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Phys. Rev. B **83**, 174205 — Published 19 May 2011

DOI: [10.1103/PhysRevB.83.174205](https://doi.org/10.1103/PhysRevB.83.174205)

**Testing the minimum thermal conductivity model
for amorphous polymers using high pressure**

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Pressure dependence of thermal conductivity provides a critical test of the validity of the
model of the minimum thermal conductivity for describing heat transport by molecular

vibrations of an amorphous polymer. We measure the pressure dependence of the thermal conductivity $\Lambda(P)$ of poly(methyl methacrylate) (PMMA) using a combination of time-domain thermorefectance and SiC anvil cell techniques. We also determine $\Lambda(P)$ from a computational model of amorphous polystyrene. In both cases, $\Lambda(P)$ is accurately predicted by the minimum thermal conductivity model via the pressure dependence of the elastic constants and density.

I. INTRODUCTION

The model of the minimum thermal conductivity was originally proposed by Einstein [1, 2] who supposed that thermal energy is transported by harmonic interactions between vibrating atoms with random phases. Allen and Feldman [3, 4] provided a more rigorous foundation for this model using a harmonic Green-Kubo formalism and introduced the terminology of “locons, diffusons, and propagons” to classify the vibrational modes of disordered materials and their contributions to thermal transport. Locons are localized vibrational modes that do not contribute to thermal transport in the harmonic

approximation. Propagons are wave-like acoustic vibrations that are analogous to the phonons of crystalline solids. The largest fraction of vibrational modes, and the dominant contributors to heat transport, are diffusons, non-propagating, diffusive vibrational modes of the type envisioned by Einstein. Building on these ideas and the assumption of a Debye-like density of vibrational states, the thermal conductivity of most amorphous materials—and many strongly disordered crystals—can be accurately predicted from the atomic density and elastic constants. (An important exception was observed recently for amorphous Si [5] deposited by hot-wire chemical vapor deposition where the experimental thermal conductivity is a factor of 4 larger than predicted.) In the high temperature limit where all vibrational modes are thermally excited, the predicted minimum thermal conductivity is $\Lambda_{\min} = 0.40k_B n^{2/3} (v_l + 2v_t)$, where n is the atomic density and v_l and v_t are the longitudinal and transverse speeds of sound, respectively [2].

The validity of this description of the thermal transport for an amorphous polymer can be questioned, however, because of strong deviations from a Debye-like density of vibrational states: stiff force constants associated with covalent bonding within the polymer backbone and side groups coexist with soft force constants associated with non-bonding interactions between chains. Furthermore, non-bonded interactions between the chains are significantly non-linear and anharmonic interactions between localized

vibrations, of the type invoked in “fracton hopping” models [6], could conceivably contribute to heat transport. Evidence for the importance of anharmonicity in the thermal conductivity of amorphous polymers was recently observed in molecular dynamics simulations of polystyrene [7] and proteins [8, 9]. Pressure tuning of the thermal conductivity enables a critical test of the minimum thermal conductivity model by enabling a continuous variation of the atomic density and elastic constants.

Prior experimental work on the pressure dependence of the thermal conductivity $\Lambda(P)$ of polymers [10-12] extends to only $P \approx 2$ GPa because of limitations of the types of pressure cells used in the prior work. Modern diamond or SiC anvil cell techniques [13-15] easily generate the high pressures needed to significantly alter the elastic constants of a polymer. For example, the pressure dependence of the elastic constant C_{11} of a typical glassy polymer is on the order of $C_{11} \approx 8 \text{ GPa} + 7P$ and, therefore, at $P=10$ GPa, C_{11} increases by an order of magnitude to $C_{11} \approx 80$ GPa, comparable to the elastic constants of Al at ambient conditions. Here, we present our combined experimental and computational study of the elastic constants and thermal conductivity Λ of glassy polymers: an experimental study of poly(methyl methacrylate) and a numerical study of a computer-based model of polystyrene.

