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Modified Lucas-Washburn theory for fluid filling in nanotubes

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2	Modified Lucas-Washburn Theory for Fluid Filling in
3	Nanotubes
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11	Ultrafast water transport in carbon nanotubes (CNTs) has drawn a great deal of attention in a
12	number of applications, such as water desalination, power generation and biomolecule detection.
13	With the recent experimental advances in water filling of isolated CNTs, the Lucas-Washburn
14	theory for capillary rise in tubes needs to be revisited for a better understanding of the physics and
15	dynamics of water filling in CNTs. Here, the Lucas-Washburn theory is corrected for the
16	hydrodynamic entrance effects and variation of capillary pressure and hydrodynamic properties
17	with the radius and length of CNTs. Due to the large slippage in CNTs, inclusion of the entrance
18	effects is important particularly for the initial stages of filling where a $L \propto t$ scaling, as opposed
19	to $L^2 \propto t$, is observed in our molecular dynamics (MD) simulations. The corrected Lucas-
20	Washburn theory is shown to predict the water filling dynamics in CNTs as observed in MD
21	simulations. With the corrected theory, we achieve a better understanding of capillary rise and
22	water filling dynamics in CNTs.

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Keywords: Capillary Rise, Filling dynamics, Nanopores, Graphene, Carbon Nanotubes, Nanofluidics,
 Water, Hydrodynamics, Slip Length, Viscosity

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27 INTRODUCTION

28 When confined in nanopores and nanochannels, water is found to possess unique properties that differ substantially from those of bulk water^{1,2}. For example, the out of plane dielectric constant 29 of water has recently been observed to be significantly lower, compared to the bulk value, when 30 confined in graphene slit channels^{3,4}. As another example, giant water flow rates have been 31 observed in carbon nanotubes (CNTs) owing to the highly frictionless surfaces⁵⁻⁹. Water transport 32 33 in CNTs has been studied for the past two decades, where enhancement factors (flow rates normalized by the rates predicted using the classical no-slip Hagen-Poiseuille (HP) equation) of 34 the order of 1000 have been reported^{6,10,11}. Recently, Secchi et al.¹² experimentally measured water 35 flow rates in individual CNTs where a massive slip length of ~300 nm was reported for a 15 nm-36 diameter CNT. This massive slip length contradicts the values obtained from the classical 37 molecular dynamics (MD) simulations (usually in the range of 70 nm-120 nm). Secchi et al.¹² 38 suggest that the unique electronic structure of the CNT confinement possibly leads to the 39 observation of the unexpectedly large slip lengths. While electronic structure effects are certainly 40 important in CNTs, the accuracy of the underlying theory used to extract slip lengths from 41 experimental data is also important. Since the hydrodynamic resistance inside CNTs is negligible 42 compared to the entrance/exit resistance, estimation of slip lengths from experimentally measured 43 flow rates strongly depends on the accuracy of the theory used to describe the entrance/exit 44 $flow^{13,14}$. For example, using a corrected Sampson theory¹⁴ to describe the entrance/exit flow, the 45 experimentally measured flow rates by Secchi et al.¹² lead to slip lengths comparable to those 46 obtained from MD simulations. Therefore, the need for accurate theories describing flow in 47 nanopores is of particular interest. Recently, water filling of isolated CNTs has been investigated¹⁵, 48 where the spatial presence of water along a single CNT is reported by a shift in the measured 49

Raman radial breathing modes. Given these advances¹⁵⁻¹⁹, accurate theoretical models are required
for a thorough understanding of the water capillary rise in CNTs from experiments.

52 Dynamics of capillary flow in circular tubes was first investigated within the framework of 53 classical fluid mechanics about a century ago^{20-22} . Edward W. Washburn introduced an equation 54 for fluid meniscus dynamics in the capillary by integrating the HP velocity of penetration equation 55 where the driving pressure on the fluid is set to be the Laplace capillary pressure $\left(\frac{2\sigma cos\theta}{P}\right)$, i.e.,

