In the MD simulations, we were able to show a correlation between the asymmetry ratio and the critical cooling rate over roughly an order of magnitude in $R_{c}^*$. In Sec. III B, we introduce a model that describes
Ting temperature, \( \Delta G \) volume (in units of \( \epsilon/\sigma \)) normalized by \( R_0 = 1 K/s \) on a logarithmic scale. The inset shows the intrinsic asymmetry ratio versus \( \log_{10}(R_c^*/R_0) \) on an expanded scale. The filled circles indicate data from the MD simulations and filled squares indicate data from experiments on Zr- and Au-based BMGs [15, 16]. The prediction (Eq. 12) from classical nucleation theory (solid line) with \( A' = (8\pi A\sigma^4)/3a^3 = 0.5 \) (in units of \( \epsilon/(m^2\sigma_\lambda^4) \)), \( \Sigma = 0.26 \), and \( Q_{eff} = 2.6 \) interpolates between the MD simulation data at high \( R_c^* \) and experimental data from BMGs at low \( R_c^* \).

**B. Classical Nucleation Theory Prediction for the Asymmetry Ratio**

In classical nucleation theory (CNT), the formation of crystals is a nucleation and growth process: fluctuations in the size of crystal nuclei that allow them to reach the critical radius \( r^* \), and then growth of post-critical nuclei with \( r > r^* \). Several recent studies [36–38] have explored a two-step mechanism for nucleation in supercooled liquids. In the current study, we measure the asymmetry in the critical cooling and heating rates, which is not sensitive to the nucleation mechanism.

To form a critical nucleus, the system must overcome a nucleation free energy barrier:

\[
\Delta G^* = \frac{16\pi}{3} \frac{\Sigma^3}{\Delta G^2},
\]

where \( \Delta G \) is the bulk Gibbs free energy difference per volume (in units of \( \epsilon/\sigma_\lambda^4 \)) and \( \Sigma \) is the surface tension between the solid and liquid phases (in units of \( \epsilon/\sigma_\lambda^2 \)). We assume that \( \Delta G = c(T_m - T) \) [34], where \( T_m \) is melting temperature, \( T_m - T \) is the degree of undercooling, and \( c \sim L_V/T_m \) is a dimensionless parameter that characterizes the thermodynamic drive to crystallize and will be used to tune the GFA of the system (where \( L_V \) is the latent heat of fusion). Within CNT, the rate of formation of critical nuclei (i.e. the nucleation rate) is given by:

\[
I = AD_0 \exp \left( -\frac{Q_{eff}}{T} \right) \exp \left( -\frac{\Delta G^*}{T} \right),
\]

where \( A \) is an \( O(1) \) constant with units \( \sigma_A^{-5} \), \( D_0 \) is the atomic diffusivity with units \( \sigma_A\sqrt{\epsilon/m} \), and \( Q_{eff} \) is an effective activation energy for the diffusivity with units \( \epsilon \). After the nucleation free energy barrier \( \Delta G^* \) has been overcome and crystal nuclei reach \( r \geq r^* \), the growth rate of crystal nuclei is given by:

\[
U = \frac{D_0}{a} \exp \left( -\frac{Q_{eff}}{T} \right) \left[ 1 - \exp \left( -\frac{\Delta G^*}{T} \right) \right],
\]

where \( a \) is the characteristic interatomic spacing.

In Fig. 5, we plot the nucleation \( I/AD_0 \) and growth rates \( U/a/D_0 \) with \( Q_{eff} = 2.6 \) and \( T_m \approx 1.40 \) from MD simulations of binary LJ systems [32], \( \Sigma = 0.26 \), which is typical for BMGs [15], while varying the GFA parameter from \( c = 1.2 \) to 0.5 (corresponding to diameter ratios from \( \alpha = 1.0 \) to 0.93.) Both \( I(T) \) and \( U(T) \) are peaked with maxima \( I^* \) and \( U^* \) at temperatures \( T_I \) and \( T_U \). In Fig. 5, we show that as the GFA increases, \( I^* \) and \( U^* \), as well as \( T_I \) and \( T_U \) decrease. However, \( T_I \) decreases...
faster than \( T_U \), so that the separation between the peaks, \( T_U - T_I \), increases with GFA.

