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# Determining the vortex tilt relative to a superconductor surface

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It is of interest to determine the exit angle of a vortex from a superconductor surface, since this affects the intervortex interactions and their consequences. Two ways to determine this angle are to image the vortex magnetic fields above the surface, or the vortex core shape at the surface. In this work we evaluate the field  $\mathbf{h}(x, y, z)$  above a flat superconducting surface  $x, y$  and the currents  $\mathbf{J}(x, y)$  at that surface for a straight vortex tilted relative to the normal to the surface, for both the isotropic and anisotropic cases. In principle, these results can be used to determine the vortex exit tilt angle from analyses of magnetic field imaging or density of states data.

## I. INTRODUCTION

In the long history of studying vortices and vortex lattices with the help of surface probes (e.g. Bitter decoration [1, 2], Hall bar microscopy [3], magnetic force microscopy [4], scanning Superconducting QUantum Interference Device microscopy (SSM) [5], or scanning tunneling microscopy (STM) [6]) vortices were commonly assumed to exit the superconductor perpendicular to the surface. H. Hess and collaborators were the first to examine vortex lattices in NbSe<sub>2</sub> in tilted fields [6] using STM. They found a peculiar “comet-like” density of states (DOS) distribution near the vortex core. Recently, the STM group of H. Suderow concluded that the vortex lattice structure in fields tilted relative to a plane surface of nearly isotropic  $\beta$ -Bi<sub>2</sub>Pd is affected by the surface contribution to the vortex-vortex interactions due to vortex stray fields outside the sample [7].

The question then arises as to whether one can determine the vortex orientation relative to the surface by measuring the field above the sample surface or the DOS at the surface for a superconductor containing vortices. This question is addressed in this paper.

There has already been a great deal of work on the structure of vortices near and above a sample surface. Abrikosov [8] used Ginzburg-Landau theory to determine the structure of a vortex lattice in a bulk, isotropic superconductor. Pearl calculated the current distribution of quantized fluxoids in superconducting thin films [9] and the currents and fields of vortices near and above a superconductor-vacuum interface [10]. Brandt [11] described a method for calculating the properties of a distorted flux line lattice near a planar surface using the London theory. Buisson *et al.* [12] generalized this study for the case of mass anisotropy orthogonal to the surface. Kogan, Simonov and Ledvij (KSL) [13] considered a uniaxial crystal with a surface in an arbitrary crystal plane and a vortex with arbitrary orientation relative to the crystal within the general anisotropic London approach. Carneiro and Brandt [14] gave general expressions for the magnetic field and energy of straight and curved vor-

trices in an anisotropic superconductor of finite thickness within anisotropic London theory.

Here we apply the formalism of KSL [13] to the problem of currents near and fields above the surface for a tilted vortex in an anisotropic superconductor. The KSL formalism is quite general, but this “generality” make the results quite cumbersome and not easily applied. Besides, it is unclear which features of the field distribution outside, or of the DOS at the interface, are due to the vortex tilt and which are due to crystal anisotropy.

For this reason, we focus here first on the isotropic half-space superconductor at  $z < 0$  and a straight vortex approaching the interface  $z = 0$  at an angle  $\theta$  with the normal  $\hat{z}$  to the surface. For  $\theta = 0$  this problem has been solved by J. Pearl [10]. We find that even in the isotropic case, the field distribution above the surface and the currents  $\mathbf{J}(x, y)$  flowing at the surface carry measurable signs of the vortex tilt. The stray field  $h_z(x, y; z)$  can, in principle, be measured by field sensitive probes such as scanning Hall bar or scanning SQUID, whereas  $|J(x, y)|$  affects the pair potential and DOS probed by STM.

In the second part of this paper, we consider tilted vortices in uniaxial superconductors with the surface in the  $ab$  plane.

## II. ISOTROPIC CASE

The formal method we use is straightforward and not new: one solves the London equations inside the superconductor, the Maxwell equations outside, and match the solutions with proper boundary conditions [10, 12–15].

