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Framework for performance forecasting and optimization of CMB B-mode observations in presence of astrophysical foregrounds

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We present a formalism for performance forecasting and optimization of future CMB experiments. We implement it in the context of nearly full sky, multi-frequency, B-mode polarization observations, incorporating statistical uncertainties due to the CMB sky statistics, instrumental noise, as well as presence of the foreground signals. We model the effects of a subtraction of these using parametric maximum likelihood technique and optimize the instrumental configuration with pre-defined or arbitrary observational frequency channels, constraining either a total number of detectors or a focal plane area. We showcase the proposed formalism by applying it to two cases of experimental set-ups based on the CMBpol and COrE mission concepts looked at as dedicated B-mode experiments. We find that if the models of the foregrounds available at the time of the optimization are sufficiently precise, the procedure can help to either improve the potential scientific outcome of the experiment by a factor of a few, while allowing to avoid excessive hardware complexity, or simplify the instrument design without compromising its science goals. However, our analysis also shows that even if the available foreground models are not considered to be sufficiently reliable, the proposed procedure can guide a design of more robust experimental set-ups, which while better suited to cope with a plausible greater complexity of the foregrounds than that foreseen by the models, could ensure the science results close to the best achievable, should the models be found to be correct.

I. INTRODUCTION

Cosmic Microwave Background (CMB) B-mode polarization offers some of the most exciting goals for the next stage of observational and experimental effort in cosmology. These goals are already aimed at by an entire slew of current, forthcoming, and planned CMB observations, e.g., [1–5]. Probably most importantly, CMB B-mode measurements could open up a window, as direct as likely ever possible, onto the physics of the very early Universe, giving us unique insights on the physical laws governing at the highest energies. Such outstanding, anticipated consequences seem to be however matched by difficulties, which need to be overcome, first, to deliver an incontrovertible, reliable detection and sufficiently precise characterization of the primordial B-mode signal, and later to interpret it. The obstacles are of fundamental and instrumental origins and stem from the fact that the anticipated B-mode amplitudes are expected to be nearly

two orders of magnitude below those of CMB E-mode polarization and up to 10 times lower than the B-mode signal generated by the Galactic foregrounds. To meet and successfully address such a challenge progressively more sophisticated and advanced observatories have to be devised and built. Their complexity results in a number of design choices and decisions instrumental teams have to make in the course of their development. As those have often a direct impact on the science output of the instrument, this is the latter, which should drive the decision-making process. Though such a situation is by far not new, the sheer size, complexity, and precision of the modern instruments and data sets call for novel, more robust ways of addressing the instrumental optimization problem.

In this paper we propose a general, methodological framework for the experiment optimization and then apply it in specific cases of CMB B-mode observatories. We note that however sophisticated an adopted optimization procedure may be, it is likely to always come up short in giving justice to all the complexity of an instrument under considerations. The goal of such a procedure, as we pursue here, is therefore not just to find a single best, in some sense, instrumental configuration, but rather to provide, on the one hand, a reference against which to

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judge actual hardware designs and, on the other, guidelines of, first, how to propose, given some science goals, a suitable and viable experimental design and, later, how to modify it to implement inevitable, real-life limitations and constraints in a way, which will have a minimal impact on its scientific performance.

Though the discussed formalism lends itself straightforwardly to a number of generalizations, in this paper we demonstrate it in the context of the B-mode detection by multi-frequency observatories taking into account presence of the astrophysical (diffuse) foregrounds, leaving a study of some of the most common instrumental effects to a future work. We note that even in this limited context a result of the instrument optimization problem will depend on a number of factors: scientific goals as set for the experiment in question, models of the physical effects, e.g., foregrounds, specific techniques, and assumptions they require, selected to be used for component separations step. This emphasizes the need for using the state-of-the-art physical models of the foregrounds and the separation techniques in this kind of problems, as well as for continuing effort aiming at better, more reliable understanding of the foreground physics.

As the optimization requires a capability to predict the performance of an instrument given its characteristics it is very closely connected with performance forecasting. In fact, in most of the similar work to date, the problem of selecting the most suitable experimental configurations is typically treated as a performance forecasting problem applied to some pre-defined, and limited, set of potential candidate experimental set-ups, relative merits of which are subsequently evaluated and compared, e.g., [6–11]. This is in contrast with this paper, which employs an actual optimization procedure. In this respect our approach is most similar to the one by Amblard et al. [12]. Here we generalize and extend the latter work on both methodological and implementation levels. We consider broader parameter space and optimization strategies, search for families of acceptable configurations, and by adopting the parametric component separation approach as the component separation technique of the choice, we manage to propagate realistic ensemble-averaged errors to our selected figure of merit indicators in a statistically sound manner.

The paper is organized as follows. In the next Section we first describe a general framework of our approach and then specialize it to our specific science case of CMB B-mode observations. In that Section we show how the parametric component separation technique can be used to assess the performance of CMB experiments in the presence of galactic foregrounds, developing the approach to a performance forecasting in such cases. In Sect. III we detail the foreground model we use in this work. Section IV describes applications of the proposed formalism to two fiducial satellite experiments, based on the CMBpol [4] and CORe [3] proposals. In Sect. V we present our conclusions. Some of the lengthy calculations are collected in Appendices A and B.

II. METHOD

Our approach is as follows. We start off from expressing our science goals in terms of acceptable ranges of values of some proposed figures of merit, hereafter FOM, (Sect. IIB), which are chosen to reflect the physical context of the considered experiment. We then first treat all FOMs separately and for each of them perform a strict optimization procedure (Sect. IIC), i.e., minimize or maximize it over a set of considered instrumental parameters. This is usually done in presence of some external constraints arising for instance due to some hardware requirements but also some other science-driven restrictions, (Sect. IIC). This first step aims at determining the best possible instrument performance from the perspective of the considered FOM and their corresponding configurations. If for any of the FOM the best performance value does not fulfill our science goals, the procedure halts and either the set of instrumental parameters have to be enlarged or the science goals/FOMs rethought. Otherwise, for each FOM, but one, we select a threshold value, which need to be attained by any acceptable configuration and perform the optimization of the one left-over FOM over the parameter space under additional constraints, requiring that all or some of the remaining FOMs are not worse than their established thresholds. If the optimization fails, we may need to adjust some of the thresholds and repeat the procedure again. This may be also the case if the solution found does not ensure an acceptable value for the FOM, which is used in the optimization. If the tuning of the thresholds succeeds, the solution obtained via the above procedure is used as a starting point for further post-processing and the corresponding set of values of all FOMs used as a reference to compare any other configuration against. The post-optimization processing is used to implement some additional constraints and/or simplifications, which for some reason could not have been imposed on the formal optimization procedure.

Below we present a specific implementation of this general framework in the context of primordial CMB B-mode observations by multi-frequency multi-detector observatories in the presence of Galactic foregrounds. In this case our FOMs need to account for some effects arising due to the component separation procedure, which has to be applied to data to recover a genuine CMB signal. We therefore start below from discussing a specific component separation approach, so called parametric maximum likelihood technique, and its impact on a CMB B-mode detection.

A. Effects of foreground separation

An estimation of the presence of the foregrounds involves two main steps. On the first step, we estimate the error incurred while constraining the spectral parameter values from the data. on the second, we translate

that error into some figures of merit expressing the overall quality of the separation process and which are then used in our optimization procedure.

1. Formalism

Hereafter we use the parametric maximum likelihood component separation approach implemented as in [13]. We thus assume a linear data model, where a signal measured in each pixel p is given by,

$$\mathbf{d}_p = \mathbf{A} \mathbf{s}_p + \mathbf{n}_p, \quad (1)$$

where for each pixel p ,

- \mathbf{d}_p is a multi-frequency data vector with each entry corresponding to a different frequency channel;
- \mathbf{s}_p is a multi-component sky signal vector each entry of which corresponds to a different sky component and which is to be estimated from the data;
- \mathbf{A} is a mixing matrix defining how the components need to be combined to give a signal for each of the considered frequency channels;
- \mathbf{n}_p is a vector containing the instrumental noise and assumed to be Gaussian and uncorrelated with a dispersion given by \mathbf{N} .

Here both \mathbf{A} and \mathbf{N} are assumed to be pixel independent for simplicity, with an exception of Sect. IV D 7.

In the parametric approach, one assumes that \mathbf{A} is parametrized by a set of spectral parameters, β , which need to be determined together with the sky signal estimates. The noise level per channel, number of frequency channels, etc are all dependent on instrument properties, which thus will affect the results of the component separation process and could therefore serve as optimization parameters. Some other effects such as calibration, beam-sizes, band-widths are also typically relevant and may need to be included in the modeling, as even if not necessarily an object of the optimization could affect its outcome. We leave a thorough evaluation of those effects for future work, while neglecting them in this paper.

Given values of β and defined instrumental parameters we can estimate the component signal using a standard Maximum Likelihood solutions,

$$\mathbf{s}_p \equiv (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \mathbf{A} \mathbf{N}^{-1} \mathbf{d}_p. \quad (2)$$

To estimate the spectral parameters we will use a pseudo (or profile) likelihood [13] given as,

$$-2 \ln \mathcal{L} = - \sum_p (\mathbf{A} \mathbf{N}^{-1} \mathbf{d}_p)^t (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \mathbf{A} \mathbf{N}^{-1} \mathbf{d}_p. \quad (3)$$

We will refer to this likelihood as the spectral likelihood and will identify its peak value with the best estimate of the spectral indices and the curvature matrix at its peak as the measure of the uncertainties expected for the spectral parameter estimation. These will be used to construct our figures of merit.

2. Spectral parameter uncertainty

The profile likelihood derivatives with respect to the spectral parameters can be readily computed and the relevant formulae are collected in Appendix A. As our purpose is to gain some insight in the constraining power of different plausible experimental set-ups rather than analyze any specific data set we will average over the possible noise realization assuming that the noise correlation matrix, \mathbf{N} , is known. Using Eq. (A1) from the Appendix we then arrive at,

$$\left\langle \frac{\partial \ln \mathcal{L}}{\partial \beta} \right\rangle_{noise} = \sum_p (\mathbf{A}_{,\beta} \bar{\mathbf{s}}_p)^t \mathbf{N}^{-1} (\hat{\mathbf{A}} \hat{\mathbf{s}}_p - \mathbf{A} \bar{\mathbf{s}}_p) \quad (4)$$

for the first derivative. In this equation, as well as everywhere hereafter, we will use a hat over a quantity to mark that we refer to its true, rather than just an estimated value. $\bar{\mathbf{s}}$ is a sky signal estimate in the case of the noiseless data and it is defined in Eq. (A7). If the data model in Eq. (1) is correct both in terms of assumed scaling laws but also a number of components, the first derivative in Eq. (4) vanishes for the true values of the parameters, $\beta \equiv \hat{\beta}$, emphasizing that the estimator is on average unbiased. Indeed in such a case we have $\hat{\mathbf{A}} = \mathbf{A}$ and $\bar{\mathbf{s}} = \hat{\mathbf{s}}$. Under the same assumptions the second order derivatives taken at the true values of the parameters can be then written as, see Eq. (A10),

$$\left\langle \frac{\partial^2 \ln \mathcal{L}}{\partial \beta \partial \beta'} \right\rangle_{noise} \Big|_{\beta=\hat{\beta}} = \text{tr} \left\{ \left[\mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \mathbf{A} (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \mathbf{A}^t \mathbf{N}^{-1} \mathbf{A}_{,\beta'} - \mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \mathbf{A}_{,\beta'} \right] \sum_p \hat{\mathbf{s}}_p \hat{\mathbf{s}}_p^t \right\}. \quad (5)$$

Hereafter we will use the inverse of this matrix to approximate the error matrix, Σ , for the recovered scaling

parameters, i.e.,

$$[\Sigma^{-1}]_{\beta\beta'} \simeq - \left\langle \frac{\partial^2 \ln \mathcal{L}}{\partial \beta \partial \beta'} \right\rangle_{noise} \Big|_{\beta=\hat{\beta}}. \quad (6)$$

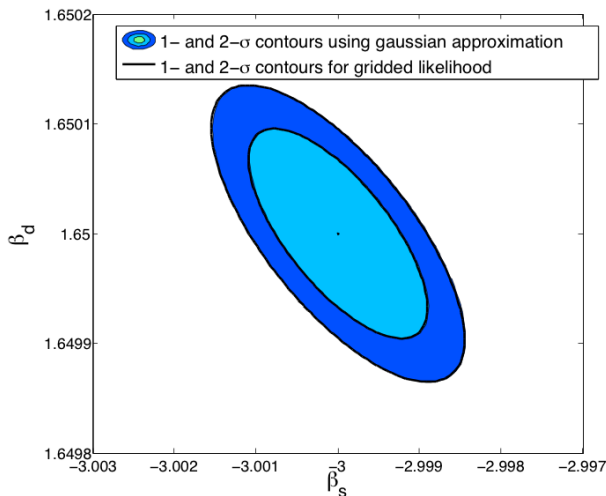


FIG. 1: 1- and 2- σ contours in the $\beta_{dust} - \beta_{sync}$ space of the spectral likelihood, \mathcal{L} , calculated using Eq. (3) for a random realization of the CMB and noise contributions, shaded areas, and compared against the Gaussian approximation with a dispersion as given by Eq. (5), solid lines. The former likelihood has been recentered at the true values of the parameters.

We note that the spatial morphology of the sky components enter the calculation of the errors only in a form of pixel averaged correlations,

$$\hat{\mathbf{F}} \equiv \frac{1}{N_{pix}} \sum_p \hat{\mathbf{s}}_p \hat{\mathbf{s}}_p^t. \quad (7)$$

Moreover, only those of the columns and rows of this correlation matrix matter, which correspond to sky components characterized by the scaling laws including some unknown parameters. Mathematically, this just follows from the fact that only columns of the derivatives of the mixing matrix, \mathbf{A}_β , corresponding to such components do not vanish. Physically, this indicates that the components for which the scaling laws are known unambiguously, e.g., CMB, are subtracted cleanly during the separation process and do not affect the result of spectral indices estimations. The immediate consequence of this is that though the averages taken, while deriving Eqs. (4) and (5) were formally performed only over an ensemble of different noise realizations, the resulting expressions are indeed equivalent to those obtained while averaging over an ensemble of realization of noise and CMB signal.

We note that though our conclusion about the impact of different components on the spectral parameter estimation is general, a simple form of the dependence of the latter on the foreground signal morphology is due to our simplifying assumption of a pixel-independent noise level. In general, the relation is more complex, with noise levels selective (de)emphasizing the contributions of some of the pixels on the sky. Though the formalism developed here is general and can be straightforwardly adopted to a case of arbitrary and correlated noise it can quickly become computationally heavy. We will therefore leave a

discussion to more complex and realistic cases for future work.

In Fig. 1 we show examples of the contours likelihoods, Eq. (3), computed for dust and synchrotron spectral indices for simulated data as described in Sect. III and for some fiducial nearly full sky experiment. They are compared with a Gaussian approximation based on the variance derived with help of the error matrix, Eq. (6). Generally we find a very good agreement. This may breakdown somewhat in cases with very few pixels when the actual spectral likelihoods typically become somewhat skewed [13]. Nevertheless, we find that even in those cases though the Gaussian approximation may fail to reproduce properly the tails of the distributions, its overall performance is still rather good. In applications of interest for this paper a sufficient number of pixels is always granted.