 $L^2 = \frac{\sigma \cos\theta}{2\mu} (R + 4b)t$

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- 57

where L is the height of the penetrating meniscus, t is the transient time, R is the tube radius, θ is 58 the contact angle of the meniscus with the tube wall, μ is the fluid viscosity, σ is the fluid surface 59 tension and b is the slip length. See Figure 1a for the definition of L, R and θ . Equation (1), 60 61 however, has been found to be inaccurate for some nanoscale flows (e.g., capillary rise in CNTs) possibly due to the deviations of fluid interfacial properties at nanoscale as observed in molecular 62 dynamics simulations²³⁻³⁰. For example, Supple et al.²⁵ found that the Lucas-Washburn (LW) 63 equation in (1) cannot describe capillary filling dynamics in CNTs as the meniscus height is 64 proportional to time $(L \propto t)$ in their simulations. In another MD study²⁴, the filling rate of 65 66 nanotubes was found to be slower than the rate predicted from the LW equation. The slower filling rate was also observed by Martic et al.²⁶ where a velocity-dependent contact angle was introduced 67 to correct the LW equation. Effects of dynamic contact angles, inertia forces, slip lengths, and 68 viscosity variation in gel pores of cement-based materials were also considered in other recent 69 studies^{31,32} for modifying LW equation. Cai et al.^{33,34} provided a comprehensive review on LW 70 equation modifications and extensions for porous media. For nanotubes (e.g., CNTs) with large 71 slip lengths, MD simulations showed that the entrance effects must be considered as the early stage 72

(1)

of filling is dominated by the viscous dissipation at the entrance^{23,27}. Here, we revisit the original 73 Lucas-Washburn equation for water capillary rise in CNTs and account for the hydrodynamic 74 entrance effects by incorporating the recently corrected-Sampson theory into the capillary rise 75 equation. Capillary pressure is also modified for tubes with small diameters as the Laplace 76 capillary pressure is likely to fail for small pores³³. Additionally, we incorporate the variation of 77 viscosity and slip length with radius and length of CNTs. The corrected Lucas-Washburn (CLW) 78 equation is able to describe the filling rate of CNTs from MD simulations where $L \propto t$ and $L \propto \sqrt{t}$ 79 80 laws are observed for short-time and long-time fillings, respectively. Water slip lengths for 81 different sizes of CNTs are also estimated from LW, CLW, and other methods. Unlike those from LW, slip lengths from CLW match the values expected from MD simulations. 82

83 CORRECTED LUCAS-WASHBURN THEORY

Ultrafast water flow inside CNTs has been observed by both experimental and computational studies due to the frictionless nature of the interface^{7,35,36}. This ultralow hydrodynamic resistance inside CNTs leads to the dominance of entrance hydrodynamic resistance for finite-length CNTs. Therefore, the recently corrected Sampson (CS) theory¹⁴ for the entrance resistance is included in the total hydrodynamic resistance as follows:

$$R_{\text{total}} = R_{\text{entrance}}^{\text{CS}} + R_{\text{CNT}}^{\text{HP}}.$$
 (2)

90 where $R_{entrance}^{CS} = \frac{C_{CS} \mu}{2R^3}$ and $R_{CNT}^{HP} = \frac{8\mu L}{\pi (R^4 + 4bR^3)}$ are, respectively, the corrected Sampson 91 resistance for the entrance (excluding the exit resistance by the $\frac{1}{2}$ factor) and Hagen-Poiseuille 92 resistance inside the CNTs. C_{CS} is the pre-factor in the corrected Sampson equation. Values of C_{CS} 93 for different pore radii can be obtained from the expressions given in Ref.¹⁴ where slip lengths 94 inside single-layer graphene nanopores, which appear in the C_{CS} expressions, are also provided. 95 Variation of μ and *b* with the radius and length are considered using the recently corrected HP 96 (CHP) theory presented in Ref.¹³. Total resistance in the left-hand side of equation (2) is obtained 97 from the driving capillary pressure and volumetric flow rate $\left(R_{\text{total}} = \frac{\Delta P}{Q}\right)$. Capillary pressure is 98 given by³⁷

99
$$\Delta P = \left(2 + \frac{\delta r}{r}\right) \frac{\sigma cos\theta}{R}$$
(3)

100 where *r* is the radius of the curvature of the meniscus and δr is an infinitesimal change in the 101 radius. See the Supplementary Information for the derivation of equation (3). For large-diameter 102 tubes, $\frac{\delta r}{r}$ is negligible reducing equation (3) to $\Delta P = \frac{2\sigma cos\theta}{R}$ which is the Laplace capillary pressure 103 used in the original Lucas-Washburn equation. However, for small-diameter CNTs, δr and *r* may 104 be comparable. Therefore, equation (3) is modified as,

105
$$\Delta P = \frac{C_{\rm cp}\sigma cos\theta}{R} \tag{4}$$

where C_{cp} is defined as the capillary pre-factor ($C_{cp} \ge 2$) which changes with pore radius. Note that $C_{cp} = 2$ in the original Lucas-Washburn equation. Here, we model the capillary pre-factor as $C_{cp} = 2 + \left(\frac{0.3 \text{nm}}{R}\right)^{1.6}$, where 0.3 nm indicates the approximate size of a single water molecule and *R* is expressed in nanometers (see the Supplementary Information for more details).