The field  $\mathbf{h}$  outside the superconductor satisfies  $\text{div } \mathbf{h} = \text{curl } \mathbf{h} = 0$ , so that one can look for this field as  $\mathbf{h} = \nabla\varphi$  with the potential  $\varphi$  obeying the Laplace equation  $\Delta\varphi = 0$ . The general solution of this equation in the upper half-space  $z > 0$  for  $\varphi \rightarrow 0$  as  $z \rightarrow \infty$  is:

$$\varphi(\mathbf{r}, z) = \int \frac{d^2\mathbf{k}}{4\pi^2} \varphi(\mathbf{k}) e^{i\mathbf{k}\mathbf{r} - kz}, \quad (1)$$

where

$$\varphi(\mathbf{k}, z) = \int d^2\mathbf{r} \varphi(\mathbf{r}, z) e^{-i\mathbf{k}\mathbf{r} - kz} \quad (2)$$

is the two dimensional (2D) Fourier transform of the potential  $\varphi$ ,  $\mathbf{r} = (x, y)$ ,  $\mathbf{k} = (k_x, k_y)$ .

Inside the superconductor, the field components satisfy the London equations

$$h_i - \lambda^2 \Delta h_i = \Phi_0 \hat{v}_i \delta(x_0, y_0). \quad (3)$$

Here  $\Delta = \nabla^2 + \partial^2/\partial z^2$  with the 2D Laplacian  $\nabla^2$ ;  $\hat{v}$  is the unit vector along the vortex axis, and  $(x_0, y_0)$  are the coordinates in the plane perpendicular to the vortex axis  $\hat{v}$ . For an infinite vortex along  $z_0$  in uniform material, the coordinates  $(x_0, y_0, z_0)$  are the best, because nothing depends on  $z_0$ . In the case of a vortex crossing the surface of superconducting half-space, this feature is lost, and the coordinates  $(x, y, z)$  with  $z = 0$  being the sample surface are more convenient. The delta-function at the right-hand side (RHS) becomes  $\delta(x_0)\delta(y_0) = \delta(x \cos \theta - z \sin \theta)\delta(y)$  where  $\theta$  is the angle between  $z$  and  $v$ , the ‘‘tilt’’ angle, and  $y$ -axis is chosen to have  $v_y = 0$ .

The solution of the system (3) of linear differential equations is the sum of its particular solution and of the solution  $\mathbf{h}^s$  of the homogeneous equation with zero RHS. To have a correct singular behavior at the vortex axis, we choose the particular solution as the well-known field of an infinite straight vortex  $\mathbf{h}^v$ :

$$\mathbf{h} = \mathbf{h}^v + \mathbf{h}^s. \quad (4)$$

After taking a 2D  $x, y$  Fourier transform of Eq. (3) one obtains at  $z = 0$  (see App. A of Ref. [15]):

$$h_x^v(\mathbf{k}) = \frac{\Phi_0 \tan \theta}{\lambda^2 Q^2}, \quad h_y^v = 0, \quad h_z^v(\mathbf{k}) = \frac{\Phi_0}{\lambda^2 Q^2}; \quad (5)$$

$$Q^2 = \lambda^{-2} + k^2 + k_x^2 \tan^2 \theta. \quad (6)$$

Further, the 2D Fourier transform turns the homogeneous Eq. (3) into a system of ordinary differential equations for  $h_i^s(\mathbf{k}, z)$  in the variable  $z$ ,

$$h_i^s \lambda^{-2} + k^2 h_i^s - \partial^2 h_i^s / \partial z^2 = 0, \quad (7)$$

with solutions:

$$h_i^s(\mathbf{k}, z) = H_i(\mathbf{k}) e^{qz}, \quad q^2 = \lambda^{-2} + k^2. \quad (8)$$

Note that all components of  $\mathbf{h}^s$  decay exponentially with the characteristic length  $1/q = \lambda/\sqrt{1 + \lambda^2 k^2}$ .