An interesting question is then how the precision of the spectral parameter estimation depends on the matrix $\hat{\mathbf{F}}$. The short answer is that given the noise levels the higher density contrast of the components, i.e., larger diagonal elements of $\hat{\mathbf{F}}$, the better precision of estimated β , while large cross-correlation terms tend to increase the error.

3. Residuals

From the discussion in the previous section it is clear that the precision of the spectral parameters determination though relevant is clearly not a single factor important in quantifying the component separation effects on the B-mode science. This is due to the fact that better precision is usually related to a higher foreground contrast and vice versa making it not straightforward to infer an effective foreground contribution left over in the CMB map after the separation process, given just the spectral indices errors. However, given the estimated value of the spectral parameters, β , we can always calculate the level of the foreground residuals, i.e., a mismatch between the estimated and true sky components. This can be expressed as follows [10],

$$\Delta = \mathbf{s} - \hat{\mathbf{s}} = (\mathbf{Z}(\beta) - \mathbf{I}) \hat{\mathbf{s}}, \quad (8)$$

where

$$\mathbf{Z}(\beta) \equiv (\mathbf{A}^t(\beta) \mathbf{N}^{-1} \mathbf{A}(\beta))^{-1} \mathbf{A}^t(\beta) \mathbf{N}^{-1} \mathbf{A}(\hat{\beta}), \quad (9)$$

\mathbf{I} is a unit matrix and as usual a hat over a quantity denotes its true underlying value.

The foreground residuals left in the CMB map are just one component of the vector, Δ , which for definiteness is assumed to be the 0th one. We will now restrict ourselves to the CMB component and linearize the problem, assuming that the errors in spectral parameter determination are small. We thus obtain,

$$\Delta^{\text{CMB}} = \sum_{k,j} \delta\beta_k \alpha_k^{0j} \hat{\mathbf{s}}^j, \quad (10)$$

where

$$\alpha_k^{ij} \equiv \frac{\partial \mathbf{Z}_{ij}(\hat{\beta})}{\partial \beta_k}, \quad (11)$$

and we assumed that the CMB component is stored as first (i.e., with an index equal to 0) in the component vector, \mathbf{s} . We can now characterize the level of the residuals either simply by its *rms* value or, in a more informative way we can estimate the noise average (though noiseless) foreground residual power spectrum, which reads,

$$\mathbf{C}_\ell^\Delta \equiv \sum_{k,k'} \sum_{j,j'} \Sigma_{kk'} \alpha_k^{0j} \alpha_{k'}^{0j'} \hat{\mathbf{C}}_\ell^{jj'}. \quad (12)$$

Given that as mentioned before (see also, [10]) no CMB signal is left in the CMB map residuals, which combine just the foreground signals, the noise ensemble averages coincide with those made over full CMB+noise set of realizations. Clearly to compute the residual spectra we need to make assumptions concerning the spatial morphology of the considered foregrounds, i.e., the knowledge beyond the $\hat{\mathbf{F}}$ matrix defined earlier. This is reflected in Eq. (12) by the presence of true auto- and cross- spectra for each considered foregrounds, $\hat{\mathbf{C}}_\ell^{jj'}$. However, the $\hat{\mathbf{F}}$ matrix provides a sufficient description necessary to calculate the rms value of the residuals. This can be seen noting that,

$$\Delta_{rms}^{\text{CMB}^2} = \sum_{k,k'} \sum_{j,j' \neq 0} \Sigma_{kk'} \alpha_k^{0j} \alpha_{k'}^{0j'} \hat{\mathbf{F}}_{jj'}. \quad (13)$$

In the following we will use the C_ℓ^Δ quantity to construct our FOMs making some specific assumptions about the foregrounds spatial properties as described in Sect. III. We point out that the formulae presented above are just a special case of those already studied in [10]. The important difference is however that the spectral indices uncertainties used in this work are computed effectively as the full CMB+noise, ensemble averages rather than derived in a single, particular study case as in that previous work.

B. Figures of merit

Given the estimates of the foreground residuals provided in the previous Section, we can now define our figures of merit. Hereafter, we will use three FOMs: two referring to the effects of the foreground residuals found in the recovered CMB map as a consequence of the separation process, and the third related to the noise level of that map. As our scientific goals here are related to the primordial B-mode signal two of the proposed FOMs express the effects of the foreground residuals on a tensor-to-scalar ratio (of the respective CMB spectra), r . The third one is more generic and is just to ensure that the least-noisy map of the sky is produced.

a. FOM#1: r_{stat} – an r value detectable on 95% confidence level incorporating the component separation uncertainties.

This FOM is computed in two steps. First, we use a generalized Fisher matrix expression to estimate the uncertainty of estimating the tensor-to-scalar ratio, r , for any given assumed r value, and subsequently we determine a value of $r \equiv r_{stat}$, which is detectable on 95% confidence level. This limiting value is defined as,

$$r_{stat} \simeq 2 F_{rr}^{-1/2} (r_{stat}). \quad (14)$$

The Fisher matrix we propose to use here accounts for usual cosmic, sampling, and noise variance, but also for an extra error resulting from the shortcomings of the foreground component separation, which is presumed to be applied to the maps beforehand. We model the separation residuals following the formalism introduced in Sect. II A 3 and which treats the map-level residuals as a linear combination of the foreground templates with Gaussian distributed amplitudes.

The detailed derivation of the Fisher formula is presented in Appendix B. Recalling that C_ℓ^Δ denotes the power spectrum of the residuals, the final expression for the Fisher matrix, F_{rr} , reads then,

$$F_{rr} = \sum_{\ell, \ell'}^{\ell_{max}} \frac{\partial C_\ell}{\partial r} \left\{ \frac{(2\ell+1) \delta_{\ell\ell'}}{2 f_{sky}^{-1} C_\ell^2} - \frac{(2\ell+1) C_\ell^{-3} C_\ell^\Delta \delta_{\ell\ell'}}{\left(1 + \sum_{\ell''}^{\ell_{max}} (2\ell''+1) \frac{C_{\ell''}^\Delta}{C_{\ell''}}\right)} + \frac{(2\ell+1) (2\ell'+1) C_\ell^\Delta C_{\ell'}^\Delta}{2 C_\ell^2 C_{\ell'}^2 \left(1 + \sum_{\ell''}^{\ell_{max}} (2\ell''+1) \frac{C_{\ell''}^\Delta}{C_{\ell''}}\right)^2} \right\} \frac{\partial C_{\ell'}}{\partial r} \quad (15)$$

where for shortness we set $C_\ell \equiv C_\ell^{\text{CMB}} + C_\ell^{\text{noise}}$.

A choice of experimental parameters will in general affect both the noise level as quantified by C_ℓ^{noise} but also the level of residuals resulting in different r_{stat} values

derived for different proposal configurations.

We note that if the level of residuals is very high as a result of the errors on spectral parameters being large then the first order expansion used to obtain Eqs. (10) & (12)

may not be any more sufficient. Likewise, if the foreground contributions are large so their residuals are comparable to the CMB signal, sufficiently precise knowledge of the foregrounds would become necessary to ensure that the above formulae produce reliable results. As one may not be completely comfortable with such a presumption, we will introduce another FOM designed to penalize such configurations.

b. FOM#2: r_{eff} - an effective r value of the foreground residuals.

We use a proposal of [12] and we characterize any obtained foreground residuals using its effective value of r defined as,

$$s(r_{eff}) \simeq u, \quad (16)$$

where

$$s(r) \equiv \sum_{\ell}^{\ell_{max}} C_{\ell}^{cmb}(r) - C_{\ell}^{cmb}(0),$$

$$u \equiv \sum_{\ell}^{\ell_{max}} C_{\ell}^{\Delta}.$$

We note that due to a missing factor of $2\ell + 1$ this criterion does not compare power contained in the primordial B-spectrum with that of the residuals (up to ℓ_{max}), and in contrast to the latter it gives more weight to low multipoles.

c. FOM#3: σ_{CMB}^{noise} - noise level of the recovered CMB map.

When the true values of the spectral parameters are available the only uncertainty of the recovered component maps, Eq. (2), is due to the instrumental noise and reads,

$$\mathcal{N} = (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1}, \quad (17)$$

and therefore depends on the number of detectors and frequency channels. With our focus on the CMB we will therefore use the diagonal element of \mathcal{N} corresponding to the CMB component as one of our criteria, which we would like to keep as low as only possible. We thus have,

$$(\sigma_{CMB}^{noise})^2 \equiv \mathcal{N}_{00}. \quad (18)$$

We note that only when \mathbf{A} is a unit matrix the above formulae corresponds to a standard, 'inverse-noise-coaddition'. This in turn can only happen if no sky components are mixed together, implying no foregrounds. In any other case the final noise of the CMB map is higher than the inverse noise weighting would imply [14] and its exact value will depend on the details of the component scalings and experimental set up. We note that unlike two other FOMs implemented here this applies on a map rather than a power spectrum level. Moreover, as the spectral parameters, β , are assumed to be known ahead of the computation, this FOM may lead to configurations in which the estimation of those is not feasible and thus rendering the residuals effectively arbitrary and unknown. Nevertheless, though it needs to be used with a care, it provides a meaningful reference against which to gauge other configurations.

C. Optimization procedure

1. Parameters and optimization approaches

In this work typically we will optimize a number of detectors in each of the pre-defined frequency channels. This is clearly one of the most basic hardware parameters one would like to know designing a B-mode experiment. Though the central frequency of the channels are often constrained from the onset by some hardware constraints, we will also consider more general optimization problems in which a number of frequency channels, their central frequencies, and a number of detectors per channel are all to be optimized with respect to.

In the former case we perform a single global optimization operation. Our numerical codes use a minimization algorithm for constrained nonlinear multivariate function, as implemented in MATLAB, which is based on a line-search algorithm with constraints introduced via a quadratic approximation to the Lagrangian function.

In the second type of the optimization problems we have found that attempts of performing a global optimization are often frustrated by numerical issues and the results are consequently not very reliable. Instead we have devised a multi-step approach which is shown schematically in Fig. 2. In the proposed method we start from a configuration consisting of a focal plane overpopulated with a large number of mock channels uniformly covering the requested interval of frequencies. Each of these channels is assigned the same number of detectors or a fraction of the focal plane area, depending on which hardware constraint we use (step 1). We then optimize the number of detectors or focal plane area as in the standard case with the fixed frequency channels with respect to a given FOM (step 2). As the obtained detector distribution is typically rather inhomogeneous we then merge the channels with close central frequencies, e.g., closer than the expected band-width of the anticipated channels. In the process of merging we replace some subsets of channels by a new channel, centered at the barycenter of the previous frequencies as weighted either by a number of detectors or focal plane assigned to each of the merged channels, and assign to it either their detectors or the corresponding focal plane area (step 3). We optimize this new configuration again with respect to numbers of detectors per channel, and go back to step 2 whenever the resulting configuration is found very inhomogeneous. Then we repeat this process again. We find however that usually a single pass over the optimization sequence produces satisfactory results.

2. Constraints

The constraints can be imposed straightforwardly via Lagrangian multipliers therefore permitting a wide variety of those, which can, and sometimes have to, be introduced.

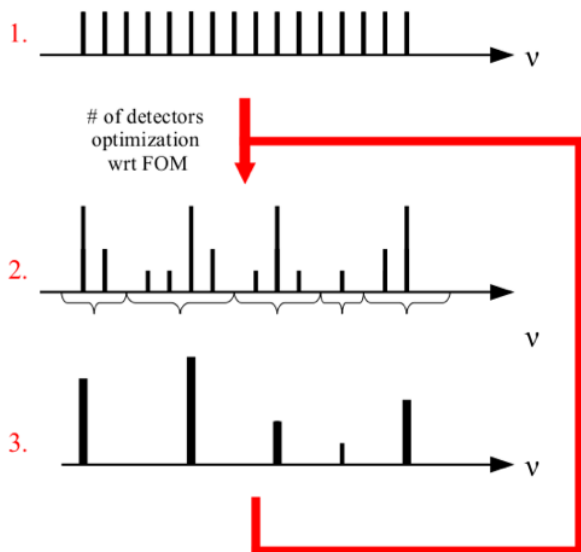


FIG. 2: Schematic illustration of our optimization procedure in a case of an adjustable number of channels, a number of detectors per channel, and their central frequencies.

These include some trivial constraints stemming from the physical interpretation of the optimized parameters, e.g., ensuring non-negative values for detector numbers or focal plane area, which have to be usually included explicitly.

There are also some fundamental constraints without each the convergence could not be reached at all. These typically followed from the hardware restrictions. As an example of the hardware constraint, hereafter we will use either a constraint on a total area of the focal plane or on a total number of detectors, corresponding to cases where we have full freedom to fill in the entire focal plane as densely as only needed or when such freedom is restricted, for instance, by capability of our read-out systems.

Yet another type of constraints invoked in the optimizations studied here includes those driven by the science goals rather than hardware requirements. For instance, we could require that some specific frequency channel map has a noise level better than some pre-set level in order to make such a map good enough to investigate some sky objects or features of interest. This kind of constraints are often needed in the post-processing phase described later.

In addition, while considering multiple FOMs simultaneously we will typically use some of them as constraints restricting the optimization to such configurations for which the required values of these FOMs is better than some suitable threshold.

D. Post-optimization processing

The optimized solution formally determined as described hereto in most of the cases will require further

adjustments and tuning, before it could become a basis for an actual instrument design and later its potential development.

Specific instances of such post-optimization processing, which we consider hereafter include:

- **design simplification** – including either rounding of numbers of detector per channels and/or removing some channels altogether, in particular those assigned a small number of detectors.
- **addition of some ad-hoc frequency channels** – for instance, either to improve the overall robustness of the derived configuration with respect to potential surprises concerning physical properties of the foregrounds, or to extend the science goals beyond what is already encoded in the FOMs.

In all these cases a crucial question is how significant modifications from the initial optimized set-up are allowed before the science goals, as expressed by the FOMs, are compromised too significantly to be acceptable. Below we outline a general approach devised to answer such questions in some specific cases relevant to the applications considered here, leaving a more detailed description of its practical implementation in our study cases to Sect. IV.

1. Detector number rounding

Let us consider only channels for which the optimization procedure has assigned non-zero number of detectors. Moreover we start from the channels for which we want to decrease a number of detectors, as a result of the rounding procedure, and postpone the treatment of the remaining ones for later. For time being we also relax all the constraints imposed on the optimization, with an exception of the ones ensuring positivity of a number of detectors or focal plane area. Removing some of the detectors decreases the instrument sensitivity and thus will affect our science goals, unavoidable rendering the experiment less competitive. **For any specific configuration we can always calculate exactly its performance in terms of the adopted FOMs. However, on the experiment designing stage, when many such configurations may need to be considered and often quickly discarded, the need for the case-by-case computation may be a hinderance. In such a context a fast, even if rough and approximate, approach could be therefore a handy substitute permitting, on the one hand, to zoom quickly on an interesting family of potential solutions, and, on the other, to reject configurations which are clearly of no interest. One way to address such a need could be to construct, for each FOM, a series of hyper-volumes, \mathcal{V}_k , ($k = 0, \dots, n_{\mathcal{V}} - 1$), centered on the optimized configuration and such that $\mathcal{V}_0 \subset \mathcal{V}_1 \subset \dots \subset \mathcal{V}_{n_{\mathcal{V}}-1}$. To each volume, \mathcal{V}_k ,**

we can assign uniquely a value, \tilde{v}_k , such as,

$$\tilde{v}_k \equiv \min_{\{d_i\} \in \mathcal{V}(v_k)} \left\{ \text{FOM}(\{d_i\}) \right\}, \quad (19)$$

i.e., which defines the worst performance plausible within the volume. The values \tilde{v}_k are directly arranged in a descending order given that any volume contains all the previous ones. If now a configuration of our interest belongs to the k -th volume and does not to the $(k-1)$ -th one we immediately can infer that its performance, \tilde{v} , expressed in terms of the given FOM, is bracketed by the two values corresponding to these two hyper-volumes, i.e., $\tilde{v}_{k-1} \leq \tilde{v} \leq \tilde{v}_k$.