To determine the critical heating and cooling rates, \( R_{c} \) and \( R_{p} \), we must calculate the fraction of the samples \( N_X \) that crystallize and the probability for crystallizing \( P(R_{h,c}) = N_X/N_{tot} \), where \( N_{tot} \) is the total number of samples, upon heating and cooling. Within classical nucleation theory, the probability to crystallize upon cooling from \( T_i \) to \( T_f \) is given by [33]:

\[
P(R_c) = \frac{4\pi}{3R_c^2} \int_{T_i}^{T_f} I(T') \left[ \int_{T'}^{T_f} U(T'')dT'' \right]^3 dT'. \tag{11}
\]

We assume that \( T_i \) is above the liquidus temperature \( T_L \), and \( T_f \) is below the glass transition temperature \( T_g \), where the time required to form crystal nuclei diverges. We can rearrange Eq. 11 to solve for the critical cooling rate at which \( P(R_c) = 0.5 \):

\[
(R_c^*)^4 = \frac{8\pi}{3} \int_{T_i}^{T_f} I(T') \left[ \int_{T'}^{T_f} U(T'')dT'' \right]^3 dT' = A' \int_{T_i}^{T_f} dT' \exp \left( -\frac{Q_{eff}}{T'} \right) \exp \left( -\frac{\Delta G^*}{T'} \right) \left[ \int_{T'}^{T_f} \exp \left( -\frac{Q_{eff}}{T''} \right) \right] \left[ 1 - \exp \left( -\frac{\Delta G^*}{T''} \right) \right] dT''^3,
\]

where \( A' = (8\pi AD_0)/\langle 3a^3 \rangle \) and we assumed that \( A \), \( D_0 \), and \( a \) are independent of temperature. A similar expression for the intrinsic critical heating rate \( R_{h}^*(\infty) \) can be obtained by reversing the bounds of integration in Eq. 12.

In Fig. 4, we plot the intrinsic asymmetry ratio \( R_{h}^*(\infty)/R_{c}^* \) predicted from Eq. 12 versus the critical cooling rate \( R_{c}^* \) after choosing the best value \( A' = 0.5 \) that interpolates between the MD simulation data at high \( R_{c}^* \) and experimental data from BMGs at low \( R_{c}^* \). We find that CNT qualitatively captures the increase in the asymmetry ratio with increasing GFA over a wide range of critical cooling rates from 1K/s (experiments on BMGs) to 10^12K/s (MD simulations of binary LJ systems). A comparison of Figs. 4 and 5 reveals that the increase in the intrinsic asymmetry ratio is caused by the separation of the peaks in the growth and nucleation rates \( U(T) \) and \( I(T) \) that occurs as the GFA increases. Thus, we predict an enhanced value for \( T_U - T_I \) in experiments on BMGs since the critical cooling rate in experiments is orders of magnitude smaller than in the MD simulations.

The fact that \( R_{h}^*(\infty) > R_{c}^* \) is also reflected in the asymmetry of the “nose” of the time-temperature-transformation (TTT) diagram. In Fig 6, we show the probability \( P \) that the system has crystallized at a given temperature \( T \) after a waiting time \( t \) for monodisperse LJ systems. We find that \( T_{min} \sim 0.5-0.6 \) is the temperature at which the waiting time for crystallization is minimized and that the time to crystallize is in general longer for \( T < T_{min} \) than for \( T > T_{min} \). Because crystallization on average occurs at a higher temperature during heating and a lower temperature during cooling, the asymmetry in the TTT diagram indicates that slower rates are required to crystallize during cooling than during heating, i.e. \( R_c^* < R_{h}^* \).