Note also that  $H_i$  are not independent: by choosing the particular solution as the field of an infinite vortex which obeys  $\text{div } \mathbf{h}^v = 0$ , we impose the same condition on  $\mathbf{h}^s$ :

$$ik_x H_x + ik_y H_y + q H_z = 0. \quad (9)$$

The boundary conditions of the field continuity at  $z = 0$  read in  $\mathbf{k}$  space:

$$\begin{aligned} ik_x \varphi &= h_x^v + h_x^s, \\ ik_y \varphi &= h_y^v + h_y^s, \\ -k \varphi &= h_z^v + h_z^s. \end{aligned} \quad (10)$$

Along with Eqs. (5) and (9) these conditions give for the external potential

$$\varphi(\mathbf{k}, z) = -\frac{\Phi_0 e^{-kz}}{\lambda^2 k(k+q)(q - ik_x \tan \theta)}, \quad (11)$$

and for the coefficients  $H_i$ :

$$\begin{aligned} H_x &= -\Phi_0 \frac{(k_y^2 + kq) \tan \theta + ik_x q}{\lambda^2 k(k+q)Q^2}, \\ H_y &= -\Phi_0 \frac{ik_y (ik_x \tan \theta + q)}{\lambda^2 k(k+q)Q^2}, \\ H_z &= \Phi_0 \frac{ik_x \tan \theta - k}{\lambda^2 (k+q)Q^2}. \end{aligned} \quad (12)$$

### A. Distribution of the field $h_z(x, y, z)$

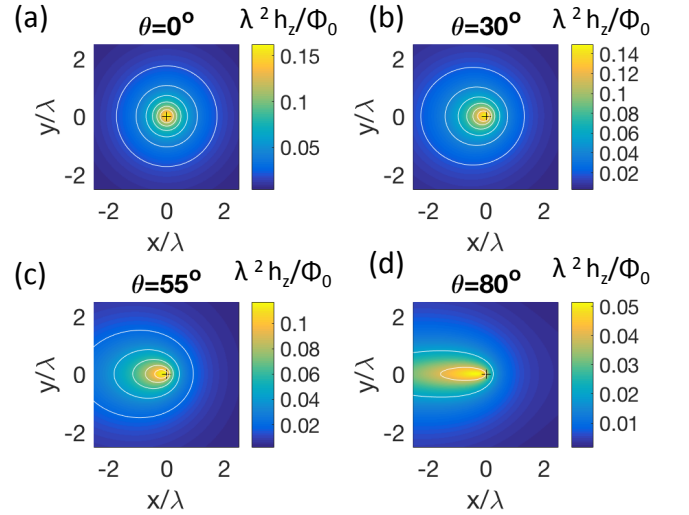


FIG. 1. (Color online) Normalized  $z$ -component of the magnetic fields  $\lambda^2 h_z / \Phi_0$  at height  $z = 0.1\lambda$  above a superconducting surface for a tilted vortex in the isotropic case. The contours of constant  $h_z$  (white) are at  $\lambda^2 h_z / \Phi_0 = 0.02, 0.04, 0.06, 0.08, 0.10$  and  $0.12$ . The ‘+’ symbols mark the centers of the vortex coordinate system where the vortex axis touches the surface.

From the potential (11) we get the  $z$  component of the field outside:

$$h_z(\mathbf{k}, z) = \frac{\Phi_0 e^{-kz}}{\lambda^2 (k+q)(q - ik_x \tan \theta)}. \quad (13)$$

In principle, this field can be measured in scanning Hall bar or SQUID experiments. Figure 1 shows results of numerical inversion of this Fourier transform to real space. The vortex fields above the sample surface become weaker and more elongated in the tilt ( $x$ ) direction as the tilt angle increases.

To characterize asymmetry of the field  $h_z$  for tilted vortices, we plot in Fig. 2 the fields  $h_z(x, 0)$  for the tilts of

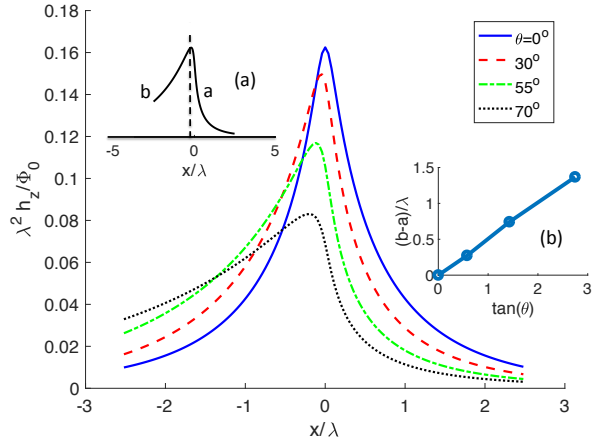


FIG. 2. (Color online) Normalized z-component of the magnetic fields  $h_z(x, 0)$  at height  $z = 0.1\lambda$  above the surface for tilted vortices in the isotropic case. Inset (a): definitions of  $a$  and  $b$  to characterize the curves' asymmetry. Inset (b):  $b - a$  vs  $\tan \theta$  extracted from curves in the main panel.

