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Fast algorithm for transient current through open quantum systems

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Transient current calculation is essential to study the response time and capture the peak transient current for preventing melt down of nano-chips in nanoelectronics. Its calculation is known to be extremely time consuming with the best scaling TN^3 where N is the dimension of the device and T is the number of time steps. The dynamical response of the system is usually probed by sending a step-like pulse and monitoring its transient behavior. Here, we provide a fast algorithm to study the transient behavior due to the step-like pulse. This algorithm consists of two parts: The algorithm I reduces the computational complexity to T^0N^3 for large systems as long as $T < N$; The algorithm II employs the fast multipole technique and achieves scaling T^0N^3 whenever $T < N^2$ beyond which it becomes $T \log_2 N$ for even longer time. Hence it is of order $O(1)$ if $T < N^2$. Benchmark calculation has been done on graphene nanoribbons with $N = 10^4$ and $T = 10^8$. This new algorithm allows us to tackle many large scale transient problems including magnetic tunneling junctions and ferroelectric tunneling junctions that cannot be touched before.

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I. INTRODUCTION

At the heart of growing demands for nanotechnology is the need of ultrafast transistors whose response time is one of the key performance indicators. The response of a general quantum open system can be probed by sending a step-like pulse across the system and monitored by its transient current over times, making transient dynamics a very important problem. Many experimental data show that most of the molecular device characteristics are closely related to material and chemical details of the device structure. Therefore, first principles analysis, that makes quantitative and predictive analysis of device characteristics especially its dynamic properties without relying on any phenomenological parameter, becomes a central problem of nanoelectronics.

The theoretical study of transient current dates back to twenty years ago when the exact solution in the wide-band limit (WBL) was obtained by Wingreen et al.¹. Since then the transient current has been studied extensively using various methods², including the scattering wavefunction^{3,4}, non-equilibrium Green's function (NEGF)⁵⁻⁸ approach, and density matrix method⁹. The major obstacle of theoretical investigation on the first principles transient current is its computational complexity. Many attempts were made trying to speed up the calculation^{3,4,10-14}. Despite of these efforts, the best algorithm to calculate the transient current from first principles going beyond WBL limit scales like TN^3 using complex absorbing potential (CAP)¹⁵ where T and N are number of time steps and size of the system respectively. We note that if WBL is used, the scaling is reduced¹². However, to capture the feature of band structure of lead and the interaction between lead and scattering region the WBL is not a good approximation in the first principles calculation.

As a result, most of the first principles investigations on transient dynamics were limited to small and simple

one-dimensional systems. There are a number of problems such as magnetic tunneling junctions (MTJ)¹⁷, ferroelectric tunneling junctions¹⁸, where the system is two dimensional or even three dimensional in nature. For these systems, large number of k points N_k has to be sampled in the first Brillouin to capture accurately the band structure of the system. For MTJ structure like Fe-MgO-Fe, at least $N_k = 10^4$ k points must be used to give a converged transmission coefficient¹⁹. This makes the time consuming transient calculation N_k times longer which is an almost impossible task even with high performance supercomputer. Clearly it is urgent to develop better algorithms to reduce the computational complexity.

In this paper, we develop a fast algorithm based on NEGF-CAP formalism to calculate transient current for step-like pulse as a function of time step T which could be helpful in speeding up the first principles transient calculation. The computational time of this algorithm is independent of T as long as $T < N^2$ where N is the system size²⁰. Hence our algorithm is order $O(1)$ as long as $T < N^2$. Four important ingredients are essential to achieve this : (1). the availability of exact solution of transient current based on NEGF that goes beyond WBL. (2). the use of CAP so that the transient current can be expressed in terms of poles of Green's function. (3). within NEGF-CAP formalism the transient current can be calculated separately in space and time domain making $O(1)$ algorithm possible. At this point the computational complexity reduces to $N^3 + TN^2$ (algorithm I). (4). the exploitation of Vandermonde matrix enables us to use fast multipole method (FMM)^{21,22} and fast Fourier transform (FFT) to further reduce the scaling to $N^3 + N^2 \log_2 N$ for $T < N^2$ and large N , therefore completely independent of T (algorithm II). To verify the computational complexity, we carry out benchmark calculations on graphene nanoribbons using the tight-binding model. A calculation is also done for a sys-

tem with $N = 10200$ and $T = 10^8$ confirming the $O(1)$ scaling. This fast algorithm makes the computational complexity of transient current calculation comparable to that of static calculation.

II. THEORETICAL FORMALISM

For a general open quantum system with multiple leads under a step-like bias pulse, the Hamiltonian is given by

$$H(t) = \sum_{k\alpha} \epsilon_{k\alpha} \hat{c}_{k\alpha}^\dagger \hat{c}_{k\alpha} + \sum_n (\epsilon_n + U_n(t)) \hat{d}_n^\dagger \hat{d}_n + \sum_{k\alpha n} h_{k\alpha n} \hat{c}_{k\alpha}^\dagger \hat{d}_n + c.c. ,$$

where c^\dagger (c) denotes the electron creation (annihilation) operator in the lead region. The first term in this equation corresponds to the Hamiltonian of leads with $\epsilon_{k\alpha}$ the energy of lead α which contains external bias voltage $v_\alpha(t) = V_\alpha \theta(\pm t)$. The second and third terms represent the Hamiltonian in the central scattering region and its coupling to leads, respectively. Here we have included the time-dependent internal response $U_n(t)$ in the scattering region due to the external bias²³. Taking $q = \hbar = 1$, the time-dependent terminal current $I_\alpha(t)$ of lead α is defined as^{15,16}