II. EXPERIMENTAL DETAILS

SiC anvils were etched in 10% HF solutions, rinsed with DI water, and sonicated in chloroform followed by ethanol to remove surface contaminants. The anvils were then treated with a piranha solution (3 H₂SO₄ : 1 H₂O₂ (v/v)) to hydroxylate the surface and facilitate chemical attachment of the radical initiator, (11-(2-bromo-2-methyl)propionyloxy) undecyltrichlorosilane [16]. PMMA brushes were grown from these surfaces by atom-transfer radical polymerization (ATRP) [17]. By term “brush”, we are referring to polymer chains covalently bonded to a surface at spacing shorter than the radius of gyration [18]. Copper (I) chloride was used as the ATRP catalyst. The thickness of the brush and molecular weight of the PMMA chains increased with increasing polymerization time. We determined the thickness of the brush by picosecond acoustics measurements and comparisons to a simulation of the acoustics signals based on Ref. [19]. From this film thickness and the molecular weight, we calculated a grafting density of ≈ 0.6 chains nm⁻², indicating sufficient overlap to force the extension of polymer chains into the brush regime [18].

The PMMA brushes were then coated with a thin Al film, ≈ 80 nm thick, by magnetron sputter deposition to act as an optical transducer for time-domain thermoreflectance measurements. We pressurized the SiC anvil cell by loading with Ar cryogenically or by

loading with H₂O as the pressure medium. (Since Ar is a liquid at $P < 1.3$ GPa and sometimes leaked from the cell, H₂O was used for measurements at $P < 1.4$ GPa. At room temperature and $P > 1.3$ GPa, the equilibrium phase of Ar is a hcp crystal [20].) The pressure was determined by ruby fluorescence [21].

The thermal conductivity Λ of PMMA brushes was measured by comparing time-domain thermoreflectance (TDTR) [22-24] data obtained at room temperature to calculations using a thermal model [25] which takes into account heat flow through the polymer layer and into the SiC substrate as well as heat flow into the pressure medium [26]. The thermal model contains many parameters—laser spot size, and the thickness, heat capacity and thermal conductivity of each layer—but the thermal conductivity of the PMMA brush is the only significant unknown. The PMMA layers are chosen to be thin so that most of the heat flows into the high thermal conductivity SiC anvil and only a small fraction of the heat flows into the low thermal conductivity pressure medium; uncertainties in the thermal properties of the pressure medium propagate to less than 2% error in the measurements of the thermal conductivity of our thickest, 22 nm, PMMA layers at 10 GPa.

The thickness of the Al film was determined by picosecond acoustics and our estimates of the heat capacity of Al at high pressures were described in Ref. [15]. Changes in the

PMMA thickness were calculated from the equation of state of PMMA. (Our approach for determining the equation of state is described below.) Because the PMMA layers are “thermally thin”, the model is not sensitive to the heat capacity of the PMMA brush.

We cannot directly measure the elastic constant of a thin polymer brush and instead measured the elastic constant C_{11} of a thick ($>1\mu\text{m}$), spun-cast layer of PMMA by time-domain Brillouin scattering [15, 27, 28]. For longitudinal modes in a backscattering geometry, the Brillouin frequency is $f = 2Nv_l / \lambda$, where N is the refractive index, v_l the longitudinal sound velocity, and $\lambda=785$ nm is the laser wavelength. Figure 1(a) shows the pressure dependence of f .

We determine the equation of state and elastic constant C_{11} by a self-consistent, iterative approach; the result is plotted in Fig. 1(b). To begin, we use a trial function for the isothermal bulk modulus $B_T=6$ GPa+ $6P$ and calculate the pressure dependence of the density $\rho(P)$, index of refraction $N(P)$, and $C_{11}(P)$ from the picosecond acoustics data using the Lorentz-Lorenz formula $(N^2 - 1)/(\rho(N^2 + 2)) = A$, where A is a constant [15]. (At ambient pressure $\rho=1.19$ g cm⁻³ and $A=0.241$.) Assuming a constant Poisson ratio of $1/3$, $B_T(P) = (2/3)C_{11}(P)$. We fit this $B_T(P)$ to a second order polynomial in P and calculate the pressure dependence of the molecular density n from $B_T = n(dP/dn)_T$. We iterate the procedure described above until C_{11} and B_T are self-consistent. The final

equation of state is $B_r = B_0 + B_1P + B_2P^2$, where $B_0=6.15$ GPa, $B_1=7$, and $B_2=-0.17$ GPa⁻¹.