Fig. 1. Clearly, asymmetry increases with increasing  $\theta$ . A simple way to quantify this asymmetry is to consider the half-width of dome-like curves  $h_z(x, 0)$  as consisting of two parts,  $a$  and  $b$ , separated by the position of the curve maximum, see Fig. 2. For  $\theta = 0$ ,  $h_z(x, 0) = h_z(-x, 0)$ , and  $b - a = 0$ . Since the angle  $\theta$  enters  $h_z(\mathbf{k}, \theta)$  only via  $\tan \theta$ , we plot  $a - b$  vs  $\tan \theta$  to see that in a broad domain of angles  $(b - a) \propto \tan \theta$ . In fact, Fig. 2 for  $z = 0.1\lambda$  suggests an empirical relation  $(b - a) \approx 0.5\lambda \tan \theta$ . Thus, measuring the asymmetry  $b - a$  one can estimate the tilt angle  $\theta$ .

### B. Supercurrents $J(x, y)$ at the surface

Supercurrents flowing at the surface affect the order parameter and the DOS measured by STM. It is not easy to track this connection for arbitrary temperatures. For a qualitative argument we can use the Ginzburg-Landau theory which gives a simple relation for the order parameter suppression by current,  $\Delta^2 = \Delta_0^2(1 - J^2/4J_d^2)$ , where  $\Delta_0$  corresponds to zero-current and  $J_d = c\Phi_0/16\pi^2\lambda^2\xi$  is on the order of the depairing current ( $\xi$  is the coherence length) [16]. According to deGennes the zero-bias density of states  $N$  in the vortex vicinity is related to the order parameter as  $N(\mathbf{r})/N_0 = 1 - \Delta^2(\mathbf{r})/\Delta_0^2$  [17]. This suggests that the contours  $J^2(x, y) = \text{const}$  should be close to the DOS contours  $N(x, y) = \text{const}$ . Of course, the London approach employed here cannot be trusted at distances on the order  $\xi$ , where the current approaches the depairing value. Still, being interested in a qualitative description of the vortex core shape at the sample surface, one can study the function  $J^2(x, y)$ .

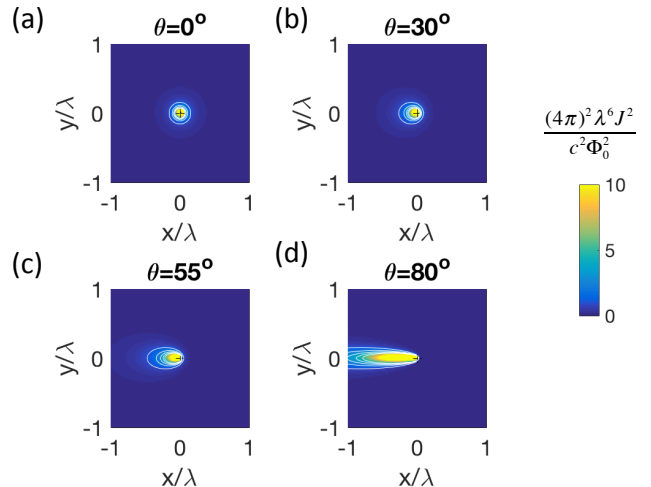


FIG. 3. (Color online) Normalized absolute value squared of the vortex currents  $(4\pi)^2 \lambda^6 J^2 / c^2 \Phi_0^2$  at the superconducting surface in the isotropic case. The tilt angle of the vortex relative to the sample surface  $\theta = 0^\circ$  (a),  $30^\circ$  (b),  $55^\circ$  (c), and  $80^\circ$  (d). The contours of constant  $J^2$  (white) are at  $(4\pi)^2 \lambda^6 J^2 / c^2 \Phi_0^2 = 1, 2, 3, 4,$  and  $5$ . The '+' symbol marks the center of the vortex coordinate system where the vortex axis touches the surface.