$$I_\alpha(t) = \text{ReTr}[\bar{\Gamma}_\alpha(2H(t) - i\partial_t)G^<(t, t)\bar{\Gamma}_\alpha] , \quad (1)$$

where $\bar{\Gamma}_\alpha$ is an auxiliary projection matrix which is used for measuring the transient current passing through the lead α . Here $G^<$ and $H(t)$ are the lesser Green's function and the Hamiltonian of the central scattering region, respectively. For step-like pulse an exact solution for $G^<$ has been obtained by Maciejko et al⁶ which goes beyond the WBL. Now we consider the case of upward pulse $v_\alpha(t) = V_\alpha \theta(t)$. In order to have the exact solution in Ref.6, we assume that $U_n(t) = U_{n,eq} + (U_{n,neq} - U_{n,eq})\theta(t)$ where $U_{n,eq}$ is the equilibrium potential while $U_{n,neq}$ is the non-equilibrium potential at long time limit. As a result of this instantaneous approximation, at $t = 0$, the system is in equilibrium with Hamiltonian H_{eq} while at $t > 0$ the system is in non-equilibrium state with a time-independent Hamiltonian H_{neq} .

Note that our fast algorithm relies critically on this approximation where two static potentials are needed at: $t = 0^-$ and $t = 0^+$. For instance, our method fails if $U_n(t) = U_{n,eq} + U_{n,neq} \cos(\omega t)$. With this instantaneous assumption, our method could be extended to the first principles calculation where only two static self-consistent Coulomb potentials can be obtained by usual NEGF-DFT calculation²⁴. In terms of spectral function $A_\alpha(\epsilon, t)$, the lesser Green's function $G^<$ is given by⁶

$$G^<(t, t) = i \sum_\alpha \int \frac{d\epsilon}{2\pi} f(\epsilon) A_\alpha(\epsilon, t) \Gamma_\alpha(\epsilon) A_\alpha^\dagger(\epsilon, t) . \quad (2)$$

For the upward step-like bias pulse the $A_\alpha(\epsilon, t)$ is⁶

$$A_\alpha(\epsilon, t) = \bar{G}^r(\epsilon + \Delta_\alpha) - \int \frac{d\omega}{2\pi i} \frac{e^{-i(\omega-\epsilon)t} \bar{G}^r(\omega + \Delta_\alpha)}{(\omega - \epsilon + \Delta_\alpha - i0^+)} \times \left[\frac{\Delta_\alpha}{(\omega - \epsilon - i0^+)} + \Delta \tilde{G}^r(\epsilon) \right] \equiv A_{1\alpha}(\epsilon + \Delta_\alpha) + \int d\omega e^{-i(\omega-\epsilon)t} A_{2\alpha}(\omega, \epsilon) , \quad (3)$$

where \bar{G}^r and \tilde{G}^r are the non-equilibrium and equilibrium retarded Green's function respectively, Δ_α is the amplitude of external bias $-V_\alpha$, and $\Delta = U_{neq} - U_{eq}$ is a matrix where the subscript 'neq' and 'eq' refer to non-equilibrium and equilibrium potentials, respectively.

Despite the simplification from the conventional double time $G^<(t, t')$ to single time $G^<(t, t)$ used in Eq.(1), the computational cost to obtain $G^<$ remains very demanding due to the following reasons. (1) Consider $A_\alpha(\epsilon, t)$ with a matrix size of N , matrix multiplications $\bar{G}^r(\omega + \Delta_\alpha)$ and $\tilde{G}^r(\epsilon)$ in the integrand of Eq.(3) requires computational complexity of $O(N^3)$ for each time step. As a result, the total computational cost over a period of time is at least $O(TN^3)$ where T is the number of time steps. (2) Double integrations in energy space are required for $G^<$. The presence of numerous quasi-resonant states whose energies are close to real energy axis makes the energy integration in A_α extremely difficult to converge. This problem can be overcome using the CAP method²⁵. The essence of CAP method is to replace each semi-infinite lead by a finite region of CAP while keeping transmission coefficient of the system unchanged. In addition, it has been demonstrated in Ref.15 that the first principles result of transient current for molecular junctions obtained from the exact numerical method (non-WBL) and the CAP method are exactly the same. Using the CAP method, the poles of the Green's function can be obtained easily and the spectral function can be calculated analytically using the residue theorem. Expanding Fermi function using Pade spectrum decomposition (PSD)²⁶ further allows us to calculate the transient current separately in space and time domain making the $O(T^0 N^3)$ algorithm possible.

Now we illustrate how to achieve our algorithm for the transient current calculation, i.e., $I_\alpha(t_j)$ for $j = 1, 2, \dots, T$. Substituting Eq.(3) to Eq.(2), $G^<(t, t)$ can be written as

$$G^<(t, t) = (i/\pi) [B_1 + \int d\omega d\omega' e^{-i(\omega-\omega')t} B_2(\omega, \omega') + \sum_\alpha \int d\epsilon d\omega' e^{i(\omega'-\epsilon)t} f(\epsilon) A_{1\alpha} W_\alpha A_{2\alpha}^\dagger + c.c.] \quad (4)$$

where $B_1 = \int d\epsilon f(\epsilon) \sum_\alpha A_{1\alpha} W_\alpha A_{1\alpha}^\dagger$, $B_2(\omega, \omega') = \int d\epsilon f(\epsilon) \sum_\alpha A_{2\alpha}(\omega, \epsilon) W_\alpha A_{2\alpha}^\dagger(\omega', \epsilon)$, and W_α is the CAP matrix. In terms of poles of Green's function and Fermi

distribution function, we have (see Appendix A)