Two features are essential to make such a scheme useful. First, we have to have an easy way to identify whether a given configuration is or is not contained in a given hyper-volume. Second, the volumes have to be defined in such a way that the values of \tilde{v}_k assigned to them span a range of interesting values and do so sufficiently densely. Given potential high-dimensionality of the parameter space we consider here, none of these two requirements is straightforward to satisfy. To address the first of them we propose to use as the volumes hyper-ellipsoids defined as,

$$\mathcal{V}_k \equiv \left\{ \{d_i\} \left| \sum_i \frac{(d_i - d_i^{opt})^2}{\sigma_i^{(k)2}} \leq 1, d_i < d_i^{opt} \right. \right\}, \quad (20)$$

where the last condition on the right hand side narrows the volume to the cases of our interest here. The semi-axes of the ellipsoid, $\sigma_i^{(k)}$, need to reflect the fact that the rate at which the given FOM changes will be in general different in different directions in the parameter space. We therefore determine them for every direction corresponding to varying detector numbers in a single channel separately and we do it for each channel of relevance here, i.e., for which $d_i^{opt} \neq 0$. The procedure here involves two steps. First, we select a grid of values of the considered FOM, v_k , which covers the range of its values of our interest and does that with a sufficient density. This grid is used consistently for all directions and channels. Subsequently, for every channel, i , we find numerically a dependence between a value of FOM and a distance from the optimized solution along i -th axis of the parameter space and use this relation to determine $\sigma_i^{(k)}$ so $\text{FOM}(\sigma_i^{(k)}) = v_k$. Typically, the grid point values, v_k , will provide a good approximation to the worst case values, \tilde{v}_k , defined earlier. The latter are therefore expected to be automatically well-spaced and to span a sufficient interval of FOM values. In actual applications, we compute more precise estimates of \tilde{v}_k than those provided by v_k . This is done by using Eq. (19)

and randomly sampling the volume of the corresponding hyper-ellipsoid.

The proposed construction therefore obeys the two requirements we defined earlier and provides a quick and easy way to find out how far the configuration can be tweaked, without compromising the science goals. The parameters $\sigma_i^{(k)}$ and \tilde{v}_k constitute an additional and important piece of information, which should be determined and provided alongside any optimized configuration to render the optimization process helpful. We demonstrate this in actual applications in Sect. IV D 5.

So far we have neglected the hardware constraints. Those would require that any subtraction of the detectors from some of the channels needs to be accompanied by adding detectors somewhere else. However, as adding detectors can only improve our FOMs, the procedure outlined above is conservative as the final outcome of the rounding with the constraints fulfilled can be only better than what the procedure implies.

We can now get back to the channels for which we might have wanted to round up the number of channels. This can be done but only by appropriately distributing the detectors we have removed earlier, as the overall hardware constraint has to be fulfilled. If we do not have however strong preferences regarding their distribution we may try to perform second round of the optimization to find out how it can be done in an optimized way. This could be done by solving the optimization problem as the initial one but adding extra constraints fixing the number of detectors to their rounded value in all the channels, where the rounding has been applied.

2. Low-populated channels

The formal optimization procedure proposed here may result in configurations, which include a number of channels with a relatively low number of detectors. As extra frequency channels contribute to an overall complexity of the instrument, it could be advantageous to remove those if there is no strong science driver behind them. Removing entire channels is more delicate than a removal of some fraction of the detectors as discussed above. This is because it can render the separation process singular or nearly so with separation errors growing rapidly. The singularities however can be usually avoided by keeping track of a number of channels needed to separate some specific number of components, each described by a well-defined number of parameters. We will therefore assume throughout that this is indeed the case. We then proceed as follows with the underpopulated channels. We remove such a channel or contiguous group of those and either redistribute the extra detectors between the adjacent channels or create a new channel with a central frequency computed as a detector (or focal plane area) weighted average of the frequencies of the channels to be

replaced. We then test the change in the FOM values. If either of the options is not satisfactory, we can try to further to improve on it by performing formal optimization but now using only channels which contain a non-zero number of detectors. If that still turns out to be much worse than the optimized values of the FOM, we subsequently need to identify, which of the low-populated channels are crucial from the performance point of view and retain them in our final configuration, while removing or merging the others.

3. *Ad-hoc extra channels*

Clearly our optimized configuration is only as good as the foreground model assumed in the optimization process. The impact of some of the uncertainties in the foreground modeling can be discussed directly within the formalism presented here as, for example, that of details of the foreground correlation matrix and/or shape of their power spectra. It is more difficult however to investigate the role of our assumptions about a number of spectral parameters and/or a number of foreground components. In that respect one may feel more at ease with the configurations, which have the entire frequency range accessible to the instrument sufficiently populated, as they, at least on the intuitive level, may appear more robust with regard to the unknown.

If the optimization does not lead to a configuration, which satisfies such a condition on its own, one may want to impose it by adding one or more ad-hoc frequency channels in the areas they are missing. This can be done straightforwardly by adding a constraint requiring at least some predefined and non-zero number of detectors in those channels. If this number is fixed exactly, it will be obviously not anymore a parameter of the optimization, however the channel will still take part in the optimization process as it will be taken into account in the FOM computation. We use this approach to answer an important question, i.e., how close such a new configuration would perform as compared to the original, optimized one. In other words, should the foreground model used turn out to be correct, would we lose much by trying to make the configuration more robust? Ideally, the loss of performance will not be significant, permitting us to reach both these goals simultaneously: near optimality whenever our modeling is correct, and ability to meet the surprises. In Sect. IV D 5 we discuss how the parameters of such ad-hoc channels can be proposed in a specific application.

E. Design robustness

A problem closely related to the one discussed above is that of the robustness of the final configuration. Given some unavoidable failure rates in a technological process involved in the instrument design and development, a

final version of the instrument typically comes short of the actual design target. An important and valid question then is how robust the science goals posed for the experiment are assuming that the target has been defined using the procedure described here. We address this problem in a specific case in which we admit some failure rate for the detector production process, ϵ . For a set of realistic values of ϵ we perform a random sampling of the parameter space randomly drawing a number of failed detectors. We then evaluate full set of FOMs for each of the samples and find what is an average, likely on 95% confidence level, etc, impact of the considered failure rates on the FOM values.

III. FOREGROUND MODELLING

As discussed earlier in our formalism there are two key quantities needed to describe completely the effect of foregrounds. These are the auto- and cross- spectra characterizing the spatial distribution of the foreground components and the component correlation matrix, $\hat{\mathbf{F}}$. To calculate these we will rely on a specific model of the Galaxy and since we are interested in the B modes, we will consider only diffuse foregrounds, synchrotron and dust, with known and non-negligible polarization emission.

To simulate these emissions in polarization we implement the same recipe as in [10], which starts off from deriving reliable total intensity templates from the available data (the Haslam map [15] for the synchrotron and the combined COBE-DIRBE and IRAS for the dust [16]), rescales them using some constant overall polarization efficiency factor, fixed to 10% in order to match the large scale E and B spectra of [17], therefore producing polarization intensity templates. The polarization angles on the largest scales are then determined using a combination of the WMAP data and 3D modeling of the Galactic magnetic field as in [17], while on the small angular scales ($\lesssim 1^\circ$), by randomly simulating those using their angular power spectra as derived from the data [18].

We assume spatially constant frequency scalings: a power law with index $\beta_s = -3$ for the synchrotron, i.e.,

$$A_{\text{sync}}(\nu, \nu_{ref}) = \left(\frac{\nu}{\nu_{ref}} \right)^{\beta_s} \quad (21)$$

and a uniform greybody scaling law, as in the Model 3 of FDS [19],

$$A_{\text{dust}}(\nu, \nu_{ref}) = \left(\frac{\nu}{\nu_{ref}} \right)^{\beta_d+1} \frac{\exp \frac{h\nu_{ref}}{kT_d} - 1}{\exp \frac{h\nu}{kT_d} - 1}, \quad (22)$$

where $T_d = 18.0$ K and $\beta_d = 1.65$ for the dust.

As pointed out in [10], by adopting this model a large amount of correlation is expected between dust and synchrotron both because the Galactic magnetic field is a common ingredient and because of the lack of high resolution data that forces us to extend the correlation to

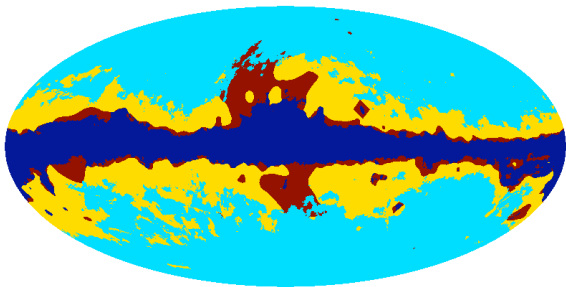


FIG. 3: Three foreground masks as used in this work. Yellow, dark red, and dark blue mark the masked out pixels for MASK II, P06, and MASK I, respectively.

mask	f_{sky}	$\hat{\mathbf{F}}_{\text{dust-dust}}$	$\hat{\mathbf{F}}_{\text{dust-sync}}$	$\hat{\mathbf{F}}_{\text{sync-sync}}$
P06 mask	0.73	3.20	0.082	0.0025
MASK I	0.82	1.12	0.029	0.00084
MASK II	0.51	1.74	0.053	0.0019

TABLE I: $\hat{\mathbf{F}}$ matrix elements computed for two foreground components, dust and synchrotron, at the fiducial frequency of 70GHz for the three masks used in this work **and all pixelized using HEALpix scheme with $n_{\text{side}} = 128$.**

small scales. This is reflected in the fact that the off-diagonal terms of $\hat{\mathbf{F}}$ are of the same order of the diagonal terms. However, as we discuss in Sect. IIA 2 large off-diagonal terms inflate the errors on spectral parameters, so from the perspective of foreground residuals the employed model can be considered conservative.

To investigate the effects of different foreground contrasts and morphology we consider here three different sky masks. MASK I and MASK II are tailored in such a way that they have the possible total polarized foreground contrast (synchrotron plus dust) lower than a predefined threshold equal to 0.86 and $0.36\mu\text{K}$, respectively. We also employ more standard the P06 mask from the WMAP team, which is optimized for the low frequency coverage of WMAP, i.e. it is skewed toward cutting out more the synchrotron than the dust emission. All three masks are shown in Fig. 3, while in Table I we list the elements of the matrix $\hat{\mathbf{F}}$ for each of them.

These masks are thought to be applied *a posteriori* to the full sky map, assumed to be homogeneously observed by the experiments. This means that the noise level per pixel, described in Sect. IV B, will be the same for each of them and thus the results of the FOM#3 optimization will be the same in all three cases.

IV. APPLICATIONS

As an illustration of the method detailed in the previous sections, we will consider the optimization of two different full sky satellite designs: Cosmic Origins Explorer (COre) proposed in response to the European

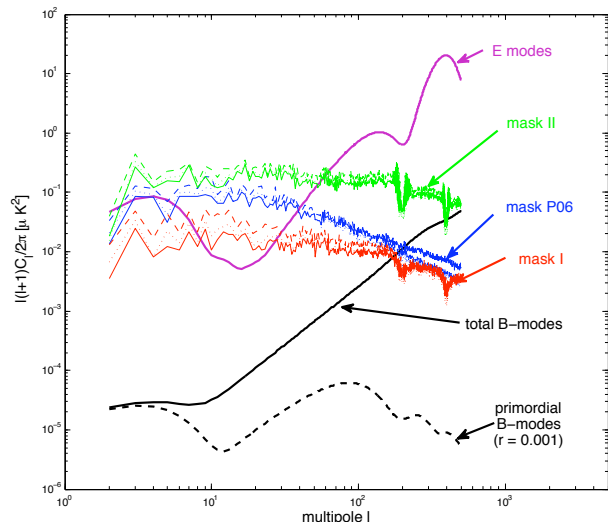


FIG. 4: Pseudo-power spectra of the foreground templates for the three different masks considered in this work and contrasted with the CMB B-mode power spectrum. For each mask the three lines show dust (solid), synchrotron (dashed), and their cross-correlation (dotted). The foreground signals are computed at the 65GHz. **All the spectra used in this work are computed from HEALpix-pixelized maps with $n_{\text{side}} = 512$.**

Space Agency Cosmic Vision 2015-2025 Call [3], and CMBpol [4, 20], proposed as part of the NASA mission concept study. The respective frequency channels and a number of detectors per channel corresponding to the original designs are summarized in Table II for CMBpol and III for COre. In our analysis we will assume the same noise levels per detector for each of the experiments, Sect. IV B, and that they scan the sky homogeneously with all the detectors observing simultaneously over the course of 4 years. With an exception of Sect. IV E we will aim at optimizing a number of detectors per channel, assuming that the latter are fixed and known, and keep either the effective area of the focal plane or total number of detectors constant. The assumed values for the two constraints are derived given the proposed configurations of COre (Table III) and CMBpol (Table II). In the case of the focal plane area we assume that an area of the focal plane occupied by a single, diffraction-limited detector operating at frequency, ν , can be expressed as,

$$\mathcal{A} \sim \frac{c^2}{\nu^2}. \quad (23)$$

The total focal plane area is then obtained by summing over the contribution coming from all the detectors. We note that this gives at the best some *effective* area because we do not take into account any kind of filling factor, which is usually driven by technical constraints such as the shape of the detectors, the wiring, etc. Fig. 5 shows the fractional area as occupied by each channel in the case of the proposed versions.

frequency [GHz]	30	45	70	100	150	220	340	500	850
# of detectors	84	364	1332	196	3048	1296	744	938	1092

TABLE II: CMBpol distribution of detectors among the different channels.

frequency [GHz]	45	75	105	135	165	195	225	255	285	315	375	435	555	675	795
# of detectors	64	300	400	550	750	1150	1800	575	375	100	64	64	64	64	64

TABLE III: COre distribution of detectors among the different channels.

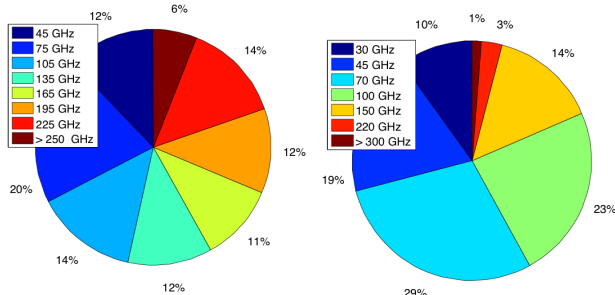


FIG. 5: Breakdown of the focal plane area between the frequency channels as originally proposed for the COre, left, and CMBpol, right, satellites. In the case of COre all the channels with frequencies larger than 250 GHz represent less than 10% of the total focal plane area.