The atomic density n increases by 31% at 5 GPa and 46% at 10 GPa. We have assumed that under high pressure the amorphous polymer deforms plastically so that the state of stress is close to hydrostatic. (At low pressures, the yield strength of PMMA is $\tau_y \approx 0.05$ GPa+0.2 P [29].)

III. RESULTS AND DISCUSSION

Figure 2 shows $\Lambda(P)$ of PMMA brushes (solid symbols) with different thicknesses; $\Lambda(P)$ is independent of the thickness h when $h > 6$ nm and increases monotonically with increasing P . (The uncertainty in the thermal conductivity measurements is ≈ 10 % and dominated by uncertainties in the thicknesses of PMMA and Al.) For comparison, we also measured $\Lambda(P)$ of a 10 nm thick spun-cast PMMA (open diamond) and found the spun-cast and brush forms of PMMA show the same behavior. Our data at ambient pressure, ≈ 0.185 W m⁻¹ K⁻¹, are in good agreement with the literature value, ≈ 0.20 W m⁻¹ K⁻¹ (open square) [30, 31]; the weaker pressure dependence at low pressure regime is similar to that of prior work by Andersson (open circle) [10] whose ambient value, 0.225 W m⁻¹ K⁻¹, is ≈ 10 % higher than the data reported in Refs. [30, 31].

The fact that brushes and spun-cast layers behave similarly is consistent with our

previous study of the thickness dependence of the effective thermal conductivity at ambient pressure [32]. The dry polymer brushes that we are studying are amorphous and the chain extension is relatively small; we estimated previously that the brushes are extended to only 25% of their contour length and that the enhancement of thermal conductivity created by this extension is not significant compared to the experimental uncertainties of the data plotted in Fig. 2.

Data sets for 9 and 22 nm thick brushes and the 10 nm thick spun-cast layer include measurements for both increasing and decreasing pressure. This lack of hysteresis shows that any structural changes in the PMMA under pressure are reversible.

Our measurements of the thermal conductivity of PMMA layers include the contribution to the thermal resistance from the bulk of the material as well as the thermal resistance of the Al/PMMA and PMMA/SiC interfaces. We have not experimentally determined the series sum of the Al/PMMA and PMMA/SiC interface conductance; instead, we estimate $G \approx 300 \text{ MW m}^{-2} \text{ K}^{-1}$ based on our previous study of the thickness dependence of the effective thermal conductivity of spun-cast PMMA [32]. Using this estimate, the sum of the Kapitza lengths of Al/PMMA and PMMA/SiC interfaces is small, $l_K = \Lambda / G \sim 1 \text{ nm}$, and therefore we do not expect a significant reduction in the effective thermal conductivity of PMMA due to the finite interfacial thermal conductance even for

our thinnest (6 nm) brushes.

In Fig. 2, we also compare our data for $\Lambda(P)$ with the behavior predicted by the model of the minimum thermal conductivity Λ_{\min} [2]. In the high temperature limit, Λ_{\min} depends only on n and the sound velocities, $v_l = \sqrt{C_{11}/\rho}$ and $v_t = \sqrt{C_{44}/\rho}$. If we assume that the ratio C_{11}/C_{44} is approximately independent of pressure, the pressure dependence of Λ_{\min} simplifies to $\Lambda_{\min} = \Lambda_0 n^{1/6} C_{11}^{1/2}$. A fit to the average of our data at ambient pressure $\Lambda = 0.185 \text{ W m}^{-1} \text{ K}^{-1}$ gives $\Lambda_0 = 3.25 \times 10^{-11} \text{ J}^{1/2} \text{ m K}^{-1} \text{ s}^{-1}$ using $n = 4.3 \times 10^{28} \text{ m}^{-3}$ and $C_{11} = 9.2 \text{ GPa}$. The dashed line in Fig. 2 shows an evaluation of this expression using the C_{11} derived from our polynomial fit and n determined by the equation of state $B_T = n(dP/dn)_T$ as described above.