$$G^<(t, t) = (i/\pi) \left[B_1 + \sum_{nm} e^{-i(\epsilon_n - \epsilon_m^*)t} \bar{B}_2(\epsilon_n, \epsilon_m^*) + \sum_{\alpha} \sum_{lm} e^{-i(\tilde{\epsilon}_l - \epsilon_m^* + \Delta_{\alpha})t} \bar{f}(\tilde{\epsilon}_l) \bar{B}_{3\alpha}(\tilde{\epsilon}_l, \epsilon_m^*) + c.c. + \sum_{\alpha} \sum_{nm} e^{-i(\epsilon_n - \epsilon_m^*)t} f(\epsilon_n - \Delta_{\alpha}) \bar{B}_{4\alpha}(\epsilon_n, \epsilon_m^*) + c.c. \right] \quad (5)$$

where ϵ_n and ϵ_m ($n = 1, 2, \dots, N$) is the complex energy spectrum of $H_{neq} - i \sum_{\alpha} W_{\alpha}$ in the lower half plane while $\tilde{\epsilon}_l$ being the poles of $f(E)$ using PSD with $l = 1, \dots, N_f$; N_f is the total number of those poles for the adopted Pade approximant; other parameters in Eq.(5) are given as

$$\bar{B}_2 = -4\pi^2 [B_2(\omega, \omega')(\omega - \epsilon_n)(\omega' - \epsilon_m^*)] \Big|_{\omega=\epsilon_n, \omega'=\epsilon_m^*}, \quad (6)$$

$$\bar{B}_{3\alpha} = -2\pi i A_{1\alpha}(\tilde{\epsilon}_l) W_{\alpha} [A_{2\alpha}^{\dagger}(\omega', \tilde{\epsilon}_l)(\omega' - \epsilon_m^*)] \Big|_{\omega'=\epsilon_m^*}, \quad (7)$$

$$\bar{B}_{4\alpha} = -4\pi^2 \left[A_{1\alpha}(\epsilon) W_{\alpha} A_{2\alpha}^{\dagger}(\omega', \epsilon)(\omega' - \epsilon_m^*) \times (\epsilon - \epsilon_n + \Delta_{\alpha}) \right] \Big|_{\epsilon=\epsilon_n - \Delta_{\alpha}, \omega'=\epsilon_m^*}, \quad (8)$$

and

$$\bar{f} = 2\pi i (f(\epsilon)(\epsilon - \tilde{\epsilon}_l)) \Big|_{\epsilon=\tilde{\epsilon}_l}, \quad (9)$$

is the residue of f in the PDS representation.

Within CAP framework, $G^<$ in Eq.(1) is the lesser Green's function of the central scattering region excluding the CAP regions. Substituting the second term of Eq.(5) into the first term in Eq.(1), we find its contribution to current (denoted as I_1)

$$I_1(t) = \text{Re} \sum_{nm} e^{-i(\epsilon_n - \epsilon_m^*)t} \text{Tr} [\bar{\Gamma}_{\alpha} 2H_{neq} \bar{B}_2(\epsilon_n, \epsilon_m^*) \bar{\Gamma}_{\alpha}] \equiv 2\text{Re} \sum_{nm} e^{-i(\epsilon_n - \epsilon_m^*)t} M_{nm}, \quad (10)$$

where the matrix M does not depend on time. We see that the space and time domains have been separated.

Denoting a Vandermonde matrix $V_{jk} = \exp(i\epsilon_k t_j)$ with $k = 1, 2, \dots, N$, $t_j = jdt$, $j = 1, 2, \dots, T$ where dt is the time interval, we have $I_1(t_j) = [V^t (M + M^{\dagger}) V^*]_{jj}$. Using this approach, we finally obtain (see supplementary material for details)

$$I_L(t_j) = I_{0L} + [V^t M_1 V^*]_{jj} + \left(\sum_{\alpha=L,R} [V^t M_{2\alpha} \tilde{V}_{\alpha}^*]_{jj} + c.c. \right) \quad (1)$$

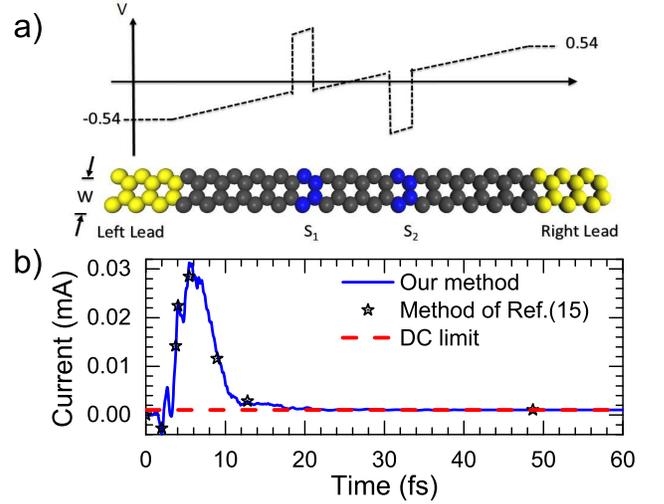


FIG. 1. a) Configuration of the gated graphene nanoribbon. The S_1 and S_2 gate are of values 0.81V and -0.81V respectively. b) Transient current of zigzag graphene nanoribbon for a system of 600 atoms. The dashed line is the dc limit.

where $\tilde{V}_{\alpha jk} = \exp(i(\tilde{\epsilon}_k + \Delta_{\alpha})t_j)$ is a $T \times N_f$ matrix, M_1 is a $N \times N$ matrix while M_2 is a $N \times N_f$ matrix. Since ϵ_k is the complex energy in the lower half plane, V_{jk} goes to zero at large j . Hence I_{0L} is the long time limit of transient current which can be calculated using Landauer Buttiker formula. The time dependent part of the transient current can be separated into real space calculation (calculation of M_1 and $M_{2\alpha}$) and then a matrix multiplication involving time. We note that at room temperatures the Fermi function can be accurately approximated by 15 or 20 Pade approximants. Hence the calculation of $[V^t M_1 V^*]_{jj} + (\sum_{\alpha} [V^t M_{2\alpha} \tilde{V}_{\alpha}^*]_{jj} + c.c.)$ can be combined to give TN^2 computational complexity.