### C. Asymmetry Ratio for Finite \( R_p \)

In Sec. III B, we assumed that the initial samples (i.e. the zero-temperature glasses) for the heating protocol were prepared in the \( R_p \to \infty \) limit and, thus were purely amorphous. How does the asymmetry ratio \( R_{h}^*(R_p)/R_{c}^* \) depend on \( R_p \) when the preparation cooling rate \( R_p \) is finite and partial crystalline order can occur in the samples? In this section, we show results for the asymmetry ratio \( R_{h}^*(R_p)/R_{c}^* \) from MD simulations using a protocol where the samples are quenched from equilibrated liquid states to zero temperature at a finite rate \( R_p \) and then heated to temperature \( T_j \) at rate \( R_h \). (See Sec. II A.) Note that when \( R_p/R_{c}^* \approx 1 \), some of the samples remain amorphous.

In Fig. 7, we show the results for the asymmetry ratio \( R_{h}^*(R_p)/R_{c}^* \) from MD simulations. We find that \( R_{h}^*(R_p)/R_{c}^* \) increases rapidly as \( R_p \) approaches \( R_{c}^* \) from above and reaches a plateau value
R as used for the fit in Fig. 4 and the GFA parameter set to the prediction from CNT (solid line) with the same parameter set dominated by the preparation protocol. In contrast, the with decreasing of crystal nuclei that form during the quench increases respectively with that from the MD simulations. The number at a finite rate. In Fig. 7, we show that the asymmetry rate can also be calculated from CNT using an expression similar to horizontal dashed lines plateau value in the $R_p \gg R_c^*$ limit and $R_h^* = R_c^*$, respectively. The gap between the horizontal dashed and dotted lines give the magnitude of the intrinsic asymmetry ratio for this particular GFA (cf. Fig. 4).

of $\sim 1.2$ in the limit $R_p/R_c^* \gg 1$.

The critical heating rate $R_h^*(R_p)$ at finite $R_p$ can also be calculated from CNT using an expression similar to Eq. 12 with an additional term that accounts for cooling the equilibrated liquid samples to zero temperature at a finite rate. In Fig. 7, we show that the asymmetry ratio $R_h^*(R_p)/R_c^*$ predicted using CNT agrees qualitatively with that from the MD simulations. The number of crystal nuclei that form during the quench increases with decreasing $R_p$, which causes $R_h^*(R_p)/R_c^*$ to diverge as $R_p \to R_c^*$. The predicted intrinsic contribution to the asymmetry ratio for $R_p \sim R_c^*$ is small, and $R_h^*(R_p)/R_c^*$ is dominated by the preparation protocol. In contrast, the asymmetry ratio $R_h^*(R_p)/R_c^* \approx 1.2$ is dominated by the intrinsic contribution in the $R_p \gg R_c^*$ limit. As shown in Fig. 4, the size of the intrinsic contribution to the asymmetry ratio can be tuned by varying the GFA, which controls the separation between the peaks in the nucleation $I(T)$ and growth $U(T)$ rates.

IV. CONCLUSION

We performed MD simulations of binary Lennard-Jones systems to model the crystallization process during heating and cooling protocols in metallic glasses. We focused on measurements of the ratio of the critical heating $R_h^*$ and cooling $R_c^*$ rates, below which crystallization occurs during the heating and cooling trajectories. We find: 1) $R_h^* > R_c^*$ for all systems studied, 2) the asymmetry ratio $R_h^*/R_c^*$ grows with increasing glass-forming ability (GFA), and 3) the critical heating rate $R_h^*(R_p)$ has an intrinsic contribution $R_h^*(\infty)$ and protocol-dependent contribution $R_h^*(R_p) - R_h^*(\infty)$ that increases with decreasing cooling rates $R_p$ used to prepare the initial samples at zero temperature. We show that these results are consistent with the prediction from classical nucleation theory that the maximal growth rate occurs at a higher temperature than the maximal nucleation rate and that the separation between the peaks in nucleation $I(T)$ and growth $U(T)$ rates increases with the GFA. Predictions from CNT are able to qualitatively capture the dependence of the asymmetry ratio on the GFA as measured through $R_c^*$ for both our MD simulations and recent experiments on BMGs as well as on $R_p$ for the MD simulations. Thus, our simulations have addressed how the thermal processing history affects crystallization, which strongly influences the thermoplastic formability of metallic glasses.

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