Hereafter we neglect the effects of the E - B leakage, e.g., [21], both in the calculations of the foreground spectra as well as the CMB variance. In the former case this is justified given the fact that E and B spectra for foregrounds are on comparable levels and the leakage is usually harmless. For the CMB variance we assume that the effects of such a leakage can be largely removed using one of the methods proposed in the literature. Though corrections of this sort usually lead to some extra precision loss, this is typically only a fraction of the standard cosmic variance and, at least for experiments with a sufficient large sky coverage, small enough not to change our results in a significant way. For small-scale observations the effect may not be negligible and should be taken into account, e.g., [10, 21].

For some alternative analyses of performance of these two experiments see, e.g., [8, 9, 14].

A. Mixing matrix

To define the mixing matrix, Eq. (1) relevant for the problem at hand, we will use the component frequency scaling laws as defined in Sect. III. We set the reference frequency, i.e., frequency at which all the component maps are recovered as equal to 150 GHz. We also account for frequency band-shapes. For this we will assume that they are top-hat-like with a width equal to $1/3$ of the central value. Therefore, an element, \mathbf{A}_{ij} of the

mixing matrix will be given as,

$$\mathbf{A}_{ij} \equiv \int d\nu \Phi_j(\nu, \nu_{ref}) W_{TH}\left(|\nu - \nu_i|, \frac{1}{3}\nu_i\right), \quad (24)$$

where ν_i is a frequency of the i th channel, $\Phi_j(\nu, \nu_{ref})$ is a photon flux as measured at frequency ν relatively to ν_{ref} , and $W_{TH}(\cdot, \sigma_{TH})$ is a top hat window centered at 0 and with a width σ_{TH} . As mentioned earlier we assume hereafter that the scaling laws adopted on this stage coincide with the true ones modulo the unknown parameters. Nonetheless we will limit the frequency range of the channels included in our discussion below to between 30 and 400GHz, to, on the one hand, avoid channels where the CMB is completely swamped by the foregrounds and, on the other, not to stretch the adequacy of the frequency scaling model of the dust over a too broad interval.

B. Noise levels

We assume sky-noise limited detectors. Their noise level, in antenna units, is taken to be independent on a detectors operating frequency and set to be equal to $\sigma_t \sim 30 \mu\text{K}\sqrt{s}$ [3]. A single detector noise level per pixel will then be given by an observation total length, T_{obs} and pixel area. The detector noise per channel will also depend on a number of detectors operating at a given frequency. The number of detectors for each channel, $\{d_i\}_{(i=0, \dots, n_f-1)}$, are the parameters we will be most frequently trying to optimize in the reminder of this paper. The noise correlation matrix will be then assumed to be diagonal and the diagonal elements will be given by,

$$\mathbf{N}_{ii} = \frac{4\sigma_t^2 N_{pix}^{tot}}{T_{obs} d_i}, \quad (25)$$

here, N_{pix}^{tot} is a total number of observed pixels (to be distinguished from N_{pix} a number of pixels included in the analysis (N_{pix} will depend on the mask we will consider, see Sect. III).

C. Resolution

So far we have ignored completely the fact that detectors operating at different frequencies will likely to have

a different resolution, in particular if they are diffraction-limited. As the parametric maximum likelihood component separation approach adopted here is pixel-based all the channel maps will have to be however smoothed to some common resolution before the separation can be accomplished. The extra smoothing required here is not generally lossless and may introduce noise correlation between the pixels. Hereafter we will ignore such effects and keep on using Eq. (25) to compute the noise levels with only the pixel size, and thus a number of pixels, adjusted accordingly. As far as the sky signals are concerned, given that our science goals are mostly constrained by the large angular scales, we will mimic the common resolution by setting a hard limit on the considered value of ℓ to be $\ell_{max} = 500$, as we have found that for the considered noise levels there is no information beyond that range. We note that in a more refined approach one may want to introduce the resolution as an optimization parameter and constraint it by requiring that the gain due to its decrease is larger than some threshold. **All the power spectra used in this work have been derived using HEALpix pixelized maps with the HEALpix resolution level, $n_{side} = 512$. This is clearly sufficient given the hard ℓ -space cut off we have adopted here. We stress that this resolution is higher than the one used in Sect. III for the determination of the matrix \hat{F} . This is because in the latter calculation only pixel-domain quantities are involved, which are overwhelmingly dominated by the large scale fluctuations for which $n_{side} = 128$ maps are entirely sufficient.**

D. Fixed number of channels with pre-defined, fixed frequencies

In this Section, we describe the optimization of the two experiments, assuming that the frequency channels are fixed ahead of the procedure. The results are summarized in Tables IV and V for COre and CMBpol respectively, and for each FOM (called there for shortness as F1, F2 or F3), three considered sky masks (P06, MASK I or MASK II), and two hardware constraints (total area or total number of detectors), and are contrasted with results obtained for the original designs of the experiments, as shown in the rightmost columns of the Tables. We note that though the latter configurations are mask-independent, the corresponding FOMs values differ somewhat from a mask to a mask due to differences of the sky included in the analysis. For each of the optimized configuration the Tables show a corresponding total number of detectors, focal plane area, effective noise levels, spectral index determination precision, and values of the three FOMs. A selection of these results is also depicted in Figs. 6-9, showing, as bars, a number of detectors for each of the considered channel, left panels, and power spectra of the residuals corresponding to each configuration, right panels. The visualized cases are those based

on the P06 mask, however the other cases would look similar. In each Figure the upper left panel shows a corresponding original configuration followed by three panels displaying configurations optimized with respect to each of the three FOMs. Four general observations are in order here.

1. the optimized configurations depend on the FOM used for the optimization.
2. the constraints imposed on the problem affect the results. Constraining the focal plane area gives preference to the high frequency channels with detectors occupying a small area and thus leads to a worse determination of the synchrotron signal, what in turn leads to a higher level of residuals, if these are left unconstrained, i.e. in cases of FOM#1 and #3. Also the overall noise, FOM#3, tends to be higher.
3. the final configurations obtained for each of the three masks are essentially identical, though the actual values of FOMs do differ mostly due to a different number of pixels with MASK II containing the fewest of those.
4. the optimized configuration contain significantly fewer frequency channels than allowed for in the optimization and therefore than proposed in the original versions of the both these experiments.

Below we comment on some of the result in more detail and leaving a general discussion for the conclusions, Sect. V.

1. FOM#1 optimization - r_{min}

For all configurations shown in Tables IV and V for which FOM#1 could be computed, i.e., those containing more than just 3 channels, r_{min} is found to be on order of 10^{-4} and varying from case to case by no more than a factor of 2. This is also the case for the original designs of the COre and CMBpol satellites. The values of FOM#1 optimized under the constraint of the total number of detectors tend to be somewhat better (worse) than those derived under the total focal plane area constraint for COre (CMBpol). The differences are however small across the board and probably irrelevant in practice.

In both the COre and CMBpol cases, the optimization of FOM#1 leads to configurations for which also FOM#3 is close to the optimum, as the latter is found to be within 5%-10% of its best value for the respective hardware constraints. This suggests that this is the variance due to the noise rather than the foreground residual, which contributes to the recovered value of the FOM#1 more significantly, (see also [10]). Conversely, as a consequence in such cases the level of the foreground residuals is not tightly controlled and therefore the FOM#1-optimized configurations result in values of FOM#2, which are at

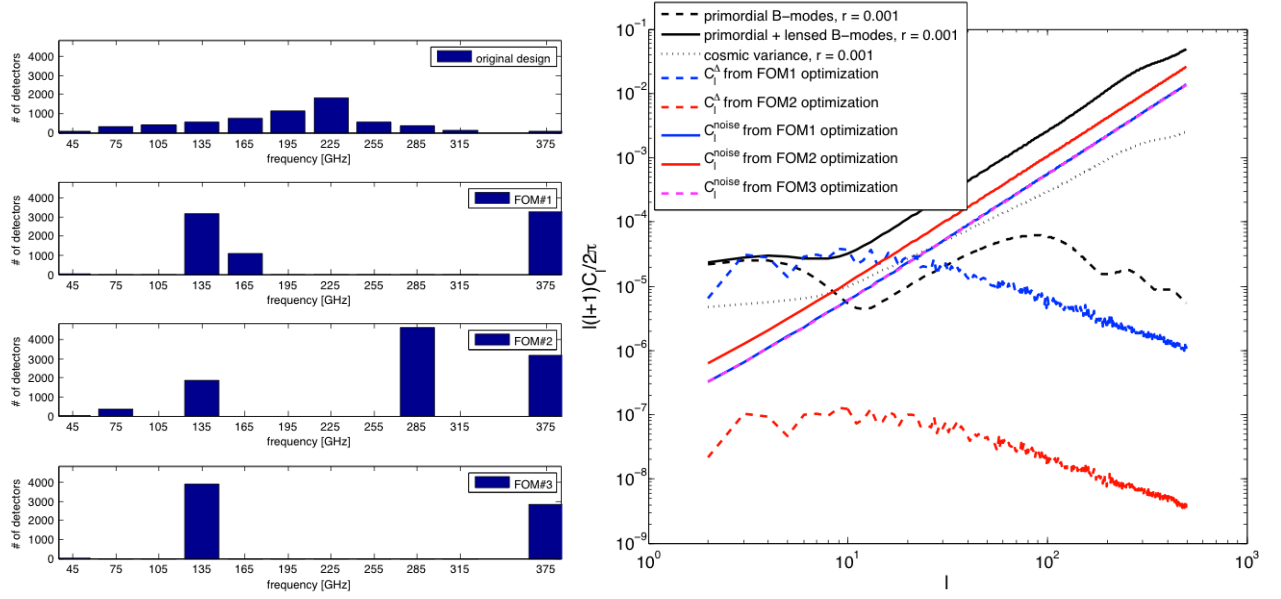


FIG. 6: *Left*: Optimized distributions of numbers of detectors per channel derived under the total focal plane area constraint for the CoRE satellite, including only channels below 400GHz. From top to bottom we show first the original distribution followed by the three optimized ones derived using FOM#1 to #3, respectively. *Right*: Corresponding power spectra of the residuals and the noise computed for the optimized configurations shown on the left and compared against the spectrum of the CMB B-modes with $r = 0.001$.

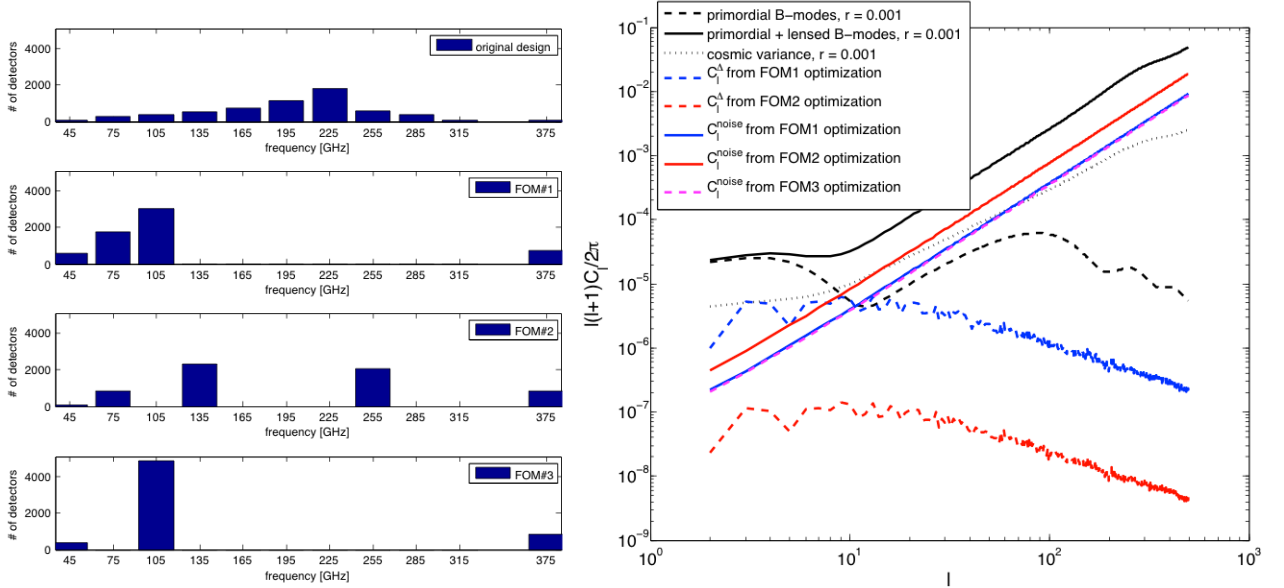


FIG. 7: As in Fig. 6 but imposing the constraint on the total number of detectors.

least one order of magnitude above the best achievable r_{eff} , and worse than the values derived for the proposed designs. As we normally would prefer to avoid too high residuals we conclude that FOM#1 is not sufficient as a stand-alone optimization criterion and preferably should be combined with some other indicator, efficient in en-

forcing low value of the residuals. We will get back to this issue later on in this Section.

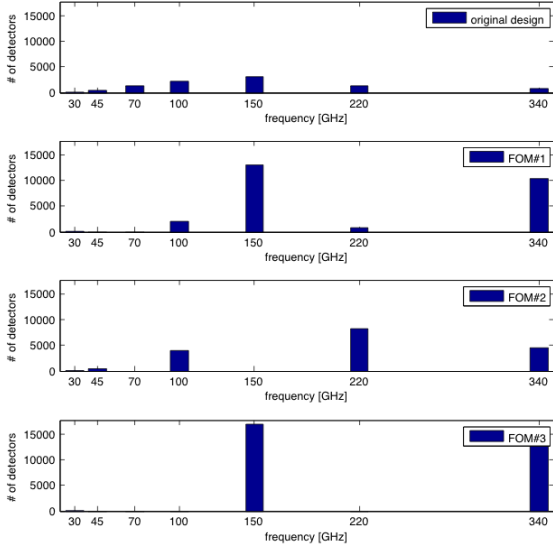


FIG. 8: As in Fig. 6 but for the CMBpol satellite.