Now we examine the computational complexity of this algorithm (denoted as algorithm I). Clearly the total computational complexity is $N^3 + TN^2$. At this stage, the algorithm is not $O(1)$ yet. In the supplementary material, we will show that matrix multiplication $V^t M$, where M is M_1 or $M_{2\alpha}$, can be done using the FMM and FFT (denoted as algorithm II). This will reduce the computational complexity of $V^t M$ from TN^2 to $T \log_2 N$. Hence for $T < N^2$, the computational complexity is $N^3 + N^2 \log_2 N$. For $T > N^2$, the scaling is $N^3 + T \log_2 N$. However, for large T , the physics comes into play. Since ϵ_j is the complex energy of the resonant state, $V_{jT} = \exp(-i\epsilon_j dtT)$ decays quickly to zero before $T = N^2$. For a graphene nanoribbon with $N = 10^4$ (see details below), the maximum value of $V_{jT} = \exp(-i\epsilon_j dtT)$ is 10^{-3} when $T = N$ and $dt = 1$ fs. Consequently all the matrix elements are zero for $T = 10N$. Hence for large systems, the chance to go beyond $T = N^2$ is small. In this sense, the algorithm II is order $O(1)$ algorithm.

III. FAST MULTIPOLE METHOD

The fast multipole method²¹ has been widely used and has been ranked top 10 best algorithms in 20th Century³³. It is extremely efficient for large N . In the following, we will illustrate how to speed up the calculation of transient current defined in Eq.(12) below. We want to calculate the following quantity

$$I(t_j) = \sum_{n,m} \exp(-i\epsilon_n t_j) M_{nm} \exp(i\epsilon_m^* t_j), \quad (12)$$

where the matrix M can be expressed in terms of vectors as $M = (c_0, c_1, \dots, c_{N-1})$ and $V_{nj} = \exp(-i\epsilon_n t_j)$ is a Vandermonde matrix with $t_j = jdt$ and $j = 1, 2, \dots, T$. Eq.(12) is of the form $V^t M V^*$ where t stands for transpose. In the following, we outline how to calculate $V^t c$ using $\kappa_1 N + \kappa_2 N \log_2 N$ operations where c is a vector of N components and κ_1 and κ_2 are constants.

Setting $a_j = \exp(-i\epsilon_j dt)$ and denoting T the number of time steps. Then $b = V^t c$ is equivalent to $b_n = \sum_{j=0}^{N-1} c_j (a_j)^n$. A direct computation shows that the entries of $b = V^t c$ are the first T coefficients of the Taylor expansion of

$$S(x) = \sum_{j=0}^{N-1} \frac{c_j}{1 - a_j x} = \sum_n \sum_{j=0}^{N-1} c_j (a_j x)^n = \sum_n b_n x^n, \quad (13)$$

where $b_n = \sum_{j=0}^{N-1} c_j (a_j)^n$. Denoting $\bar{S}(x) = \sum_{n=0}^{T-1} b_n x^n$ and setting $x = \omega_T^l$ with $\omega_T = \exp(i2\pi/T)$ we can calculate $\bar{S}(\omega_T^l)$ which is the Fourier transform of b_n ,

$$\begin{aligned} \bar{S}(\omega_T^l) &= \sum_{j=0}^{N-1} \sum_{n=0}^{T-1} c_j a_j^n \omega_T^{nl} = \sum_{j=0}^{N-1} c_j \frac{1 - (a_j \omega_T^l)^T}{1 - a_j \omega_T^l} \\ &= \omega_T^{-l} \sum_{j=0}^{N-1} \frac{c_j (1 - a_j^T)}{(1/\omega_T)^l - a_j}, \end{aligned}$$

where we have used $[\omega_T]^T = 1$. Note that the fast multipole method (FMM) aims to calculate $v_l = \sum_j c_j / (x_l - a_j)$ with $O(N)$ operations instead of N^2 operations. Hence $\bar{S}(\omega_T^l)$ can be obtained using FMM, from which we calculate b_n using FFT.

Now we estimate the computational complexity for $T \leq N$. For FMM we need $\kappa_1 \max(T, N)$ operations where κ_1 is about $40 \log_2(1/\tau)$ with τ the tolerance³¹. For FFT the computational complexity is at most $\kappa_2 N \log_2 N$ where κ_2 is a coefficient for FFT calculation³¹. To compute $V^t c$ where M has N vectors, we have to calculate $V^t c$ N times. Hence the total computational complexity is $\kappa_1 N^2 + \kappa_2 N^2 \log_2 N$. This algorithm is denoted as algorithm IIa while the algorithm for $T < N^2$ discussed below is denoted as algorithm IIb.