110 Neglecting inertia forces and using equations (2), (4), and $R_{\text{total}} = \frac{\Delta P}{Q}$, the rate of penetration can 111 be written as

112
$$\frac{dL}{dt} = \frac{2C_{\rm cp}\sigma\cos\theta(R+4b)}{\pi C_{\rm CS}\mu(R+4b)+16\mu L}.$$
 (5)

113 Integrating equation (5), the corrected Lucas-Washburn equation is given by

$$t = \frac{\pi C_{\rm cs} \mu}{2C_{\rm cp} \sigma \cos\theta} L + \int_0^L \frac{8\mu(z)z}{C_{\rm cp} \sigma \cos\theta(R+4b(z))} dz \tag{6}$$

115

116 where z is the axial coordinate of the tube as shown in Figure 1a. Previously, it was shown that the slip length varies along the tube b(z) for very short CNTs¹³. Assuming a constant slip length, 117 constant viscosity, a C_{cp} pre-factor of 2 and neglecting the first term, equation (6) reduces to the 118 original LW equation (see equation (1)). The first term in equation (6) is due to the entrance effects 119 and follows the $L \propto t$ scaling which was observed in some previous studies. The $L \propto t$ scaling 120 dominates the filling dynamics for short-time (or short-length) filling. For long-time (or long-121 122 length) filling, the second term in equation (6) dominates the filling. Assuming a constant slip 123 length b and viscosity μ for long-time filling, the first term in equation (6) (entrance effects) can be neglected for $L \gg \frac{\pi C_{cs}}{8}(R+4b)$ where the filling dynamics follows $L \propto \sqrt{t}$ scaling. The 124 condition reduces to $L \gg \frac{\pi C_{cs}}{2} b$ for small-radius CNTs as the slip length is much larger than the 125 radius $(b \gg R)$. 126

127 WATER STRUCTURE AND DYNAMICS OF FILLING FROM MD SIMULATIONS

All-atom MD (AAMD) simulations have been performed to study the structure and dynamics 128 of capillary rise in CNTs. As shown in Figure 1b, each simulation box consists of water molecules, 129 130 a graphene sheet at the entrance and a CNT. In each graphene sheet, a nanopore with a size similar to the diameter of the CNT is drilled. (10,10), (14,14), (18,18), (26,26) and (34,34) CNTs with the 131 center-to-center diameters of 1.36 nm, 1.90 nm, 2.44 nm, 3.53 nm and 4.61 nm are considered in 132 this study. The simulation box dimensions vary from 6.3 nm to 20.01 nm in x and y, and 100 nm 133 to 400 nm in z. Different dimensions in x and y are used to account for the porosity of the nanopores 134 (the ratio of pore area to membrane area is < 0.042). The systems contain about 326,000-783,000 135

atoms of which about 200,000-300,000 atoms are the reservoir water molecules initially placed
next to the graphene sheets. Note that the schematic of the simulation box in Figure 1b is truncated
for a better presentation. See the Methods section and Supplementary Information, for more details
about MD simulations.

Water contact angles are calculated geometrically from the MD simulations by first obtaining 140 the water densities averaged for different rectangular slabs placed in each CNT³⁸⁻⁴⁰ (see the 141 142 Supplementary Information). The region with the sharp reduction in density indicates the boundary of the meniscus (liquid-vapor interface). The cosine of the contact angles are reported for different 143 144 CNT radii in Figure 2a. The cosine of the contact angles increases with increasing radius from $0.125 \ (\theta = 82.8^{\circ})$ for the (10,10) CNT to $0.180 \ (\theta = 79.6^{\circ})$ for the (34,34) CNT. For very large 145 radii, the cosine of the angles is expected to converge to that of the limiting case of a single-layer 146 graphene (0.53 or $\theta = 58^{\circ}$) for the carbon-water interaction parameters³⁸ employed in this study 147 (see the methods section). As the contact angle increases for smaller radii, the surface becomes 148 149 more hydrophobic due to the enhanced confinement in smaller CNTs.