The part of the current at  $z = 0$  associated with the unperturbed tilted vortex has been given in [15]:

$$J_x^v(\mathbf{k}) = \frac{c\Phi_0}{4\pi\lambda^2} \frac{ik_y}{Q^2}, \quad (14)$$

$$J_y^v(\mathbf{k}) = -\frac{c\Phi_0}{4\pi\lambda^2} \frac{ik_x}{Q^2 \cos^2 \theta}. \quad (15)$$

The contribution to the current due to the field  $\mathbf{h}^s$  of Eq. (8) at  $z = 0$  follows from Maxwell's equations:

$$\frac{4\pi}{c} J_x^s(\mathbf{k}) = ik_y H_z(\mathbf{k}) - qH_y(\mathbf{k}). \quad (16)$$

$$\frac{4\pi}{c} J_y^s(\mathbf{k}) = qH_x(\mathbf{k}) - ik_x H_z(\mathbf{k}), \quad (17)$$

It is worth noting that the continuity of the tangential fields  $h_{x,y}$  assures also the continuity of their tangential derivatives, in other words, the continuity of the normal current component  $J_z$ . But  $J_z = 0$  outside the sample and so does the normal component of the total current inside  $(\mathbf{J}^v + \mathbf{J}^s)_z = 0$  at the interface.

Hence, we can evaluate the current value at the surface in real space:

$$J^2(x, y) = (J_x^s + J_x^v)^2 + (J_y^s + J_y^v)^2. \quad (18)$$

Some numerical evaluations of Eq. 18 are displayed in Figures 3 and 4. For these calculations we applied a high frequency filter by multiplying the right hand sides of Eqs. (14)–(17) by  $e^{-k^2 dz^2}$  with  $dz = 0.01\lambda$ . This damps out high frequency artifacts at  $x = 0$  and  $y = 0$  without significantly affecting the low frequency properties of the solutions. The false color scale in Fig. 3 is

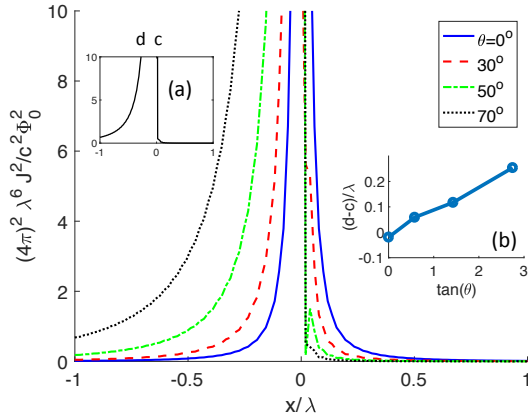


FIG. 4. (Color online) Cross-sections through  $y = 0$  of the vortex currents  $(4\pi)^2\lambda^6 J^2/c^2\Phi_0^2$  at the superconducting surface in the isotropic case. The tilt angle of the vortex relative to the sample surface  $\theta = 0^\circ, 30^\circ, 55^\circ$ , and  $70^\circ$ . Inset (a) defines  $c$  and  $d$ , the values of  $|x|$  when  $(4\pi)^2\lambda^6 J^2/c^2\Phi_0^2 = 10$ . Inset (b) plots  $d - c$  as a function of  $\tan(\theta)$ .

saturated at  $(4\pi)^2\lambda^6 J^2/c^2\Phi_0^2 = 10$ . Since physically the core shape (as observed in e.g. STM) is determined by a contour where  $J$  reaches the depairing value, the contours  $J^2(x, y) = \text{constant}$  will also give the contours of  $\text{DOS}(x, y) = \text{constant}$ : the observed vortex cores will become more elongated along the tilt ( $x$ ) direction as the tilt angle increases. To avoid misunderstanding, we stress that the white curves in Fig. 3 are contours  $J^2(x, y) = \text{const}$ , not the stream lines of the vector  $\mathbf{J}(x, y)$ .