For very large T up to $T = N^2$ (if $N = 10^4$ we have $T = 10^8$), we will show that the computational complexity is $\kappa_1 N^2 + 2\kappa_2 N^2 \log_2 N$. In fact, it is easy to see that $I(t_j)$

defined in Eq.(12) is the first T coefficients of the Taylor expansion of

$$\begin{aligned} S(x) &= \sum_{n,m=0}^{N-1} \frac{M_{nm}}{1 - a_n a_m^* x} \\ &= \sum_j \sum_{n,m=0}^{N-1} M_{nm} (a_n a_m^*)^j x^j = \sum_j I(t_j) x^j, \end{aligned} \quad (14)$$

where $a_n = \exp(-i\epsilon_n dt)$. Now we define two new vectors u and d which have N^2 components with $u^t = (c_0^t, c_1^t, \dots, c_{N-1}^t)$ (recall our definition $M = (c_0, c_1, \dots, c_{N-1})$) and $d^t = (a_0^* a^t, a_1^* a^t, \dots, a_{N-1}^* a^t)$, where once again t stands for transpose. With the new vectors defined, $S(x)$ in Eq.(14) is expressed as

$$S(x) = \sum_{j=0}^{N^2-1} \frac{u_j}{1 - d_j x}, \quad (16)$$

which is exactly the same form as Eq.(13). The only difference is that c and a in Eq.(13) have N components and S has to be calculated N times while u and d in Eq.(16) have N^2 components and we calculate S defined according to Eq.(16) just once. Therefore the computational complexity is $\kappa_1 N^2 + \kappa_2 N^2 \log_2 N^2$. If $T = nN$ with $n = 1, 2, \dots, N$, it is not difficult to show that the computational complexity is $\kappa_1 T N / n + \kappa_2 T (N/n) \log_2(nN) = \kappa_1 N^2 + \kappa_2 N^2 \log_2(nN)$.

To summarize, the computational complexity of Eq.(12) is $\kappa_1 N^2 + 2\kappa_2 N^2 \log_2 N$ for $T < N^2$. It is easy to show that for $T > N^2$ the scaling is dominated by $\kappa_2 T \log_2 N$. However, for large T , the physics comes into play. Since $a_j = \exp(-i\epsilon_j dt)$ with ϵ_j the energy of resonant state, a_j^T quickly decays to zero before $T = N^2$ and hence no need to go up for $T > N^2$.

IV. NUMERICAL TEST

To demonstrate the power of this algorithm, we calculate the transient current in a graphene nanoribbon. Graphene is a well-known intrinsic 2D material with many exotic properties^{27,28}. Its transient behaviour in response to a step-like pulse was studied in the literature^{7,29,30}. R. Tuovinen et al.⁷ explored the metal-graphene-metal system at zero temperature under the effect of ribbon length, width and bias and found the presence of several-hundreds-femtoseconds oscillation period in transient current, caused by the lead-ribbon reflections; Again at zero temperature, E. Perfetto et al.²⁹ studied the phenomenon of two temporal plateaus that appeared in the transient current of wide graphene nanoribbon (width $W \geq 20$ nm) and deduced the two have arisen from diverse origins; For zigzag ribbon, Xie et al.³⁰, investigated the difference in the current response for symmetric and asymmetric systems. While in all these studies, the transient current through a central region of pure graphene nanoribbons under a step bias have

been studied for both armchair and zigzag structures under different circumstances, none of them has considered the cases when barrier-like gated regions exist in central region. Here, we will test our algorithm on a gated zigzag graphene nanoribbon at room temperature using the tight-binding (TB) Hamiltonian given by

$$\hat{H} = -h_0 \sum_{\langle i,j \rangle} \hat{c}_i^\dagger \hat{c}_j - q \sum_i [V_i \theta(t) + V_{g1i} + V_{g2i}] \hat{c}_i^\dagger \hat{c}_i, \quad (17)$$

where \hat{c}_i^\dagger (\hat{c}_i) is the creation (annihilation) operator at site i and $h_0 = 2.7\text{eV}$ being the nearest hopping constant. Here $V(x) = V_L + (V_R - V_L)x/L$ is the potential landscape due to the external bias with $V_R = -V_L = 0.54\text{V}$ and V_{g1} and V_{g2} are gate voltages in regions S_1 and S_2 , respectively.

We first confirm that the transient current calculated using the new method is the same as that of Ref.15. Using 30 layers of CAP, transmission coefficient versus energy was calculated which shows good agreement with the exact solution (Fig.2 gives the comparison for a graphene nanoribbon with $N = 10000$). This also ensures the correct steady state current. For the transient current, excellent agreement is also obtained between our algorithm and that of Ref.15 (see Fig.1). We note that even in the presence of gates, an overshooting at the beginning is still observed, similar to the un-gated graphene³⁰ but the oscillating tail is not observable after the overshooting peak. We also tested with the cases for gated graphene ribbon with a larger width W (not shown) and obtained higher transient current over time which was observed previously⁷ for the un-gated condition.

We have performed calculation on transient current through a zigzag graphene nanoribbon of 10000 atoms with $T = 20000$ time steps (each time step is 1fs). The width of the system is two unit cells (16 atoms) while the length of the system is 625 unit cells. Two gate voltages of 2.2V were applied so that the system is in the tunneling regime. The bias voltage is $v_L = -v_R = 0.5\text{V}$. From Fig. 3, we see a typical behavior of transient current with the current shoots up initially and then decreases to the long time limit. Our numerical results using FMM (algorithm II) show that 100ps is needed to reach the dc limit. The oscillatory behavior is due to resonant states in the system.