The pressure dependence of the thermal conductivity can also be described approximately by a relatively simple function of pressure. In the limit of high pressure, the elastic constant C_{11} is approximately linear in P , and $n^{1/6}$ is essentially constant. As a result, the predicted thermal conductivity can be expressed as $\Lambda = \Lambda_1 + \Lambda_2 P^{1/2}$, where $\Lambda_1 = 0.185 \text{ W m}^{-1} \text{ K}^{-1}$ is the thermal conductivity at ambient pressure and $\Lambda_2 \approx 0.11 \text{ W m}^{-1} \text{ K}^{-1} \text{ GPa}^{-1/2}$.

The predicted thermal conductivity based on $\Lambda_{\min} = \Lambda_0 n^{1/6} C_{11}^{1/2}$ captures the trends in our data and accurately predicts $\Lambda(P)$ at higher pressures. We note that in the low pressure

regime, $P < 1$ GPa, our data deviate slightly from the prediction but the difference is small and comparable to the experimental uncertainties. (Andersson's data show a similar deviation from the model prediction even after picking a new $\Lambda_0 = 3.95 \times 10^{-11} \text{ J}^{1/2} \text{ m K}^{-1} \text{ s}^{-1}$ to fit the data of Ref. [10] at ambient pressure.) The good agreement between our data and the model prediction over the entire pressure range supports the idea that the dominant mechanism of thermal transport in glassy polymers is the exchange of thermal energy between non-propagating vibrational modes [33].

To gain further insight into the mechanism of heat transport in amorphous polymers, and to evaluate the generality of our findings, we performed molecular dynamics (MD) simulations on a model of polystyrene (PS); polystyrene is chosen because of a well-established set of force field parameters for sp^3 - and sp^2 -hybridized carbon atoms and hydrogen atoms existing in Polymer Consistent Force Field [34]. Recently, Algaer and collaborators [35] also reported the pressure dependence of the thermal conductivity of polystyrene obtained via MD simulations. However, in their studies, pressures up to only 60 MPa were investigated, and consequently no dependence on the elastic constants was determined.

A structural model of amorphous atactic polystyrene (PS) including all atoms was initially generated by a Monte-Carlo algorithm based on the rotational isomeric state (RIS)

model [36]. The initial structure was then equilibrated at $T=298$ K and various hydrostatic pressures for times up to 3 ns until a stable density was reached. The model contained 6084 atoms in 18 chains, packed in a bar-shaped cell. At ambient pressure, the size of the simulation cell was $139.6 \times 22.5 \times 21.4 \text{ \AA}^3$, corresponding to a density of 0.966 g cm^{-3} . At a pressure of 20 GPa, the stable density was 1.665 g cm^{-3} .

To calculate the thermal conductivity, we used an MD time step of 0.5 fs and periodic boundary conditions in 3 dimensions. The temperature and pressure were controlled during equilibration by a Berendsen thermostat and barostat. The non-equilibrium thermal conductivity [37] was determined using a constant heat flux imposed by a heat source at the center of the computational cell and a heat sink at the edges of the cell. The value of the flux was chosen such that the total temperature drop across the model was in the range of 20-50 K. In steady-state, a linear temperature profile is established and the thermal conductivity was evaluated from Fourier's law. Molecular dynamics simulations capture heat transfer due to propagating (polarized), and diffusive (delocalized but not polarized) modes, as well as heat transfer between localized modes when anharmonic effects are important [7-9]. By analyzing the results as a function of cell size, we established that the conductivity converges at cell sizes of approximately 10 nm. Our reported results are for a simulation cell that is 14 nm long at ambient pressure.