Figure 4 plots cross-sections through  $y = 0$  of the calculated vortex currents of Fig. 3 in the isotropic case for various vortex tilt angles  $\theta$ . The inset Fig. 4a diagrams the intercepts  $c$  and  $d$  where  $\bar{j}^2 \equiv (4\pi)^2\lambda^6 J^2/c^2\Phi_0^2 = 10$ . Fig. 4b plots  $(d-c)/\lambda$ , a measure of the asymmetry of the vortex currents at the surface, as a function of  $\tan\theta$ . The vortex current asymmetry varies roughly linearly with  $\tan\theta$ , as does the vortex field asymmetry (Fig. 2). When we fit the vortex current asymmetry to the expression  $(d-c)/\lambda = a_1 \tan\theta + a_2$  for various values of  $\bar{j}^2$ , we find the empirical relation  $a_1 = \alpha/\bar{j}$  with  $\alpha = 0.335 \pm 0.004$ . One can in principle determine the vortex tilt angle from the vortex current asymmetry using this relation.

### III. UNIAXIAL CRYSTAL WITH SURFACE AT $ab$ PLANE

The general case of an anisotropic half-space superconductor with an arbitrary plane surface and arbitrarily oriented vortex has been considered in Ref. [13]. Here, we are interested in the surface coinciding with the  $ab$  plane, Section III.A of [13]. In this case, the coordinates  $x, y, z$  coincide with the crystal's  $a, b, c$  axes, and the mass

tensor is diagonal:  $m_{xx} = m_{yy} = m_a$ ,  $m_{zz} = m_c$ , the “effective masses” are normalized  $m_a^2 m_c = 1$ , and the anisotropy parameter  $\gamma = \sqrt{m_c/m_a} = \lambda_c/\lambda_{ab}$ .

The basic scheme of the solution is the same as in the isotropic case: one has to solve the anisotropic London equations [18] inside and to match them to solutions of the Maxwell equations for the field outside. Without going into formal details (for which readers are referred to Ref. [13]) we note a relevant point: while solving the system of London equations for the surface contribution to the internal field in the form  $h_i^s(\mathbf{k}, z) = H_i(\mathbf{k})e^{qz}$  we obtain a system of linear homogeneous equations for  $H_i(\mathbf{k})$ , the determinant of which must be zero. This gives possible values of the parameter  $q$ . After straightforward algebra one obtains two positive roots:

$$q_1 = \sqrt{\lambda_{ab}^{-2} + k^2}, \quad q_2 = \sqrt{\lambda_{ab}^{-2} + \gamma^2 k^2}. \quad (19)$$

Hence, instead of one mode of the field decay of the isotropic case, we have now two such modes. The prefactors  $\mathbf{H}^{(1)}$  and  $\mathbf{H}^{(2)}$  are given by:

$$H_x^{(1)} = H_y^{(1)} \frac{k_x}{k_y} = H_z^{(1)} \frac{ik_x q_1}{k^2}, \quad (20)$$

$$H_z^{(1)} = \Phi_0 \frac{ik_x \tan\theta - k}{(k + q_1)d_1}, \quad (21)$$

$$d_1 = 1 + \lambda_{ab}^2(k^2 + k_x^2 \tan^2\theta); \quad (22)$$

$$H_x^{(2)} = -H_y^{(2)} \frac{k_y}{k_x} = -\Phi_0 \frac{k_y^2 \tan\theta}{k^2 d_2}, \quad H_z^{(2)} = 0, \quad (23)$$

$$d_2 = 1 + \lambda_c^2 k^2 + \lambda_{ab}^2 k_x^2 \tan^2\theta. \quad (24)$$

The boundary conditions of the field continuity at  $z = 0$  now read:

$$ik_x \varphi = h_x^v + H_x^{(1)} + H_x^{(2)}, \quad (25)$$

$$ik_y \varphi = h_y^v + H_y^{(1)} + H_y^{(2)}, \quad (26)$$

$$-k \varphi = h_z^v + H_z^{(1)}. \quad (27)$$

The 2D Fourier components of the field  $\mathbf{h}^v$  at  $z = 0$  are given in App. A of Ref. [15]:

$$h_x^v = \Phi_0 \tan\theta [1 + \lambda_{ab}^2(k_x^2 \tan^2\theta + k_y^2) + \lambda_c^2 k_x^2]/d, \quad (28)$$

$$h_y^v = \Phi_0 \tan\theta (\lambda_c^2 - \lambda_{ab}^2) k_x k_y / d, \quad (29)$$

$$h_z^v = \Phi_0 / [1 + \lambda_{ab}^2(k_x^2 \sec^2\theta + k_y^2)], \quad d = d_1 d_2. \quad (30)$$