Now we test the scaling of our algorithm by calculating the transient current for nanoribbons with different system sizes ranging from 600 to 10200 atoms. We first test the algorithm I. Computational time of transient current for 3 time steps against system sizes N is shown in Fig. 4a. We have fitted the data using $50N^3 + TN^2$ with very good agreement showing TN^2 scaling for the time-dependent part. For comparison, we have also plotted the computation time using method in Ref.15. We found that the number of energy points N_E depends on the spectrum of resonant states of the system. For graphene nanoribbons with 600 atoms, we have used $N_E = 6000$ to

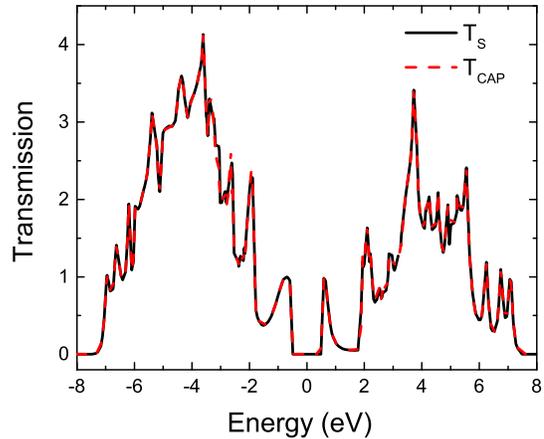


FIG. 2. The transmission coefficient of the zigzag graphene nanoribbon for a system of 10000 atoms. The solid line (T_S) is the exact numerical result using self-energy of the lead and the dashed line (T_{CAP}) is from CAP.

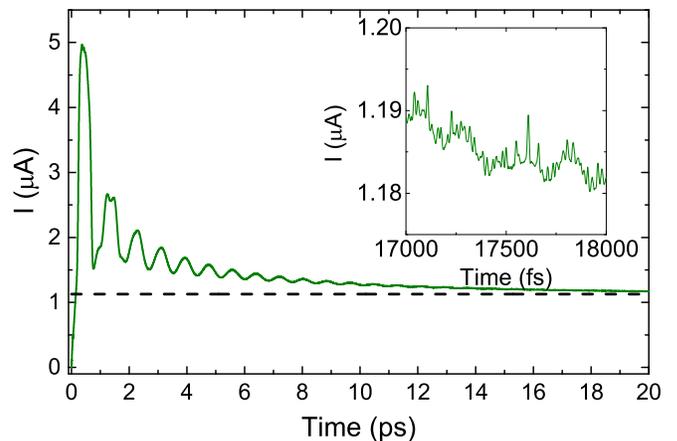


FIG. 3. Transient current of zigzag graphene nanoribbon for a system of 10000 atoms at temperature of 300K. The inset is the long time behavior between 17ps to 18ps. The dashed line is the dc limit of transient current.

converge the integral over Fermi function. Fig. 4a shows that a speed up factor of 1000T is achieved at $N = 2400$. The scaling is shown in Fig. 4b, from which we see that for $T < N$ the computational time is almost independent of the number of time steps.

Now we examine the algorithm II which reduces the scaling TN^2 further. Notice that the scaling TN^2 comes from matrix multiplication involving Vandermonde matrix $V^t M_1$. Fast algorithm is available to speed up the calculation involving structured matrix such as Vandermonde matrix. As discussed in details in section III, we can use FMM^{21,22} and FFT to carry out the same ma-

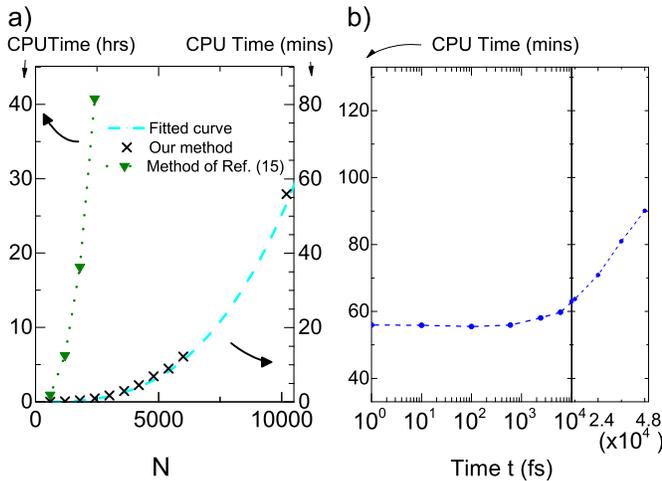


FIG. 4. (a) Scaling of computation time against N at $T=3$ (each time step is 1fs). The fitted curve in the form of $50N^3 + TN^2$ is in good agreement with the calculated results (Y-axis is on the right). In order compare the performance of Ref.(15), 6000 energy points was used for integration(Y-axis is on the left). (b) Scaling of CPU time against t for $N=10200$ ($t=100$ fs corresponds to $T=100$) using algorithm I. Left hand side: exponential scale in t ; Right hand side: linear scale in t , shows that at extreme large data points ranges over 10 thousands points, computational time is proportional to T .

trix multiplication using only $\kappa_1 N^2 + \kappa_2 N^2 \log_2 N$ operations provided $T < N^2$. Here the coefficient κ_1 is a large constant that depends only on the tolerance of the calculation τ and the setup of FMM. The theoretical estimate of this coefficient is about $40 \log_2(1/\tau)$ where τ is the tolerance³¹ in FMM calculation which we used $\tau = 10^{-4}$. When implementing FMM, this coefficient is in general larger than the theoretical one.