150 In Figure 2b, normalized water density as a function of the normalized radial distance from the 151 CNT center is plotted for the different CNTs considered in this study. Water density layering is observed near the wall of CNTs where the density can reach about 3 times the bulk water density. 152 Water density reaches that of the bulk water in the center of CNTs except for the small CNTs (e.g., 153 154 (10,10) CNT) where the density layering regions are overlapped with no bulk-like region. The 155 velocity distribution in the radial direction (Figure 2c) exhibits plug-like flow profiles with velocity 156 jumps at the interfacial region of CNTs. These velocity profiles are similar to flow profiles 157 observed in pressure driven flows. In Figure 2c, one might argue that the velocity should increase 158 for smaller radii as the slip length is larger. Although this may be true for pressure-driven flows

(assuming a fixed external pressure for all radii), it is not the case here since the capillary pressure decreases for small radii (e.g., velocities in (14,14) and (10,10) CNTs are lower than those of other larger CNTs). This can also be confirmed by examining equation (5) where the penetration velocity decreases with decreasing $\cos \theta$ for small radii.

163 DYNAMICS OF FILLING FROM THE CORRECTED LUCAS-WASHBURN THEORY

Extensive MD simulations have been carried out to report the penetration length of the meniscus 164 as a function of simulation time for all CNT sizes considered in this study (see Figure 3). Since 165 166 the simulations involve a large number of atoms and the capillary rise is a slow process, simulating filling dynamics is limited to filling lengths of about 45 nm-150 nm depending on the diameter of 167 the CNTs. The MD results are used as the reference to examine the accuracy of the corrected model 168 169 (equation (6)) compared to the original LW theory (equation (1)). As mentioned in the previous sections, slip length and viscosity for the CLW equation are obtained from Ref.¹³ where the 170 variation of viscosity $\mu(L, R)$ and friction coefficient $\lambda(L, R)$ with length and radius of CNT are 171 given. Slip length can simply be obtained from $\overline{b}(L, R) = \frac{\mu(L, R)}{\lambda(L, R)}$. For a given radius, $\overline{b}(L)$ is a CNT 172 173 length-averaged slip length (considering that slip length in the entrance region of the CNT differs from that of the middle section of the CNT). However, slip length at a given point along the CNT, 174 b(z), is required in equation (6). Therefore, we discretize the entire length of the CNT with a 175 uniform mesh, $z_n = \frac{\text{Total length}}{N}n$ and n = 1, 2, ..., N. The slip length at any point z_n can then be 176 written as $b_n = n\overline{b}_n - (b_1 + b_2 + \dots + b_{n-1})$ for $n \ge 2$. $b_1 = \overline{b}_1$ for n = 1. The same can be 177 applied to the viscosity inside the CNTs. However, as discussed in the Supplementary Information, 178 we observed that the length-variation of viscosity does not significantly change the filling 179 180 dynamics (i.e., for simplicity, one can use the values of water viscosity for an infinity-long CNTs).

181 The corrected Sampson pre-factor is given in Ref.¹⁴ as it changes depending on the radius and 182 slippage at the graphene nanopore. The surface tension of water is taken to be 0.072 N/m. Capillary 183 pre-factor for different CNTs is obtained from $C_{cp} = 2 + \left(\frac{0.3 \text{nm}}{R}\right)^{1.6}$. Note that for $R > \sim 1$ nm, 184 we can simply use a constant pre-factor $C_{cp} = 2$ (see the Supplementary Information). All the 185 parameters used in equation (6) are tabulated in TABLE 1.

As shown in Figure 3, the CLW theory is able to match the meniscus penetration displacement 186 with time obtained from MD simulations. The initial filling of CNTs follows a nearly linear 187 scaling, $L \propto t$, indicating the importance of accounting for the entrance effects in the model. 188 However, one should note that the filling dynamics cannot be approximated solely by the Sampson 189 equation (entrance resistance) as suggested by Gravelle et al.²³ since the dependence of L on t190 starts to deviate from the $L \propto t$ scaling in the subsequent stages of filling (Figure 3 and Figure S8 191 192 of the Supplementary Information). The LW theory, where a constant slip length is assumed in equation (1), fails to predict the filling dynamics in CNTs mainly because the entrance effects are 193 ignored (the filling dynamics always obeys the $L^2 \propto t$ law in LW theory). For long-length or long-194 time filling where the entrance effects can be ignored (e.g., for lengths much larger than $L \gg$ 195 $\frac{\pi C_{cs}}{2}b = 102$ nm in (10,10) CNTs), CLW and LW result in similar filling dynamics assuming that, 196 in the LW equation, slip length and viscosity for infinitely long CNTs, contact angles from MD 197 simulations, and modified capillary pre-factors for small-diameter CNTs are considered (see 198 Supplementary Information). 199