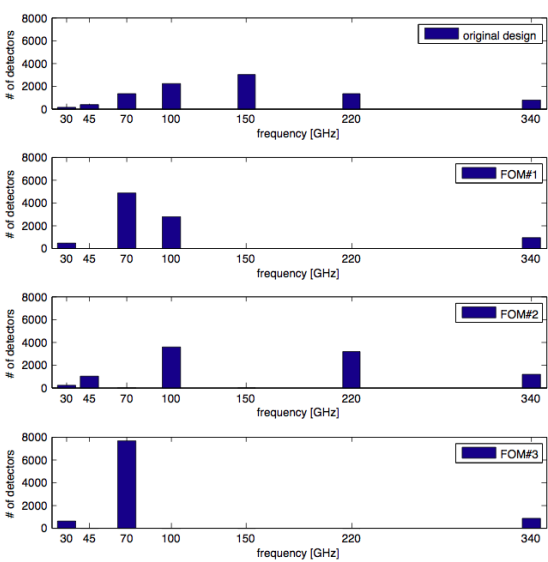
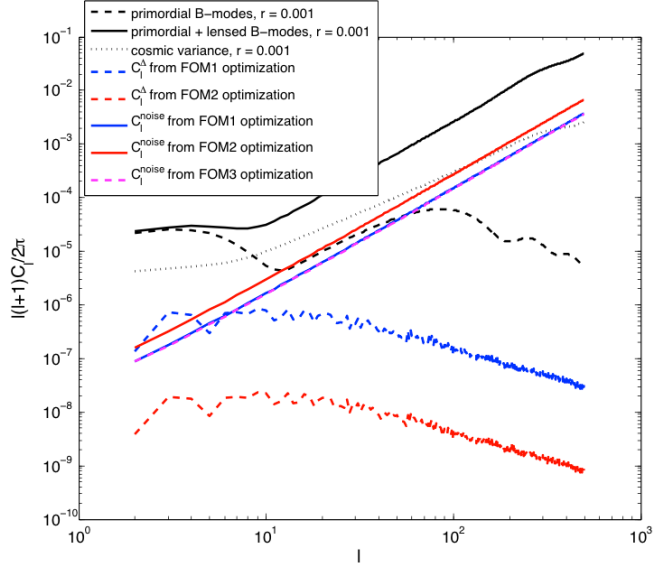
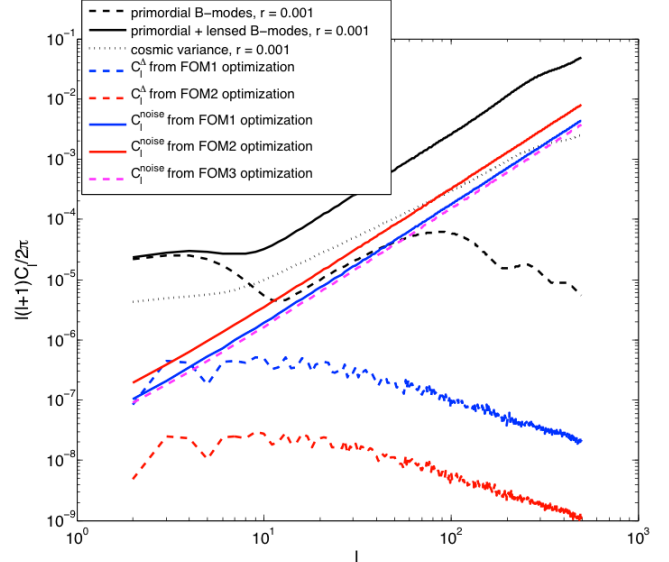


FIG. 9: As in Fig. 7 but for the CMBpol satellite.



2. FOM#2 optimization - r_{eff}

From Eqs. (10)–(12) it follows that a good determination of the spectral parameters β_{dust} and β_{sync} is necessary and sufficient to ensure a low level of the foreground residuals. We therefore expect, see also [12], that in the FOM#2-optimized configuration the detectors should populate predominantly low frequency band, which are dominated by the synchrotron signal, the CMB band, and high frequency band, dominated by the dust. As we require at least 4 channels in the case at hand

to avoid problem singularity and impose the hardware constraint the actual answer is somewhat more complex, nevertheless the overall detector distribution conform with the above intuition. Indeed the FOM#2-optimized configurations include channels below 50GHz, around 100 – 130GHz, and above 250GHz. This applies for both the experiments and for every mask. The details of the distribution depend on a type of the constraint. As the high frequency detectors have smaller area we find that the dust is better estimated ($\delta\beta_{dust}$ lower) under total area constraint case as more high frequency detectors can be had. The opposite can be seen for the synchrotron

constraint	channels (GHz)	P06 mask						mask I				mask II				proposed version		
		area			total #			area		total #		area		total #		P06 mask	mask I	mask II
		F1	F2	F3	F1	F2	F3	F1	F2	F1	F2	F1	F2	F1	F2			
# of detectors	45	45	22	48	610	87	382	45	21	610	72	45	22	607	88	64	-	-
	75	-	370	-	1775	827	-	-	366	1775	778	-	37	1759	832	300	-	-
	105	-	-	-	3027	-	4876	-	-	3026	-	-	-	3042	-	400	-	-
	135	3160	1872	3918	-	2313	-	3161	1886	-	2322	3124	1871	-	2315	550	-	-
	165	1092	-	-	-	-	-	1091	-	-	-	1146	0	-	-	750	-	-
	195	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1150	-	-
	225	-	-	-	-	-	-	-	-	-	-	-	-	-	-	1800	-	-
	255	-	-	-	-	2081	-	-	-	-	2141	-	-	-	2073	575	-	-
	285	-	4623	-	-	-	-	-	4669	-	-	-	-	4610	-	375	-	-
	315	-	-	-	-	-	-	-	-	-	-	-	-	-	-	100	-	-
375	3281	3186	2859	717	820	870	3281	3156	717	816	3294	3188	719	820	64	-	-	
total area		0.023	0.023	0.023	0.081	0.032	0.057	0.023	0.023	0.081	0.031	0.023	0.023	0.080	0.032	0.023	-	-
Σ [# of dets]		7579	10073	6824	6128	6128	6128	7577	10099	6128	6128	7608	10062	6128	6128	6128	-	-
fractional area	45	0.085	0.042	0.091	0.34	0.12	0.30	0.085	0.040	0.34	0.10	0.085	0.042	0.36	0.12	0.12	-	-
	75	-	0.25	-	0.35	0.42	-	-	0.25	0.35	0.41	-	0.25	0.35	0.42	0.21	-	-
	105	-	-	-	0.31	-	0.69	-	-	0.31	-	-	-	0.31	-	0.14	-	-
	135	0.67	0.40	0.83	-	0.358	-	0.67	0.40	-	0.37	0.66	0.40	-	0.36	0.12	-	-
	165	0.15	-	-	-	-	-	0.15	-	-	-	0.16	-	-	-	0.11	-	-
	195	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.12	-	-
	225	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.14	-	-
	255	-	-	-	-	0.090	-	-	-	-	0.097	-	-	-	0.090	0.034	-	-
	285	-	0.22	-	-	-	-	-	0.22	-	-	-	0.22	-	-	0.018	-	-
	315	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.0039	-	-
375	0.090	0.088	0.079	0.006	0.016	0.010	0.090	0.087	0.0057	0.017	0.090	0.088	0.0057	0.016	0.0018	-	-	
noise per channel [$\mu K_{antenna}$]	45	0.37	0.524	0.354	0.099	0.263	0.125	0.37	0.53	0.099	0.30	0.37	0.52	0.099	0.26	0.31	-	-
	75	-	0.127	-	0.058	0.085	-	-	0.13	0.058	0.088	-	0.13	0.058	0.085	0.14	-	-
	105	-	-	-	0.044	-	0.035	-	-	0.044	-	-	-	0.044	-	0.12	-	-
	135	0.044	0.057	0.039	-	0.051	-	0.044	0.056	-	0.051	0.044	0.036	-	0.051	0.10	-	-
	165	0.074	-	-	-	-	-	0.074	-	-	-	0.072	-	-	-	0.089	-	-
	195	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.072	-	-
	225	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.058	-	-
	255	-	-	-	-	0.054	-	-	-	-	0.053	-	-	-	-	0.10	-	-
	285	-	0.036	-	-	-	-	-	0.036	-	-	-	0.036	-	-	0.13	-	-
	315	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.24	-	-
375	0.043	0.043	0.046	0.091	0.085	0.083	0.043	0.044	0.091	0.086	0.043	0.043	0.091	0.085	0.31	-	-	
$\delta\beta_d [10^{-3}]$		0.96	0.12	-	0.95	0.16	-	0.83	0.074	0.82	0.10	1.47	0.19	1.48	0.25	0.28	0.18	0.45
$\delta\beta_s [10^{-3}]$		30	2.9	-	4.3	2.2	-	26	1.9	3.7	1.4	38	3.9	5.6	2.9	3.4	2.2	4.5
$\frac{\delta\beta_d\delta\beta_s}{\delta\beta_d \times \delta\beta_s}$		-0.918	-0.44	-	-0.92	-0.57	-	-0.96	-0.46	-0.96	-0.58	-0.91	-0.44	-0.91	-0.57	-0.67	-0.70	-0.67
F1 [10^{-3}]		0.22	0.26	-	0.21	0.24	-	0.20	0.23	0.19	0.21	0.31	0.37	0.29	0.34	0.28	0.25	0.40
F2 [10^{-3}]		0.95	0.0097	-	0.16	0.011	-	1.06	0.0057	0.18	0.0065	0.79	0.086	0.14	0.0094	0.028	0.018	0.025
F3 [nK _{cmb}]		5.4	10	5.3	3.6	7.4	3.4	5.4	10	3.6	7.7	5.4	10	3.6	7.4	14	14	14

TABLE IV: Summary of the optimization results in the case of COre considering channels only below 400 GHz. For each of the three masks, we present results for each of the three FOMs optimized under one of the two constraints, either fixing the focal plane area or the total number of detectors. The results for FOM#3 are quoted only once as they do not depend on the choice of the mask. The rightmost columns show the results computed using the original version of COre as proposed in [3]. In the latter case the configuration is always the same, whatever the choice of the mask.

estimation. The resulting levels of the residuals are however essentially identical in both these cases. More aggressive masking clearly helps, MASK I, but a balance has to be maintained between lowering the overall foreground level and the precision of the spectral index determination. The latter, unlike the former, benefits from a larger number of pixels and higher foregrounds and, otherwise, can therefore start driving the effective residual up, e.g., MASK II.

The FOM#2-optimized configurations usually render good values for FOM#1 (within 10 – 15% of the best achievable values), but result in the CMB map noise levels (FOM#3) up to twice higher than the best ones. The original versions of the considered experiments also yield the values of r_{eff} close to the best ones.

3. FOM#3 optimization

For this FOM, and in every considered here case, the optimization of the focal plane with respect to the noise in the CMB map ends up with only 3 non zero channels: two at frequencies as extreme as only allowed for, and one at an intermediate one contained in the CMB frequency band. The precise position of the latter is found again to be dependent on a type of the hardware constraint used. For the CMBpol satellite the values of the central frequencies are 70 or 150GHz for the constraint on the total number of detectors and the area, respectively. For COre they are 105 and 135GHz, respectively. We recall that in the case of this FOM all the spectral indices are assumed to be known, otherwise the 3 channel

constraint	channels (GHz)	P06 mask						mask I				mask II				proposed version		
		area			tot #			area		tot #		area		tot #		P06 mask	mask I	mask II
		F1	F2	F3	F1	F2	F3	F1	F2	F1	F2	F1	F2	F1	F2			
# of detectors	30	35	62	52	472	185	601	33	61	448	168	56	62	672	187	84	-	-
	45	-	491	-	-	1016	-	-	493	-	975	10	491	1240	1021	364	-	-
	70	-	-	-	4861	-	7646	-	-	4935	-	-	-	3643	-	1332	-	-
	100	1970	4056	-	2776	3546	-	1400	4101	2579	3567	6311	4049	2583	3544	2196	-	-
	150	13159	-	16995	-	-	-	14639	-	-	-	3518	-	-	-	3048	-	-
	220	823	8328	-	-	3164	-	-	8228	-	3207	178	8340	-	3157	1296	-	-
340	10364	4525	13210	954	1154	817	11586	4259	1102	1148	7988	4566	926	1154	744	-	-	
total area		0.084	0.084	0.084	0.16	0.10	0.20	0.084	0.084	0.16	0.099	0.084	0.084	0.21	0.10	0.084	-	-
Σ [# of dets]		26352	17462	30258	9064	9064	9064	27658	17143	9064	9064	18061	17508	9064	9064	9064	-	-
fractional area	30	0.042	0.074	0.063	0.29	0.18	0.30	0.040	0.073	0.28	0.17	0.068	0.074	0.32	0.18	0.10	-	-
	45	-	0.26	-	-	0.44	-	-	0.26	-	0.44	0.0054	0.26	0.26	0.44	0.19	-	-
	70	-	-	-	0.55	-	0.70	-	-	0.57	-	-	-	0.31	-	0.29	-	-
	100	0.21	0.44	-	0.15	0.31	-	0.15	0.44	0.15	0.32	0.68	0.44	0.11	0.31	0.24	-	-
	150	0.63	-	0.81	-	-	-	0.70	-	-	-	0.17	-	-	-	0.15	-	-
	220	0.018	0.19	-	-	0.057	-	-	0.18	-	0.060	0.0040	0.19	-	0.057	0.029	-	-
340	0.097	0.042	0.12	0.0046	0.0088	0.0032	0.11	0.040	0.0054	0.0090	0.074	0.043	0.0034	0.0087	0.0069	-	-	
noise per channel [$\mu K_{antenna}$]	30	0.41	0.31	0.34	0.11	0.18	0.010	0.42	0.31	0.12	0.19	0.33	0.31	0.094	0.18	0.27	-	-
	45	-	0.11	-	-	0.077	-	-	0.11	-	0.078	0.77	0.11	0.070	0.077	0.13	-	-
	70	-	-	-	0.035	-	0.028	-	-	0.035	-	-	-	0.041	-	0.067	-	-
	100	0.055	0.038	-	0.046	0.041	-	0.065	0.038	0.048	0.04	0.031	0.038	0.048	0.041	0.052	-	-
	150	0.021	-	0.019	-	-	-	0.020	-	-	-	0.041	-	-	-	0.044	-	-
	220	0.085	0.027	-	-	0.044	-	-	0.027	-	0.043	0.18	0.027	-	0.044	0.068	-	-
340	0.024	0.036	0.021	0.079	0.072	0.086	0.023	0.038	0.074	0.072	0.027	0.036	0.080	0.072	0.090	-	-	
$\delta\beta_d [10^{-3}]$		0.25	0.086	-	0.71	0.13	-	0.37	0.055	0.62	0.055	0.41	0.14	0.066	0.21	0.16	0.10	0.25
$\delta\beta_s [10^{-3}]$		2.39	0.51	-	1.5	0.38	-	3.2	0.33	1.4	0.33	2.7	0.68	0.67	0.50	0.55	0.36	0.73
$\frac{\delta\beta_d\delta\beta_s}{\delta\beta_d\times\delta\beta_s}$		-0.66	-0.46	-	-0.96	-0.48	-	-0.10	-0.48	-0.88	-0.49	-0.88	-0.46	-0.54	-0.48	-0.63	-0.65	-0.62
F1 [10^{-3}]		0.19	0.20	-	0.19	0.20	-	0.17	0.18	0.17	0.18	0.27	0.28	0.27	0.29	0.20	0.18	0.29
F2 [10^{-3}]		0.024	0.0018	-	0.059	0.0023	-	0.076	0.0011	0.069	0.0014	0.020	0.0016	0.012	0.0020	0.0041	0.0026	0.0036
F3 [nK _{CMB}]		1.5	2.7	1.4	1.6	3.1	1.5	1.4	2.7	1.6	3.2	1.6	2.7	1.7	3.14	3.0	3.0	3.0

TABLE V: As in Table IV but for CMBpol [4].

configurations derived here would be singular and would not permit a determination of the spectral indices. The achieved noise levels are better when the total number of detectors is constrained, and are lower by a factor up to ~ 1.6 . The original versions of the satellites result in quite high noise (higher by a factor of 2.5 – 4) in comparison with the one derived for the optimized configurations.