To test the algorithm II, we have calculated the transient current numerically for $N = 10^4$ and $T = 10^8$ using FMM and FFT. The configuration of the system is the same as that appeared in main text (Fig.1) except the width W of the system is now 17 times wider with a total of $10200 \sim 10^4$ atoms. The time step is 0.012 fs. The computed transient current using Algorithm I and II are shown in Fig.5. The purpose of this calculation is to test the computational complexity only. All we need to do is to compute,

$$\bar{S}(\omega_T^l) = \omega_T^{-l} \sum_{j=0}^{N^2-1} \frac{u_j(1-d_j^T)}{(1/\omega_T)^l - d_j}, \quad (18)$$

using FMM and then take FFT to obtain $I(t_j)$ where u_j and d_j have been defined just before Eq.(16). Note that u_j has been obtained in the time independent calculation.

If $(1/\omega_T)^j$ and d_j in Eq.(18) are uniformly distributed on the complex plane, the FMM can be done much faster. However, as shown in Fig.6 and Fig.7, the unit distribution of $(1/\omega_T)^j$ and d_j are highly non-uniform in our

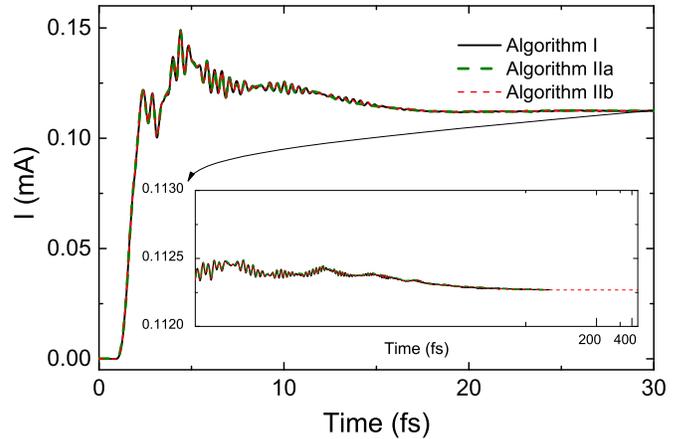


FIG. 5. Transient current calculated by algorithm I, Algorithm IIa and Algorithm IIb;IIa and IIb refer to the cases with FMM methods targeting $T = N$ and $T = N^2$ respectively.

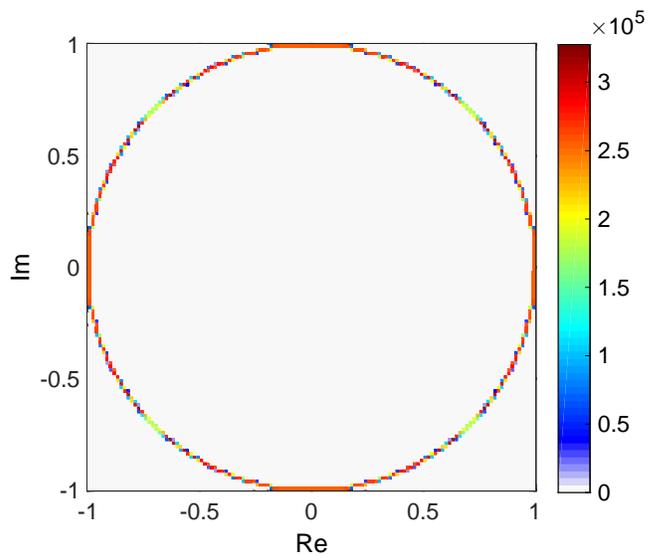


FIG. 6. Distribution of $(1/\omega_T)^j$ on the complex plane.

case. Actually, $(1/\omega_T)^j$ are distributed non-uniformly along the circle (Fig.6) while d_j are distributed in a sector of unit circle (Fig.7). This makes the calculation more difficult. For $N = 10^4$ and $T = N^8$, we found that the optimum number of levels in FMM is 10. With 10 levels in FMM, over 60% of CPU time was spent on direct sum in FMM calculation.

In Fig.5, we have tested the algorithm IIa which is suitable for $T = N$ and the algorithm IIb designed for $T = N^2$ against the algorithm I. For $T < N$, the results of the algorithm I, the algorithm IIa and IIb are on top of each other. For $T > N$, the calculation was done for $T = N^2$. In Fig.5, we only show the results for $T < 40000$.

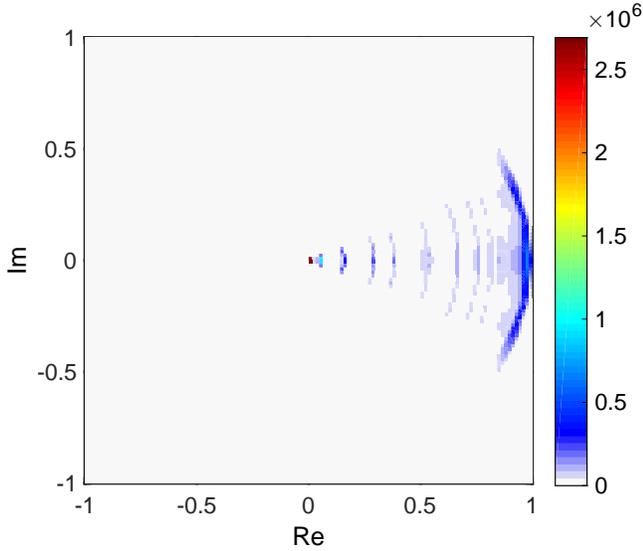


FIG. 7. Distribution of d_j on the complex plane.

There is no significant feature in the transient current plot beyond that.