Figure 3 presents the pressure dependence of the thermal conductivity of polystyrene by MD simulations. The solid line shows the predicted Λ based on the minimum thermal conductivity model with $\Lambda_0 = 5.66 \times 10^{-11} \text{ J}^{1/2} \text{ m K}^{-1} \text{ s}^{-1}$, determined from a fit to $\Lambda_{\text{min}} = 0.20 \text{ W m}^{-1} \text{ K}^{-1}$ at ambient pressure. The excellent agreement between the MD simulations and the model prediction indicates that the mechanism of thermal transport in amorphous polymers is the same as assumed by the minimum thermal conductivity model. It also suggests that indeed a universal thermal transport mechanism exists in amorphous polymers where thermal energy is transferred predominately through the diffusion of thermal energy between non-propagating vibrational modes.

As a striking contrast with the relatively weak pressure dependence predicted by the model of minimum thermal conductivity, the Leibfried-Schlömann (LS) equation, often used to describe the thermal conductivity of isotropic crystalline solids, predicts a strong pressure dependence:

$$\Lambda_{LS} = A \frac{V^{\frac{1}{3}} \omega_D^3}{\gamma^2 T}, \quad (1)$$

where V is the volume, ω_D the Debye frequency, γ the Grüneisen constant, T the temperature, and A is a constant independent of pressure [38, 39]. If we assume that γ is also independent of pressure and $\omega_D \propto \sqrt{C_{11}}$, then the predicted $\Lambda(P)$ based on Eq. (1) is

shown as the dashed line in Fig. 3. The distinctly different pressure dependence of Λ predicted by the LS equation supports our conclusion that diffusion of thermal energy between non-propagating vibrational modes dominates heat conduction in amorphous polymers. The propagation of wave-like vibrational modes—the dominant heat conduction mechanism in crystalline structures—is a minor consideration.

IV. CONCLUSION

In summary, we have studied the pressure dependence of elastic constants and thermal conductivity of PMMA using time-domain Brillouin scattering and time-domain thermoreflectance combined with SiC anvil cell techniques. The pressure dependent $\Lambda(P)$ of PMMA by TDTR measurements and polystyrene by MD simulations can both be well accounted for by the model of minimum thermal conductivity. It also appears that there is no need to invoke localized excitations and non-harmonic energy transfer to capture the basic heat transfer mechanism in amorphous polymers. We point out, however, that with increasing pressure, contrast in the bonding strength between non-bonded and covalent interactions becomes less pronounced; these effects may reduce the density of localized vibrations at high pressures and suppress contributions to thermal transport from localized modes and anharmonic effects.

ACKNOWLEDGMENTS

This work was supported by the US Air Force Office of Scientific Research Grant No. MURI FA9550-08-1-0407. W.-P. H. acknowledges support from the Carnegie-DOE Alliance Center (CDAC) through grant DE-FC52-08NA28554. We thank H. Maris and B. Daly for providing a computer code for simulating picosecond acoustics data.