4. Consensus configuration

Having postulated three different FOMs we have obtained three different, optimized configurations. Moreover, as we have already mentioned earlier there is clearly tension between some of the considered FOMs. The issue now is therefore how to find a compromise between them in order to select a single configuration as a result of our procedure. To do so we first recall that in our case the configurations preferred from the point of view of FOM#1 fail to ensure a satisfactory level of the residuals, as quantified by FOM#2, while optimization of the latter yields a rather high level of noise, i.e., FOM#3. Simultaneously however optimizing FOM#1 effectively ensures a near optimization of FOM#3. Therefore we will retain the former as part of the optimization and drop the latter, which from now on will be used only as a benchmark to compare the obtained configurations against. As FOM#1 on its own is not fully satisfac-

tory we will therefore optimize it, while imposing a constraint based on a value of FOM#2. Clearly if more FOMs are used more constraints can be introduced in the same way. What values to choose for the thresholds is a somewhat debatable question, an answer to which will depend on a specific application. In our case, we first note that for the FOM#2-optimized configuration the resulting r_{eff} is an order of magnitude lower than the respective value of r_{min} . The latter is moreover typically 20% higher than its corresponding best value. From the viewpoint of these two indicators the FOM#2-optimized solution looks therefore quite satisfactory. This is particularly true for the CMBpol case for which this solution can be accepted as indeed the final outcome of the procedure. For CORe the potential remaining problem could be the noise level. In search of the consensus configuration we may therefore want to let the residual grow in particularly relatively to the value of r_{min} and gain in terms of the noise. Clearly more we compromise on r_{eff} more we can gain on σ_{CMB}^2 . As for CORe the values of r_{min} are close to 2×10^{-4} we will allow r_{min} to be as large as 10^{-4} , and re-optimize the problem with respect to FOM#1 with the constraint that $r_{eff} \leq 10^{-4}$. This specific choice is in fact arguably rather high. In fact we find that imposing more strict limits of $r_{eff} \leq 2.5 \times 10^{-5}$ or 5×10^{-5} already can ensure satisfactory noise levels, 4.0 and 3.9 nK_{CMB}, respectively, and thus could be preferred for the actual experiment optimization. We will

however use hereafter the threshold of 10^{-4} as it is more useful for the demonstration purposes.

The resulting configuration is shown in Fig. 10 and summarized in Table VI, where we show the results obtained for the two hardware constraints. The spectra of the noise and residuals are also displayed in the right panel of the Figure. We conclude that the detector distribution indeed resemble a hybrid between two solutions obtained earlier as a result of the optimization of FOMs: #1 and #2 separately with a respective hardware constraint, Figs. 6 & 7. As anticipated above the overall level of the foreground residual spectrum is rather high as compared to both the B-mode spectrum and its respective variance due to the noise and the sky. However, as intended, the noise level has been successfully suppressed to the levels close to those computed for FOM#3 optimized configurations.

5. Post-processing

For definiteness in this Section we focus on a single, specific configuration, and choose for it the optimized CORE set-up obtained from the optimization of the FOM#1 value, while constraining the corresponding value of FOM#2 to be no more than 10^{-4} and keeping the total number of detectors fixed, as discussed at the end of the previous Section. The details of this configuration are listed in the fourth column of Table VI together with the respective FOMs values.

The procedure employed in this Section follows the steps outlined in Sect. IID. In Fig. 11 we show an impact of a fractional change of a number of detectors in one channel at the time on the values of the FOMs. The latter are given relatively to their optimized values and therefore all the curves shown in the Figure are expected to start from a FOM value equal to one for a fractional change equal to zero, i.e., the optimized configuration itself, and typically monotonically grow with an increasing value of the fractional change parameter. In addition, for reference we also show how the FOMs values would change if numbers of detectors in all the channels are decreased by the same fraction. We note that at least for the two of the FOMs, i.e., FOM#2 and #3, the latter dependence can be straightforwardly predicted using Eqs. (5), (12), & (17) and shown to be inversely proportional to an actual number of detectors in the corresponding configurations and thus inversely proportional to (1–fractional change of detectors). This indeed is adhered to by our numerical results.

The most striking features of some of the results is their apparent flatness extending on occasions to a rather high values of the fractional change. At a face value that suggests that one is at liberty to change a number of detectors in some of the channels rather drastically but without noticeably penalizing the performance of the instrument. However, though some freedom indeed exists, it has to be exploited carefully. In particular, significantly

changing a number of detectors in one selected channel, will usually have an effect of removing any freedom in adjusting the number of detectors in the remaining channels. Therefore if one’s goal is to round-up the optimization results in a way to make them more amenable to an actual implementation that may not be the right way to go. Below we showcase some of these issues in the specific case at hand.

Probably most conspicuous thing about the configuration considered here is the presence of a channel centered at 255GHz, to which are assigned only 17 detectors, as opposed to a few thousands in some of the other channels. A natural question to ask is therefore whether this channel is needed at all. In fact, the two outermost panels of Fig. 11 seem to confirm our feeling that this channel is in practice irrelevant as both the FOMs #1 and #3 effectively do not depend on its being present or not. This is not so however for the FOM#2 as shown in the middle panel. In this case removing this channel altogether will boost the value of this FOM, and thus the level of the foreground residual by a factor of ~ 1.5 . Though not overwhelmingly large it is substantial enough to justify holding on to this channel (unless of course the hardware cost of having the extra channel tips the balance the other way). These expectations are confirmed by direct calculations, results of which as shown a 5th column in Table VI. (We note that an attempt to re-optimize the resulting 4-channel system ”a posteriori” does not bring much improvement either, Table VI, column 6). We note that trying to keep the level of residuals down in this case can be of particular importance given that already in its original, optimized version (Table VI) the resulting values of r_{min} and r_{eff} are close enough to each other that this is probably the latter, i.e., the level of residuals, which would drive the actual limit on a detectable r value for this set-up, rather than statistical estimate provided by FOM#1. Letting r_{eff} grow any further would therefore directly affect our science goals. Instead we can therefore try to trim a number of detectors in either 45 or 375GHz channel. We see that we can potentially reject up to $\sim 70\%$ of the detectors in the former or $\sim 80\%$ in the latter, without affecting the residuals level (FOM#2) in any appreciable manner. This would have an effect of increasing FOM#1 value by no more than $\sim 5\%$ and FOM#3 by no more than $\sim 50\%$, both of which may therefore look perfectly acceptable. Whichever option we opt for, we can then re-use the spare detectors by distributing them to some of the existing channels or creating some additional ones, say at 165GHz, in order to be better equipped to face some potential surprises (Sect, IID). However a special care then has to be taken if a number of detectors in some other channels needs to be concurrently decreased. This is because, as illustrated by lines marked with circles in Fig. 11, not all directions in the parameter space are similarly flat.

If our aim is to just round-up the detector numbers we can proceed as outlined in Sect. IID. We first postulate a set of fractional changes from the optimized values. In

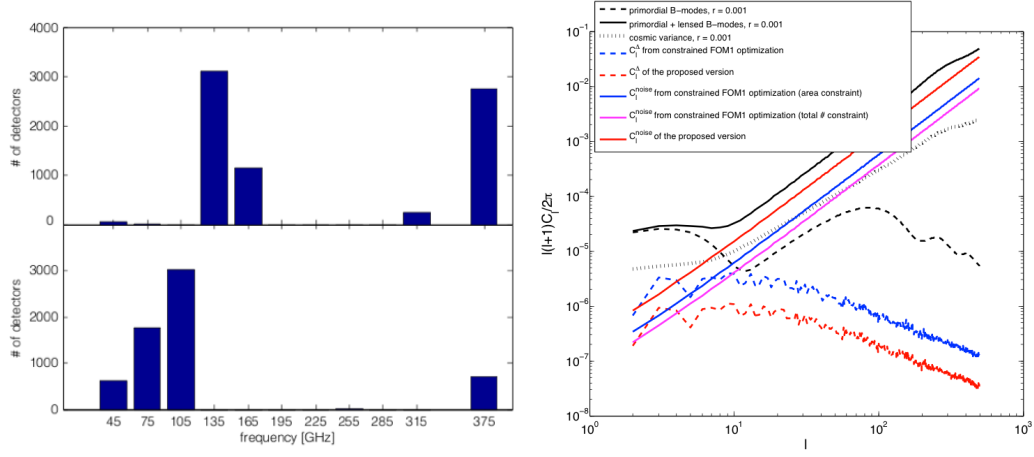


FIG. 10: Left panel: Result of the optimization of FOM#1, under the constraint $\text{FOM}\#2 \leq 10^{-4}$, in the case of COre, considering only channels below 400 GHz and the P06 mask. Upper (lower) histogram corresponds to the optimization of the number of detectors under the total area (total number of detectors) constraint.

Right panel: illustration of the optimization result described in table VI and shown on the left panel. We see power spectra of the proposed COre and the optimized versions. This has been obtained in the case of COre, considering only channels below 400 GHz for the P06 mask. The FOM#1 optimization has been done under total area constraint (blue curves) and total number of detectors constraint (magenta curve). Residuals for both constraints are the same.

	channels (GHz)	F1-optimized	no 255GHz channel cases		extra channels	original version [3]
		+ constraint $\text{F2} \leq 10^{-4}$	no optimization	F1-optimized + $\text{F2} \leq 1.5 \times 10^{-4}$	F1 optimized + $\text{F2} \leq 10^{-4}$	
# of detectors	45	607	607	592	366	64
	75	1771	1771	2112	47	300
	105	3021	3021	2801	4551	400
	135	-	-	0	-	550
	165	-	-	0	-	750
	195	-	-	0	200	1150
	225	-	-	0	-	1800
	255	17	0	0	-	575
	285	-	-	0	200	375
	315	-	-	0	-	100
	375	711	711	623	764	64
$\delta\beta_d [10^{-3}]$		0.74	0.95	0.91	0.35	0.28
$\delta\beta_s [10^{-3}]$		3.5	4.3	4.1	8.1	3.4
$\frac{\delta\beta_d \delta\beta_s}{\delta\beta_d \times \delta\beta_s}$		-0.88	-0.92	-0.92	-0.66	-0.67
F1 [10^{-3}]		0.21	0.21	0.21	0.21	0.28
F2 [10^{-3}]		0.10	0.16	0.15	0.10	0.028
F3 [nK _{cmb}]		3.6	3.6	3.6	3.6	14

TABLE VI: Comparison of performance of the variants of the COre set-ups considered in Sect. IV D 5. All the optimization runs have been performed while keeping the total # of detectors constant, used the P06 mask and only the channels below 400GHz. The configurations in the Table include, from left to right, (1) a result of the optimization procedure with respect to FOM#1 with a constraint on FOM#2 of $\leq 10^{-4}$, (2) the same configuration but with the 255GHz channel suppressed, (3) a configuration with the same frequency channels as in (2), but with numbers of detectors re-derived via an optimization with respect to FOM#1 and a constraint $\text{FOM}\#2 \leq 1.5 \times 10^{-4}$, and (4) a re-optimized configuration with the channels as before plus two extra ones with a fixed number of detectors (= 200 each). The very last column shows the original COre configuration for comparison.

our case these could be $[v_k] = [1.025, 1.05., 1.1, 1.15]$ for FOM#1 and $[v_k] = [1.05, 1.25., 1.5, 2.0]$ otherwise, and then use Fig. 11 to read off the corresponding values of the fractional change for each channel and each FOM. These are values denoted σ in Sect. II D. In our case for

FOM#1 they read,

$$\left\{ \sigma_j^{(k)} \right\} = \left\{ \begin{array}{cccc} 409 & 496 & 555 & 577 \\ 1017 & 1664 & 1771 & \infty \\ 880 & 1477 & 2236 & 2697 \\ \infty & \infty & \infty & \infty \\ 442 & 549 & 624 & 654 \end{array} \right\}, \quad (26)$$

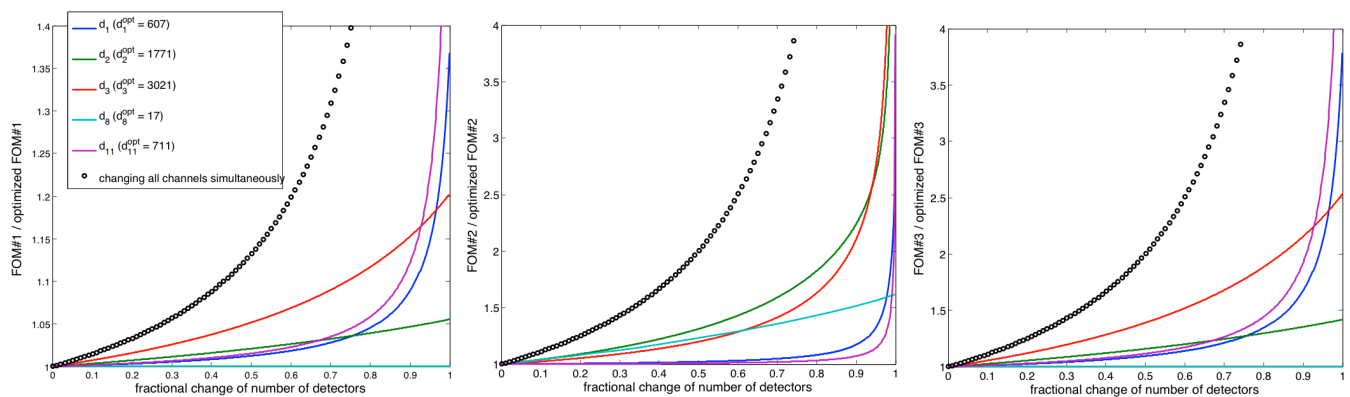


FIG. 11: Dependence of the values of FOM#1 (left), #2 (middle), and #3 (right), on a fractional change of a number of detectors in the hardware configuration as detailed in the 4th column of Table VI. The solid lines show cases when a number of detector in only one selected channel being gradually decreased (left to right) and all the others being kept fixed at their optimized values. The circles show the case with a number of detectors in all channels decreasing by the same fraction simultaneously. The color schemes for the lines are the same in all the panels and described in the legend.

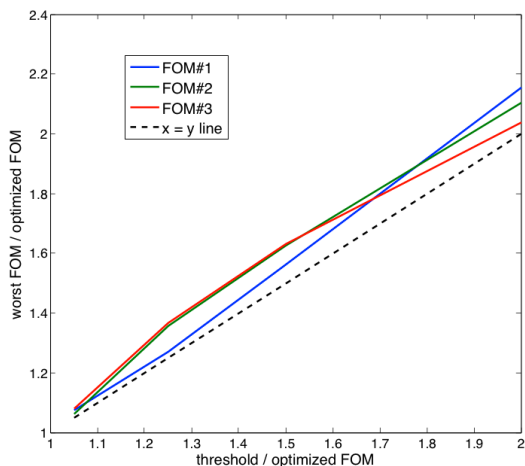


FIG. 12: The worst values of each FOM, \tilde{v} , computed for each of the concentric hyper-ellipsoids, Eq. 20, defined by the threshold values, v , as shown on the horizontal axis. The dotted line shows $\tilde{v} = v$ case. Clearly, $\tilde{v} \simeq v$ in all shown cases, where the latter approximate equality holds to within 10%. The values of \tilde{v} and v given here are relative to the optimized values of the respective FOMs.

where k th column corresponds to the k th value of v_k and thus gives values of σ for each of the five channels with non-zero number of detectors in the optimized configuration (see 2nd column of Table VI). We can use these values to define, Eq. (20), hyper-ellipsoidal volumes, \mathcal{V}_k , in the parameter space centered on the optimized configuration. We note that the infinity sign marks the cases, where the desired value of v_k could not have been reached due to the parameter space boundary. For instance, the values in the 4th row of Eq. (26) are all infinite as in the neighborhood of the optimized configuration the value of FOM#1 does not depend on a number of detectors in

this channel as can be seen in Fig. 11.