200 PREDICTING SLIP LENGTHS FROM FILLING DYNAMICS IN CNTS

Accurate estimation of slip lengths in CNTs from the experimentally measured flow rates is of particular interest in the nanofluidic community. Lack of accurate theories (Sampson and HP 203 theories) has been suggested as one of the possible explanations for the estimated giant slip lengths from the experimental pressure-driven flow rates reported by Secchi et al¹². Recently, with the 204 advances in detecting water molecules spatially along isolated CNTs¹⁵, dynamics of capillary rise, 205 206 obtained from experiments, could potentially be used to estimate the slip lengths of water in CNTs. Slip lengths can be determined from LW and CLW theories (equations (1) and (6)), given that the 207 208 filling rates are available from experiments or computational simulations. For the CLW theory, the CNT-length dependent slip length b(z) can be solved for numerically by using a uniform mesh 209 210 along the CNT. In Figure 4, slip length as a function of CNT radius for different CNT lengths is 211 plotted from different theories, simulations, and experiments. The corrected HP theory, which is based on MD simulations, is used to generate the reference slip length data. Flow rates from the 212 CHP theory have been shown to compare well with the rates from MD simulations and 213 experiments in the previous study¹³. The filling dynamics in Figure 3 is used to predict the slip 214 lengths from LW and CLW theories for the CNT radii considered in this work. As expected, the 215 216 slip lengths from the CLW theory follow the trend obtained from the CHP. The original LW theory underestimates the slip lengths for short and small-radius CNTs. This is because entrance effects, 217 218 viscosity variation with CNT size and capillary pre-factor variation with radii are important for 219 shorter and smaller CNTs. The slips lengths from LW and CLW theories, however, become comparable for longer and larger-diameter CNTs. Most of the slip length measurements from 220 221 experiments and simulations are for μ *m*-long and infinitely-long CNTs. The estimated slip lengths are widely scattered where the slip lengths range from ~10 nm to 450,000 nm. These discrepancies 222 223 are possibly due to the inaccurate theories used to estimate slip lengths, lack of accurate forcefields 224 for the interaction between water and CNTs, challenging experimental flow rate measurements and effects of defects and contaminants in experiments. We should note that we used the force-225

field developed by Wu et al.³⁸ which results in comparable water contact angles on graphene with
the experimental values.

228 CONCLUSION

The Lucas-Washburn theory was revisited and corrected for the hydrodynamic entrance effects 229 and variation of capillary pressure and hydrodynamic properties for nanometer scale pores. The 230 effect of the entrance resistance, modeled by the corrected Sampson theory¹⁴, is important for 231 initial stages of filling (i.e., short-time or short-length filling) as well as for tubes with large slip 232 lengths. The capillary pressure is predicted to decrease slightly as radius of CNTs decreases 233 (nanometer-radius CNTs). Effect of the variation of viscosity and slip length on filling dynamics 234 is significant for short and small-radius CNTs. The corrected theory is able to predict the water 235 filling dynamics in CNT from MD simulations. For the initial stages of filling, a $L \propto t$ scaling is 236 observed due to the effects of the entrance resistance. $L^2 \propto t$ scaling is expected for long-length or 237 238 long-time stages of filling similar to the filling dynamics obtained from the original Lucas-Washburn theory. 239

240 METHODS

MD simulations were carried out using the LAMMPS package.⁴¹ The features of simulation boxes (Figure 1b) were discussed in the Water Structure and Dynamics of Filling from MD Simulations section. We used the SPC/E water model and the SHAKE algorithm to maintain the rigidity of the water molecule. The interactions between carbon atoms and water molecules were modeled by the force-field parameters given in Wu *et al.*³⁸ The carbon atoms are frozen in space. We note that freezing the carbon atoms can affect the flow rates up to 10%-20% ^{7,42}. The LJ cutoff distance was 12 Å. The long range electrostatic interactions were computed by the Particle-