The condition  $\text{div} \mathbf{h}^s = 0$  at  $z = 0$  translates to  $ik_x(H_x^{(1)} + H_x^{(2)}) + ik_y(H_y^{(1)} + H_y^{(2)}) + q_1 H_z^{(1)} = 0$ , so that one easily excludes all  $\mathbf{H}$ 's from the system (25)-(27) to obtain:

$$\varphi = -\frac{\Phi_0 e^{-kz}}{\lambda_{ab}^2 k (k + q_1) (q_1 - ik_x \tan\theta)}. \quad (31)$$

Note that  $\lambda_c$  does not enter this expression. Hence, the outside field depends only on  $\lambda_{ab}$ . It is worth noting that if the vortex as the field source is replaced with some external source, the response field outside also does not depend on  $\lambda_c$  [19].

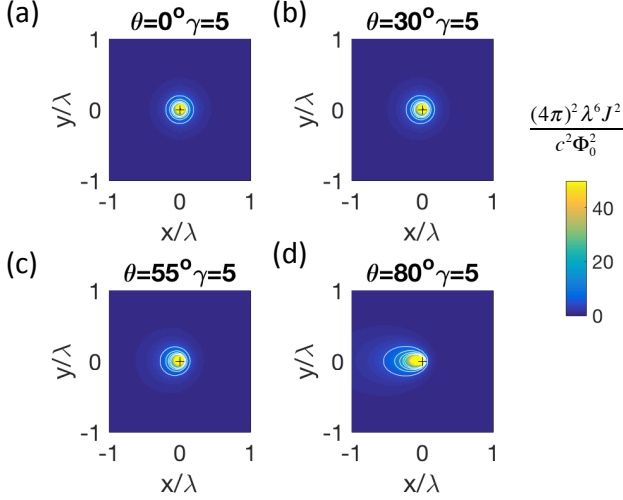


FIG. 5. (Color online) Normalized absolute value squared of the vortex currents  $(4\pi)^2\lambda^6 J^2/c^2\Phi_0^2$  at the superconducting surface in the uniaxial anisotropic case with  $\gamma = 5$ . The tilt angle of the vortex relative to the sample surface  $\theta = 0^\circ$  (a),  $30^\circ$  (b),  $55^\circ$  (c), and  $80^\circ$  (d). The false colormap is saturated at  $(4\pi)^2\lambda^6 J^2/c^2\Phi_0^2 = 50$ . The contours of constant  $J^2$  (white) are at  $(4\pi)^2\lambda^6 J^2/c^2\Phi_0^2 = 5, 10, 15, 20$ , and  $25$ . The ‘+’ symbol marks the center of the vortex coordinate system.

From the potential we get:

$$h_z = -k\varphi(\mathbf{k}) = \frac{\Phi_0 e^{-kz}}{\lambda_{ab}^2(k + q_1)(q_1 - ik_x \tan \theta)}. \quad (32)$$

For  $k \rightarrow 0$ ,  $q_1 = 1/\lambda_{ab}$  so that the total flux  $h_z(k = 0) = \Phi_0$ , as it should.

### A. Surface currents

As before, the current consists of the vortex and surface contributions,  $\mathbf{J}^v$  and  $\mathbf{J}^s$ . The surface contribution is given by

$$\frac{4\pi}{c} J_x^s(\mathbf{k}) = ik_y H_z^{(1)} - q_1 H_y^{(1)} - q_2 H_y^{(2)}, \quad (33)$$

$$\frac{4\pi}{c} J_y^s(\mathbf{k}) = q_1 H_x^{(1)} + q_2 H_x^{(2)} - ik_x H_z^{(1)}. \quad (34)$$

For a tilted vortex, the currents at the surface are given in Appendix A of Ref. [15]:

$$\frac{4\pi}{c} J_x^v = \Phi_0 \frac{ik_y [1 + \lambda_c^2(k^2 + k_x^2 \tan^2 \theta)]}{d_1 d_2}, \quad (35)$$

$$\frac{4\pi}{c} J_y^v = -\Phi_0 \frac{ik_x [1 + \lambda_{ab}^2(\sin^2 \theta + \gamma^2 \cos^2 \theta)(k^2 + k_x^2 \tan^2 \theta)]}{d_1 d_2 \cos^2 \theta}. \quad (36)$$