To find the worst case value of the FOM for a k th hyper-ellipsoid, \tilde{v}_k , we use random sampling of first an entire volume of the ellipsoid followed by that of only its surface. The latter requires fewer samples to ensure proper sampling density and is more efficient if we have some expectation of the FOM values being monotonically deteriorating away from the optimized configuration. As anticipated in Sect. IID the corrected values, \tilde{v}_k , and initial ones, v_k , are indeed found to be quite close, typically within 20% of each other as illustrated in Fig. 12.

The series of the concentric hyper-ellipsoids constructed here gives us a quick, though approximate, way to estimate the performance of some proposed configurations derived from the optimized one via small changes of all or some optimization parameters. As an example, consider an configuration with $[d_j] = [600, 1700, 3000, 17, 700]$ detectors in each of the five channels considered here respectively. Given that for FOM#1,

$$\sum_k \frac{(d_j - d_j^{opt})^2}{\sigma_j^{(k)^2}} \leq 1 \quad (27)$$

is fulfilled for any k , we conclude that the respective value of FOM#1 for this case will not be larger than by a factor $\tilde{v}_{k=1} \lesssim 1.025$ than the optimized value. Indeed a direct calculation renders a value 1.002 times higher than the optimized one in agreement with our quick estimation. Similarly, we can deduce the performance of this configuration as expressed by the two other FOMs. These are more sensitive at least to changes in some of the channels however we find that for this specific configuration we can lose no more than a factor of 1.05 for both of them. These could be compared to the actual values of 1.01 and 1.02, respectively, all relative to the corresponding optimized values.

In this case overall the loss of performance seems rather benign and acceptable. Moreover, as a result of rounding-down the detector numbers we have gained around 100 of those, which we can arbitrarily assign to any of the existing channels or even create a new one to saturate the constraint on the total number of detectors. Whatever decision we make we will not compromise any of the performance figures derived earlier.

To illustrate a process of adding some ad-hoc channels at this time we start from a configuration more drastically stripped-down than the one discussed above. Let that be for instance $[d_k] = [500, 1500, 3000, 0, 600]$, where we not only reduced numbers of detectors per channel more substantially but also removed the 4th channel altogether. Using the hyper-ellipsoid formalism we get quickly a helpful insight into how much we have lost as a result of choosing this configuration. As we already discussed that earlier the biggest loss is found with regard to the value of FOM#2, which is boosted by more than 50% (but less than 100%) with FOM#1 and #3 changing by $\lesssim 1.05$ and ~ 1.1 respectively. (The actual values being 1.01, 1.81 and 1.09 for FOMs: #1, #2, & #3.) However we have also gained as many as 400 detectors, which can be distributed at our discretion to fill the constraint. Let us do so by introducing two extra channels at 195 and 285GHz with 200 detectors each. This improves the performance of the considered configuration, an improvement, which we can ameliorate even further by performing the optimization with respect to the detector numbers in the four original channels and keeping the detector numbers of the new channels fixed to 200. We indeed find that the new set-up performs nearly as well as the initial optimized one (Table VI, column 3 vs. 7) but possesses a more uniform frequency coverage. If we now want to perform a controlled detector number rounding and analyze its impact on the configuration performance we would need to restart the entire procedure described above.

6. Robustness tests

As explained in Sect. II E, for each FOM, we start from the optimized configurations, as determined earlier and check how the values of the FOMs depend on a random suppression a number of detectors in each channel by some fraction. Specifically, we assume here that the distribution of the anticipated detector failures is Gaussian with the dispersion equal to ε of which is the same for each of the considered channel and taken to change from 5%, 10%, 25%, and 50%. We randomly draw some large number of samples, here 10^4 , and histogram the results for each of the FOMs. We then compute the most likely value of the FOMs, 95%-confidence limit, and the worst drawn value. In the case of the CORe configuration studied in the previous Section we collect the results in Fig. 13. We conclude, as probably could have been anticipated from the results of the previous Section, that

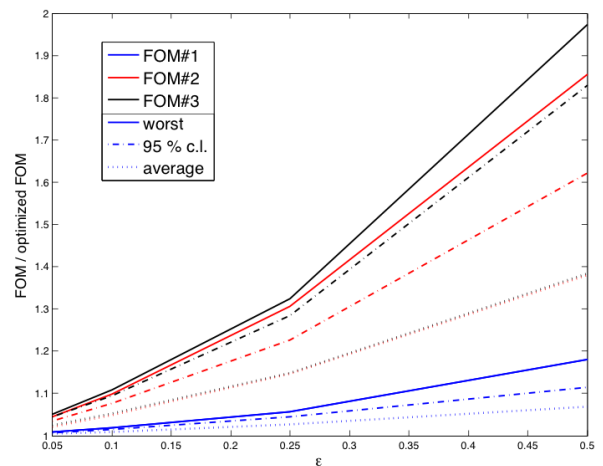


FIG. 13: Summary of our robustness tests applied to the CORe configuration obtained via the optimization of FOM#1 with constraints of $\text{FOM}\#2 \leq 10^{-4}$ and a fixed number of detectors. The lines of different colors correspond to different FOMs and different lines show: average (dotted), 95% c.l. (dot-dashed), and the worst value (solid).

for failure rate as large as 30% we will not compromise on the FOM values by more than 50% with respect to the optimized ones, while failure rate of 10% will result in their 10% increase. These results affirm the practical soundness of the derived configuration.

7. Robustness with respect to the foreground modeling

Results of the optimization procedures as the one considered here are usually only as good as the foreground models used in their course. In the specific case studied here we expect that our results are fairly robust as far as foreground morphology is concerned. Our estimates are driven by two compact descriptions of those, the foreground correlation matrix, $\hat{\mathbf{F}}$, and the foreground power spectra, which are not expected to be wildly different than what we have assumed here. We note in particular that an increasing amplitude of the foregrounds leading to an increase of both the elements of the matrix, $\hat{\mathbf{F}}$, and overall normalization of the foreground power spectra would decrease the errors on the spectral parameters and result in the amplitude of the residuals virtually unchanged. These expectations are confirmed by the results obtained hereto for the three different masks.

It is more difficult to assess, though potentially more crucial, an impact of increasing a number of spectral parameters. This could be either due to a more complicated spectral dependence of true foreground components, or as a result of a spatial dependence of spectral parameters. The former problem is inherent to all parametric component separation approaches as the one assumed here. In general, a wrong parametrization or frequency scaling laws assumed in such approaches may invalidate separa-

tion results. In practice, the effects are more subtle but arising biases can affect an interpretation of the results. This is therefore important that the scaling laws assumed in the optimization are kept on being improved on reflecting any relevant, new observational data and more detailed, theoretical models of the foreground physics as they become available. In a case of some doubts a rather conservative approach of restricting channel frequencies to a range for which the scaling laws are known to provide at least good approximations to the actual ones, can be fruitful. This is in fact an approach we used in this work by selecting a parametric model for the dust signal with a single parameter and reduced the frequency range to those lower than 400GHz.

A spatial dependence of the scaling parameters can be treated more directly. We will implement that by dividing the observed sky into multiple disjoint regions and introduce one set of parameters for each of those. To abstract from details of the regions shape and position, we assume that they are defined in such a way that the errors on spectral parameters are the same for each of the regions, i.e., that the differences of the overall magnitude of the matrix $\hat{\mathbf{F}}$ are compensated by a respective number of pixels in each area. In general this assumption would imply that more, though smaller by area, regions are defined in high foreground contrast sky areas. This indeed could well be the case as the high-contrast foreground regions are expected to be more complex and may require more parameters to ensure sufficient accuracy. For demonstration purposes we assume that we have 10 regions with the corresponding errors on spectral parameters being $\sqrt{10}$ times larger than in the single region case as studied before. We note that cutting the sky into regions will unavoidably affect the foregrounds and thus residual power spectrum on the scales larger than a typical size of the region. We will ignore this effect here, motivated by the fact that our earlier results did not find any strong dependence on the shape of the power spectrum. We also neglect here all practical difficulties such as matching the results on the map level coming from the different regions and which will have to be addressed in any actual application of the discussed method. We limit here ourselves to the CORe-like configuration as defined earlier, calculate the FOMs as before, and optimize the configuration following the steps outlined before. As expected we find that the optimal configurations found this time are not very different from the ones obtained earlier. This is because FOM#1 and #3 are mostly trying to optimize the overall noise level, and which is the same now as before, and though the value of FOM#2 increased by a factor 10 due to increase of the spectral index errors this is the same configuration, which ensures its minimum. As a consequence the new value of r_{eff} is now higher than that of r_{min} . This clearly does not invalidate results of the optimization procedure as such, however a care has to be exercised, while interpreting the obtained values of r_{min} , which may not be taken directly as the performance forecasts for the set-up as far as detecting r

is concerned.

E. Varying the number of channels and their frequencies

We present here some results based on an implementation of the scheme proposed in Sect. II C. We start from ~ 70 channels evenly spaced between 45 and 375GHz every 5GHz, with ~ 6000 detectors (total number of the CORe proposed version) equally distributed among those, as shown in Fig. 14. Then we preform the optimization with respect to FOM#1, while keeping $FOM\#2 \leq 10^{-4}$ and the total number of detectors fixed. As a result we obtain a highly clustered distribution of detectors in between the initial channels, with many of these being empty. We therefore combine together detectors of neighboring channels and replace them by a new channel with the central frequency set as a weighted, by a number of detectors, mean of the optimized distribution. The new channels are defined to ensure proper spacing between them. Once the new channels are determined we perform a second round of the optimization, this time invoking only the new channels and aiming at optimization of the detector distribution between them. The result is shown in the left bottom panel of Fig. 14. We note that the procedure not only improved on the values of the FOMs with respect to the starting (original) configuration, i.e., FOM#1 has been decreased by $\sim 17\%$ ($\sim 25\%$), while the noise by a factor ~ 4 (~ 3), but also, and arguably most importantly, it resulted in a configuration significantly simpler than the initial one with the number of channels reduced from 70 down to 9.

We note that maybe somewhat surprisingly both the configurations derived here, the final one as well as the intermediate one obtained after the first optimization step, show only a minor, \sim few percent, gain over the 5-channel configuration we have considered earlier, see, e.g., first column of Table VI. This is due to our setting the threshold for FOM#2 rather high, while the main advantage of the significantly larger set of the initial channels used here is that it permits finding in principle more satisfactory compromises between the three FOMs, characterized by values of FOM#2 lower than what could be achieved with more modest set-ups discussed earlier.

V. CONCLUSIONS

In this work we have proposed a general scheme for a performance optimization and forecasting of the CMB B-mode experiments in the presence of astrophysical foregrounds. Our approach is based on a maximum likelihood parametric technique for component separation, for which we have derived Fisher-like error estimates for spectral parameters. We use the latter to calculate the residual level of the foregrounds in cleaned CMB maps given assumed, instrument characteristics and fore-

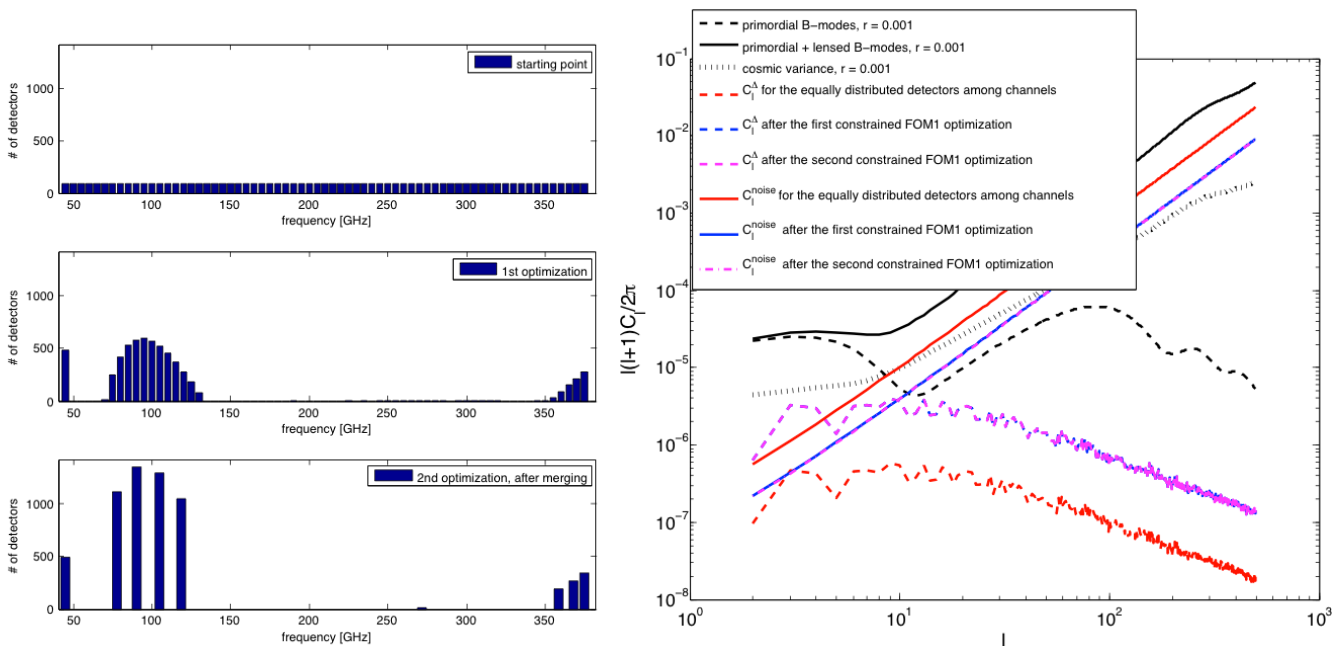


FIG. 14: Demonstration of the optimization results derived with respect to a variable number of channels, numbers of detectors per channel, and their central frequencies, while constraining the total number of detectors (= 6128 as in the proposed CORe version). *Upper left panel* shows, from top to bottom, (1) the starting configuration with all the detectors evenly distributed among a fine-grid of channels; (2) a configuration after the first optimization of FOM#1 constrained to ensure that $\text{FOM}\#2 \leq 10^{-4}$, (3) the re-optimization of configuration (2) restricted only to channels with a number of detectors larger than 5 and after adjacent channels merging and re-centering as described in Sect. IV E. *Right panel* shows power spectra corresponding to these configurations contrasted against the expected CMB signals.

ground model. We then optimize the former by minimizing a set of proposed figure of merit (FOM) indicators, which reflect our science goals. Subsequently we have applied this approach to two specific cases of recently proposed CMB B-mode satellites: American CMBpol [4] and European CORe [3]. We have discussed in detail the choices and trade-offs inevitable in such an optimization process. We have demonstrated how such a procedure can help to simplify the resulting hardware design, while ensuring the same (or nearly the same) science outcome.

We emphasize that results of such a procedure can be only as reliable as the foreground models, which are applied. This underlines the import of developing better understanding of the polarized foregrounds, in particular, and characteristically of the parametric methods, as far as the functional form of the foreground component scaling laws is concerned. However, our approach is expected to be relatively robust as far as other details of the foreground signals are concerned, such as, spatial distribution or spatial variability of the spectral parameters, with the latter playing a major role in determining the scientific reach of the experiment but not affecting its configuration.