Particle-Particle-Mesh (PPPM) method.⁴³ Periodic boundary conditions were applied in all the 248 three directions. In the z direction, the simulation box is separated from its images by large vacuum 249 regions (see the Supplementary Information). For each system, the energy of the system was first 250 251 minimized for 10000 steps. Next, the water reservoir was equilibrated using NPT ensemble for 1 ns at a pressure of 1 atm and a temperature of 300 K with a time-step of 1fs. The NPT simulations 252 allow the water molecules to reach the bulk water equilibrium density (1 g/cm³). Then, NVT 253 simulations were performed for 2 ns to further equilibrate the systems. Temperature was 254 maintained at 300 K by using the Nosè-Hoover thermostat with a time constant of 0.1 ps.^{44,45} In 255 the equilibrium simulations, a graphene sheet with no pore is used to solely equilibrate water 256 molecules without penetrating the tube. The final production simulations were performed in NVT 257 ensemble for up to 12 ns to study the capillary rise in CNTs. 258

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Figure 1. a) Schematic of capillary filling of a CNT is shown. Radius (*R*), water contact angle (θ) and filling length (*L*) of the CNT are illustrated. *z* is the axial coordinate along the CNT. The CNT and graphene walls are shown in cyan and water is shown in light blue. **b**) A typical simulation system for a (26,26) CNT (*R*=1.76 nm) is shown for the simulation time of ~1 nanosecond. The carbon, oxygen and hydrogen atoms are presented in cyan, red and white, respectively. The simulation box is truncated for a better presentation.



320 Figure 2. a) Cosines of water contact angles for the different CNTs considered in this study. The cosine of 321 contact angle increases with increasing radius. It is expected to reach the cosine of contact angle on a flat 322 graphene for very large CNT radii. b) Water density distribution (normalized by the bulk water density) in 323 the radial direction (normalized by the CNT radius) for the different CNTs considered in this study. c) Axial 324 velocity of water molecules as a function of the normalized radial distance from the center of CNTs. The 325 water velocity is calculated for the CNT filling in the time interval of 1900ps-2100ps. For both density and 326 velocity calculations, we consider the water molecules that are 1 nm away from the pore entrance and 327 the meniscus surface

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Figure 3. The length of the CNTs filled with water as a function of time from all-atom MD simulations is compared with the filling lengths predicted by the corrected Washburn (CLW) theory and the original

360 Washburn (LW) theory for a) (10,10), b) (14,14), c) (18,18), d) (26,26), and e) (34,34) CNTs. The corrected 361 Washburn theory is able to describe the filling dynamics well compared to that of the AAMD simulations. 362 The original Washburn theory, however, fails as it does not account for the hydrodynamic entrance effects, slip length and viscosity variations with CNT length and radius, as well as the corrected capillary 363 364 pressure in nanometer-diameter CNTs. In the original LW theory, viscosity is taken as 0.85 mPa·s which is the water bulk viscosity. The slip length in the original LW theory is chosen such that we obtain the best 365 possible match with the data from MD simulations. We note that slip lengths based on infinitely-long CNTs 366 367 lead to a massive overestimation of filling rates by the original LW theory (see Figure S8a of the 368 Supplementary Information).

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Figure 4. Slip lengths as a function of radius of CNTs with different tube lengths predicted by different theories (corrected Hagen-Poiseuille theory (CHP, blue curve), corrected Lucas-Washburn theory (CLW, filled black symbols) and original Lucas-Washburn theory (LW, hollow black symbols)). The CHP model, which is based on MD simulations, is used as the reference here. The LW theory fails to predict the slip lengths for short and small-radius CNTs. As both length and radius increase, LW and CLW theories result in identical slip lengths since the effects of hydrodynamic entrance, viscosity variation and nano-capillary pressure vanish. Experimental^{5,6,46} and computational^{7,35,47-50} data (shown by red and green symbols, respectively) shows how wide the range of slip lengths are in the literature. In other notable experiments by Majumder et al⁵. and Du et al⁵¹. (not shown in the Figure), very high slip lengths of 39000nm-68000nm and 485000nm are reported, respectively.

408	Cases	C _{CS}	C _{cp}	σ (N/m)	cosθ
409	(10,10) CNT	0.465	2.27	0.072	0.125
410	(14,14) CNT	0.480	2.15	0.072	0.139
	(18,18) CNT	0.495	2.10	0.072	0.158
411	(26,26) CNT	0.630	2.05	0.072	0.172
412	(34,34) CNT	0.780	2.03	0.072	0.180

TABLE 1 The parameters used in the CLW model (equation (6)) for different CNT sizes. Slip length and
 407 viscosity vary along the tube length. The resulting filling dynamics are plotted in Figure 3.

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