One can now evaluate numerically  $J^2(x, y) = (J_x^s + J_x^v)^2 + (J_y^s + J_y^v)^2$  at the surface. Results are shown in

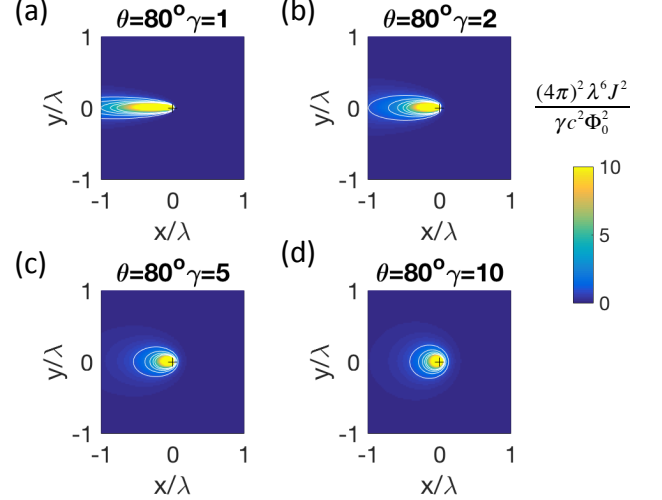


FIG. 6. (Color online) Normalized absolute value squared of the vortex currents  $(4\pi)^2\lambda^6 J^2/\gamma c^2\Phi_0^2$  at the superconducting surface in the uniaxial anisotropic case for a tilt angle of  $80^\circ$ . The anisotropy parameter is  $\gamma = 1$  (a),  $2$  (b),  $5$  (c), and  $10$  (d). The false color scales are saturated at  $(4\pi)^2\lambda^6 J^2/\gamma c^2\Phi_0^2 = 10$ . The contours of constant  $J^2$  (white) are at  $(4\pi)^2\lambda^6 J^2/\gamma c^2\Phi_0^2 = 1, 2, 3, 4, 5$ . The ‘+’ symbol marks the center of the vortex coordinate system.

Figure 5. We again applied a high frequency filter  $e^{-k^2 dz^2}$  with  $dz = 0.01\lambda$  to damp out high frequency oscillations at  $x = 0$  and  $y = 0$ . The false color scale in Fig. 5 is saturated at  $(4\pi)^2\lambda^6 J^2/c^2\Phi_0^2 = 50$ . Note that the current densities are higher and the elongation of the vortex core along the tilt axis at high tilt angles is less pronounced as compared with the isotropic case (Fig. 3).

The systematic behavior of the vortex core with uniaxial anisotropy is illustrated in Figure 6.

## IV. DISCUSSION

Numerical analysis of the expressions given above show that the external magnetic fields from vortices become weaker as the tilt angle increases, at the same time as the vortex shape becomes more elongated in the tilt direction (Fig. 1). In contrast, the peak absolute values of the surface supercurrents are relatively insensitive to tilt angle, while the vortex core elongation increases with tilt angle (Fig. 3). For a uniaxial superconductor the surface currents become stronger with higher anisotropy, but the vortex cores become less elongated (Fig.’s 5, 6). This, at first sight, is surprising but could be understood qualitatively by comparing tilted vortices near the surface in the isotropic and anisotropic cases. Since there the currents must be parallel to the surface, in isotropic materials the surface causes a strong distortion of the currents in its vicinity as compared to the bulk. On the other hand, in an anisotropic uniaxial sample with the  $ab$

surface, the unperturbed bulk current planes are already tilted toward  $ab$  due to anisotropy, so that the distortion caused by the surface is getting weaker with increasing anisotropy. In the limit  $\gamma \gg 1$ , the surface distortion disappears altogether, which we in fact see in our simulations.

Experimental tests of these effects would be a challenge with existing trilayer [20] or Dayem bridge [21] SQUID microscopes, which have spatial resolution of somewhat less than  $1\mu\text{m}$ , while superconducting penetration depths are typically  $0.1\mu\text{m}$ . However, recent SQUID-on-a-tip sensors [22] may have the spatial resolution required. Of course, STM easily has the spatial resolution to look for

the vortex elongations predicted here.

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