We also note here that the presented framework could be extended to work with any component separation method, which implements the separation by first es-

timating the mixing matrix, in a parametric or non-parametric way, and which is capable of producing estimates for the errors of the spectral parameters for any hardware configuration. One could, and ideally would, therefore use the formalism proposed here to define configurations, which would ensure that many of the available component separation methods perform well. Though the component separation methods usually conform with the first requirement, the second is more demanding and typically it can be done only via computationally-heavy Monte Carlo simulations. Those may be often impractical for the optimization purposes, making an implementation of such a program difficult. A related, but simpler to address, problem is whether the configurations optimized with one method will work for satisfactorily with the others. We will leave an investigation of both these issue to future work.

As we point out in the introduction, FOMs required for the optimization procedure are also suitable for the performance forecasting. This also clearly applies to the FOMs proposed here and in particular FOM#1 and #2 seem relevant to the primordial signal detection producing values of r_{min} and r_{eff} on order of $\mathcal{O}(10^{-4})$ for the considered optimized configurations. However, given that each of these two FOMs reflects a somewhat different aspect of the problem – a statistical uncertainty in

former cases versus a systematic one in the latter – a care has to be taken while interpreting these values. Nevertheless, as is, our results seem to support at least the contentions made elsewhere suggesting that $r \simeq 10^{-3}$ is a realistic goal for the experiments considered here.

Finally, we point out that the science goals we have posed for the considered CMB experiments are clearly more modest than those targeted by the original CMBpol and CORe designs. This is responsible, at least in part, for the more complex and advanced instrumental configurations as proposed in the original proposal. More diverse science goals can, and should, be studied in the presented framework. We leave this as well as considerations of other possible extensions,

e.g., an inclusion of some of the instrumental effects, to future work.

Acknowledgments

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APPENDIX A: SPECTRAL LIKELIHOOD DERIVATIVES.

We present here some details of the derivation of Eqs. (4) & (5).
First from Eq. (3) we have,

$$\frac{\partial \ln \mathcal{L}}{\partial \beta} = \sum_p (\mathbf{A}_{,\beta} \bar{\mathbf{s}}_p)^t \mathbf{N}^{-1} (\mathbf{d}_p - \mathbf{A} \bar{\mathbf{s}}_p) \quad (\text{A1})$$

from which the second derivatives of the spectral likelihood follow as,

$$\frac{\partial^2 \ln \mathcal{L}}{\partial \beta \partial \beta'} = \sum_p \left\{ (\mathbf{A}_{,\beta\beta'} \mathbf{s}_p + \mathbf{A}_{,\beta} \mathbf{s}_{p,\beta'})^t \mathbf{N}^{-1} (\mathbf{d}_p - \mathbf{A} \mathbf{s}_p) - (\mathbf{A}_{,\beta} \mathbf{s}_p)^t \mathbf{N}^{-1} (\mathbf{A}_{,\beta'} \mathbf{s}_p + \mathbf{A} \mathbf{s}_{p,\beta'}) \right\} \quad (\text{A2})$$

And the noise ensemble average reads,

$$\begin{aligned} \left\langle \frac{\partial^2 \ln \mathcal{L}}{\partial \beta \partial \beta'} \right\rangle_{noise} &= \sum_p \left\{ \text{tr} \left[\mathbf{A}_{,\beta\beta'}^t \mathbf{N}^{-1} \langle (\mathbf{d} - \mathbf{A} \mathbf{s}_p) \mathbf{s}_p^t \rangle_{noise} \right] - \text{tr} \left[\mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \mathbf{A}_{,\beta'} \langle \mathbf{s}_p \mathbf{s}_p^t \rangle_{noise} \right] \right. \\ &\quad \left. + \text{tr} \left[\mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \langle (\mathbf{d}_p - \mathbf{A} \mathbf{s}_p) \mathbf{s}_{p,\beta'}^t \rangle_{noise} \right] - \text{tr} \left[\mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \mathbf{A} \langle \mathbf{s}_{p,\beta'} \mathbf{s}_p^t \rangle_{noise} \right] \right\}. \end{aligned} \quad (\text{A3})$$

From Eqs. (1) & (2) we now have,

$$\langle \mathbf{s}_p \mathbf{s}_p^t \rangle_{noise} = \bar{\mathbf{s}}_p \bar{\mathbf{s}}_p^t + (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1}, \quad (\text{A4})$$

$$\begin{aligned} \langle \mathbf{s}_p \mathbf{s}_{p,\beta'}^t \rangle_{noise} &= -\bar{\mathbf{s}}_p \bar{\mathbf{s}}_p^t (\mathbf{A}_{,\beta'}^t \mathbf{N}^{-1} \mathbf{A} + \mathbf{A}^t \mathbf{N}^{-1} \mathbf{A}_{,\beta'}) (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} + \bar{\mathbf{s}}_p \bar{\mathbf{q}}_{p(\beta')}^t \\ &\quad - (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} (\mathbf{A}_{,\beta'}^t \mathbf{N}^{-1} \mathbf{A}) (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \end{aligned} \quad (\text{A5})$$

$$\begin{aligned} \langle (\mathbf{d}_p - \mathbf{A} \mathbf{s}_p) \mathbf{s}_p^t \rangle_{noise} &= (\hat{\mathbf{A}} \hat{\mathbf{s}} - \mathbf{A} \bar{\mathbf{s}}_p) \bar{\mathbf{s}}_p^t \\ \langle (\mathbf{d}_p - \mathbf{A} \mathbf{s}_p) \mathbf{s}_{p,\beta'}^t \rangle_{noise} &= -(\hat{\mathbf{A}} \hat{\mathbf{s}} - \mathbf{A} \bar{\mathbf{s}}_p) \bar{\mathbf{s}}_p^t (\mathbf{A}_{,\beta'}^t \mathbf{N}^{-1} \mathbf{A} + \mathbf{A}^t \mathbf{N}^{-1} \mathbf{A}_{,\beta'}) (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \\ &\quad + (\hat{\mathbf{A}} \hat{\mathbf{s}} - \mathbf{A} \bar{\mathbf{s}}_p) \bar{\mathbf{q}}_{p(\beta')}^t + \mathbf{A}_{,\beta'} (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \\ &\quad + \mathbf{A} (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} (\mathbf{A}_{,\beta'}^t \mathbf{N}^{-1} \mathbf{A}) (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \end{aligned} \quad (\text{A6})$$

where $\hat{\mathbf{A}}$ and $\hat{\mathbf{s}}$ are the true mixing matrix and sky components, respectively, $\bar{\mathbf{s}}$ is a component estimate in a case of noiseless experiment, i.e.,

$$\bar{\mathbf{s}}_p \equiv (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \mathbf{A} \mathbf{N}^{-1} \hat{\mathbf{A}} \hat{\mathbf{s}}_p \quad (\text{A7})$$

and $\bar{\mathbf{q}}_{p(\beta)}$ is defined as,

$$\bar{\mathbf{q}}_{p(\beta')} \equiv (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \mathbf{A}_{,\beta'} \mathbf{N}^{-1} \hat{\mathbf{A}} \hat{\mathbf{s}}_p. \quad (\text{A8})$$

Hence,

$$\left\langle \frac{\partial^2 \ln \mathcal{L}}{\partial \beta \partial \beta'} \right\rangle_{noise} = - \sum_p \left\{ (\mathbf{A}_{,\beta\beta'} \bar{\mathbf{s}}_p)^t \mathbf{N}^{-1} (\mathbf{A} \bar{\mathbf{s}}_p - \hat{\mathbf{A}} \hat{\mathbf{s}}_p) + (\mathbf{A}_{,\beta} \bar{\mathbf{s}}_p)^t \mathbf{N}^{-1} (\mathbf{A}_{,\beta'} \bar{\mathbf{s}}_p) \right. \quad (\text{A9})$$

$$\begin{aligned} &+ \text{tr} \left[\mathbf{A}_{,\beta}^t \mathbf{N}^{-1} (\hat{\mathbf{A}} \hat{\mathbf{s}}_p - \mathbf{A} \bar{\mathbf{s}}_p) \bar{\mathbf{s}}_p^t (\mathbf{A}_{,\beta'}^t \mathbf{N}^{-1} \mathbf{A} + \mathbf{A}^t \mathbf{N}^{-1} \mathbf{A}_{,\beta'}) (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \right] \\ &- \text{tr} \left[(\mathbf{A}_{,\beta} \bar{\mathbf{q}}_{p(\beta')})^t \mathbf{N}^{-1} (\hat{\mathbf{A}} \hat{\mathbf{s}}_p - \mathbf{A} \bar{\mathbf{s}}_p) \right] \\ &- \text{tr} \left[\mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \mathbf{A} (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} (\mathbf{A}_{,\beta'}^t \mathbf{N}^{-1} \mathbf{A} + \mathbf{A}^t \mathbf{N}^{-1} \mathbf{A}_{,\beta'}) \bar{\mathbf{s}}_p \bar{\mathbf{s}}_p^t \right] \\ &+ \text{tr} \left[\mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \mathbf{A} \bar{\mathbf{q}}_{p(\beta')} \bar{\mathbf{s}}_p^t \right] \}. \end{aligned} \quad (\text{A10})$$

Moreover assuming now the true values of the spectral indices, i.e., $\beta = \hat{\beta}$,

$$\begin{aligned} \left\langle \frac{\partial^2 \ln \mathcal{L}_{profile}}{\partial \beta \partial \beta'} \right\rangle_{noise} \Big|_{\beta=\hat{\beta}} &= - \text{tr} \left[\mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \mathbf{A}_{,\beta'} \sum_p \hat{\mathbf{s}}_p \hat{\mathbf{s}}_p^t \right] \\ &+ \text{tr} \left[\mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \mathbf{A} (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} (\mathbf{A}_{,\beta'}^t \mathbf{N}^{-1} \mathbf{A} + \mathbf{A}^t \mathbf{N}^{-1} \mathbf{A}_{,\beta'}) \sum_p \hat{\mathbf{s}}_p \hat{\mathbf{s}}_p^t \right] \\ &- \text{tr} \left[\mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \mathbf{A} (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \mathbf{A}_{,\beta'}^t \mathbf{N}^{-1} \mathbf{A} \sum_p \hat{\mathbf{s}}_p \hat{\mathbf{s}}_p^t \right] \\ &= \text{tr} \left\{ \left[\mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \mathbf{A} (\mathbf{A}^t \mathbf{N}^{-1} \mathbf{A})^{-1} \mathbf{A}^t \mathbf{N}^{-1} \mathbf{A}_{,\beta'} - \mathbf{A}_{,\beta}^t \mathbf{N}^{-1} \mathbf{A}_{,\beta'} \right] \sum_p \hat{\mathbf{s}}_p \hat{\mathbf{s}}_p^t \right\}, \end{aligned} \quad (\text{A11})$$

from which Eq. (5) follows.

APPENDIX B: FISHER MATRIX ALGEBRA.

The Fisher matrix can be expressed as [24],

$$F_{\alpha\beta} \equiv \left\langle \frac{\partial^2 \ln \mathcal{L}}{\partial \lambda_\alpha \partial \lambda_\beta} \right\rangle = \frac{1}{2} \text{Tr} [\mathbf{C}_{,\alpha} \mathbf{C}^{-1} \mathbf{C}_{,\beta} \mathbf{C}^{-1}] \quad (\text{B1})$$

where \mathbf{C} is the covariance matrix and λ is some parameter.

In our case, $\lambda_\alpha = \lambda_\beta = r$, the tensor-to-scalar ratio, while the covariance matrix in a harmonic space, \mathbf{C} , is given by,

$$\mathbf{C} \equiv \mathbf{C}_{jj'} \equiv \langle a_{lm} a_{l'm'}^\dagger \rangle, \quad (\text{B2})$$

where,

$$\begin{aligned} j &= \ell^2 + \ell + m, \\ \ell &= \text{round} [(-1 + \sqrt{1 + 4j})/2], \\ m &= j - \ell(\ell + 2), \end{aligned} \quad (\text{B3})$$

and thus j goes from 0 to $(\ell_{max} + 1)^2 - 1$. The function *round* rounds a real number to a *closest* integer. The Fisher matrix expression can be now specialized as,

$$F_{rr} = \frac{1}{2} \sum_{j,j'} \frac{\partial C_\ell}{\partial r} [\mathbf{C}^{-1}]_{jj'}^2 \frac{\partial C_{\ell'}}{\partial r}. \quad (\text{B4})$$

where j (j') is related to ℓ (ℓ') as in Eqs. (B3).

As there are three uncorrelated contributions to the overall signal, which are CMB, noise and foreground residuals, we can write,

$$\begin{aligned} \mathbf{C}_{jj'} &= \langle a_{lm}^{CMB} a_{l'm'}^{CMB,\dagger} \rangle + \langle a_{lm}^{noise} a_{l'm'}^{noise,\dagger} \rangle + \langle a_{lm}^{res} a_{l'm'}^{res,\dagger} \rangle \\ &= C_l^{CMB} \delta_{jj'} + C_l^{noise} \delta_{jj'} + f_j f_{j'}^\dagger \\ &\equiv D_{jj'} + f_j f_{j'}^\dagger \end{aligned} \quad (\text{B5})$$

where f_j stands for a vector of a_{lm}^{res} coefficients arranged according to the j index.

To compute the \mathbf{C}^{-1} matrix used in equation (B1), we can use the Sherman-Morrison formula obtaining,

$$\mathbf{C}^{-1} = \mathbf{D}^{-1} - \mathbf{D}^{-1} f (1 + f^\dagger \mathbf{D}^{-1} f)^{-1} f^\dagger \mathbf{D}^{-1} \quad (\text{B6})$$

where $(1 + f^\dagger \mathbf{D}^{-1} f)^{-1}$ is a number and hence,

$$\mathbf{C}^{-1} = \mathbf{D}^{-1} - \frac{\mathbf{D}^{-1} f f^\dagger \mathbf{D}^{-1}}{(1 + f^\dagger \mathbf{D}^{-1} f)}, \quad (\text{B7})$$

what given that $[D^{-1}]_{jj'} = (1/C_\ell) \delta_{jj'}$ becomes,

$$[\mathbf{C}^{-1}]_{jj'} = \frac{\delta_{jj'}}{C_\ell} - \frac{C_\ell^{-1} C_{\ell'}^{-1} f_j f_{j'}^\dagger}{1 + \sum_{\ell''=0}^{\ell_{max}} (2\ell'' + 1) \frac{C_{\ell''}^\Delta}{C_{\ell''}}}, \quad (\text{B8})$$

where C_ℓ^Δ is a residuals power spectrum, Eq. (12), defined here as,

$$C_\ell^\Delta \equiv \frac{1}{2\ell + 1} \sum_{m=\ell^2}^{\ell^2+2\ell} |f_m|^2. \quad (\text{B9})$$

So now we have finally,

$$[\mathbf{C}^{-1}]_{jj'}^2 = \frac{\delta_{jj'}}{C_\ell^2} - \frac{2 f_j f_j^\dagger}{C_\ell^3 \left(1 + \sum_{\ell''=0}^{\ell_{max}} (2\ell'' + 1) \frac{C_{\ell''}^\Delta}{C_{\ell''}} \right)} \delta_{jj'} + \frac{f_j^2 f_{j'}^{\dagger 2}}{C_\ell^2 C_{\ell'}^2 \left(1 + \sum_{\ell''=0}^{\ell_{max}} (2\ell'' + 1) \frac{C_{\ell''}^\Delta}{C_{\ell''}} \right)^2}, \quad (\text{B10})$$

which inserted into Eq. (B4) gives Eq. (15).