Denote t_1 the CPU time needed for the spacial calculation (order N^3), t_2 needed for the temporal part (matrix multiplication in Eq.(7)). Using a workstation of Xeon X5650 with 12 cores and frequency 2.67GHz, we obtained $t_1 = 3500s$ using 12 cores and $t_1 = 33800s$ using a single core so the efficiency of multithreading is about 80%. For FMM calculation, multithreading could be very inefficient and we have used a single core to perform the calculation. We found $t_2 = 3400s$ for $T = 10^8$ using a single core. We see that for $T = 10^8$ the time spent in time dependent part is about one tenth of the time independent calculation. This confirms that our method is of order $O(1)$ as long as $T < N^2$. We wish to point out that the algorithm II is aimed to calculate the transient current $I(t)$ with time steps $T = N^2$ at one shot with scaling $N^2 \log_2 N$. This scaling remains if we want $I(t)$ with the number of time step less than N^2 .

V. DISCUSSION AND CONCLUSION

Since our algorithm is based on the NEGF-CAP formalism, it could be extended to the NEGF-DFT-CAP formalism which performs the first principles calculation. With the fast algorithm at hand, many applications can be envisaged. For instance, the transient spin current (related to spin transfer torque) using the NEGF-DFT-CAP formalism could be carried out for planar structures where k-sampling in the first Brillouin zone is needed. It is straightforward to include k-sampling in our method. It is also possible to extend this method to the case when electron-phonon interaction in the Born approximation as well as other dephasing mechanism are present³². Fi-

nally, first principles transient photo-induced current on two dimensional layered materials could be calculated using our method.

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APPENDIX A: PADE APPROXIMANT

Brute force integration over Fermi function along real energy axis to obtain $G^<(t, t)$ may need thousands of energy points to converge which is very inefficient. To obtain an accurate result while reducing the cost, fast converging Pade spectrum decomposition (PSD) is used for the Fermi function f in Eq.(4) in the main text so that the residue theorem can be applied.

Using [n-1/n] PSD scheme²⁶ with the Pade approximant accurate up to $O((\epsilon/kT)^{4n-1})$, Fermi function f can be expressed as

$$f(\epsilon) = \frac{1}{2} - \sum_{j=1}^n \frac{2\eta_j \beta \epsilon}{(\beta \epsilon)^2 + \xi_j^2}, \quad (19)$$

where ξ_j and η_j are two set of constants that can be calculated easily. Using the PSD scheme analytic form of $G^<$ in Eq.(4) of the main text can be obtained using the residue theorem.

APPENDIX B: CALCULATION OF THE SPECTRAL FUNCTION

We express $\tilde{G}^r(\epsilon)$ and $\overline{G}^r(\epsilon)$, the equilibrium and non-equilibrium retarded Green's functions, respectively in terms of their eigen-functions by solving the following eigen-equations for H_{eq} and H_{neq} ,¹⁵ i.e.,

$$\begin{aligned} (H_{eq} - iW)\psi_n^0 &= \epsilon_n^0 \psi_n^0, \\ (H_{eq} + iW^\dagger)\phi_n^0 &= \epsilon_n^0 \phi_n^0, \end{aligned} \quad (20)$$

where $W = \sum_\alpha W_\alpha$ and similar equations can be defined for H_{neq} . Using the eigen-functions of $H_{eq} - iW$ and $H_{neq} - iW$, we have

$$\tilde{G}^r(\epsilon) = [\epsilon - H_{eq} + iW]^{-1} = \sum_n \frac{|\psi_n^0\rangle\langle\phi_n^0|}{(\epsilon - \epsilon_n^0 + i0^+)}, \quad (21)$$

$$\overline{G}^r(\epsilon) = [\epsilon - H_{neq} + iW]^{-1} = \sum_n \frac{|\psi_n\rangle\langle\phi_n|}{(\epsilon - \epsilon_n + i0^+)}. \quad (22)$$

Performing integral over ω using the residue theorem, the analytic solution of A_α is obtained

$$A_\alpha(\epsilon, t) = \sum_n \frac{|\psi_n\rangle\langle\phi_n|}{\epsilon + \Delta_\alpha - \epsilon_n + i0^+} + \sum_n \frac{e^{i(\epsilon + \Delta_\alpha - \epsilon_n)t} |\psi_n\rangle\langle\phi_n|}{\epsilon - \epsilon_n + i0^+} \\ \times \left[\frac{\Delta_\alpha}{\epsilon + \Delta_\alpha - \epsilon_n + i0^+} - \Delta \sum_l \frac{|\psi_l^0\rangle\langle\phi_l^0|}{\epsilon - \epsilon_l^0 + i0^+} \right], \quad (23)$$

where $\Delta = H_{neq} - H_{eq}$.

APPENDIX C: CALCULATION OF THE TRANSIENT CURRENT

Starting from Eq.(1) and in analogue to Eq.(6) of the main text, the expressions of the current in Eq.(7) of the main text can be obtained as follows:

$$I_{0L}(t_j) = 2\text{ReTr} \left[\frac{i}{\pi} \bar{\Gamma}_L H_{neq} B_1 \bar{\Gamma}_L \right],$$

$$M_1 = \text{ReTr} \left[\frac{i}{\pi} \bar{\Gamma}_L (2H_{neq} - (\epsilon_n - \epsilon_m^*)) \left(\bar{B}_2 + \sum_\alpha f(\epsilon_n - \Delta_\alpha) \bar{B}_{4\alpha} \right) \bar{\Gamma}_L \right]$$

$$M_{2\alpha} = \text{ReTr} \left[\frac{i}{\pi} \bar{\Gamma}_L (2H_{neq} - (\tilde{\epsilon}_l - \epsilon_m^* + \Delta_\alpha)) (f(\epsilon_m^*) \bar{B}_{3\alpha}) \bar{\Gamma}_L \right].$$

The expression of transient current $I_R(t)$ is similar to Eq.(7).

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