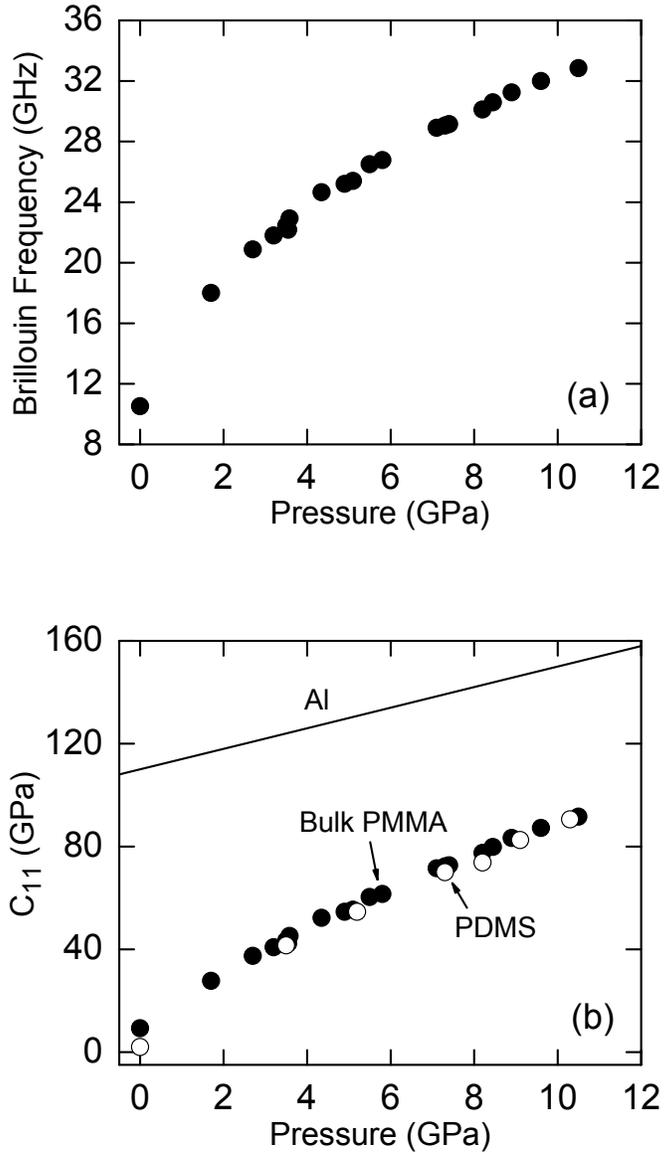


FIG. 1. Pressure dependence of the (a) Brillouin frequency and (b) C_{11} of a spun-cast layer of PMMA. C_{11} is derived from the Brillouin frequency data using a self-consistent equation of state of PMMA and the assumptions that the Poisson ratio is constant and the refractive index follows the Lorentz-Lorenz equation. Data for PDMS [40] and previously estimated $C_{11} = 110 \text{ GPa} + 4P$ of Al [41] are plotted for comparison.

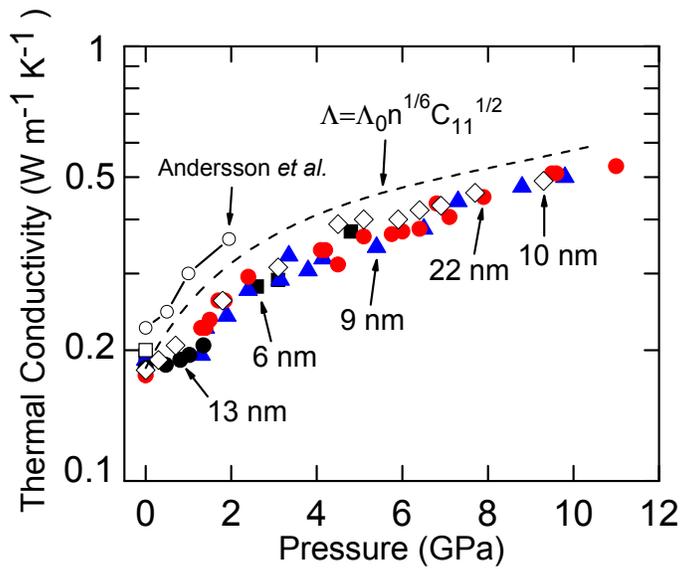


FIG. 2. Measurements of the thermal conductivity of PMMA brushes (solid symbols) and a spun-cast layer (open diamond) as a function of pressure. The uncertainty in the thermal conductivity and pressure measurements are $\approx 10\%$ and 0.2 GPa, respectively. Ar was the pressure medium for all measurements except for that of 13 nm brushes and 10 nm spun-cast layer where H₂O was used. The dashed line shows the predicted thermal conductivity of PMMA based on the minimum thermal conductivity model, the pressure dependence of the atomic density n , and the elastic constant C_{11} obtained by a polynomial fit. Data for bulk PMMA by Andersson *et al.* (open circle) [10] and by Cahill *et al.* and Putnam *et al.* (open square) [30, 31] are included for comparison. Lines between Andersson's data are added to emphasize that the pressure dependence of the prior data are similar to that of our measurements in the low pressure regime.

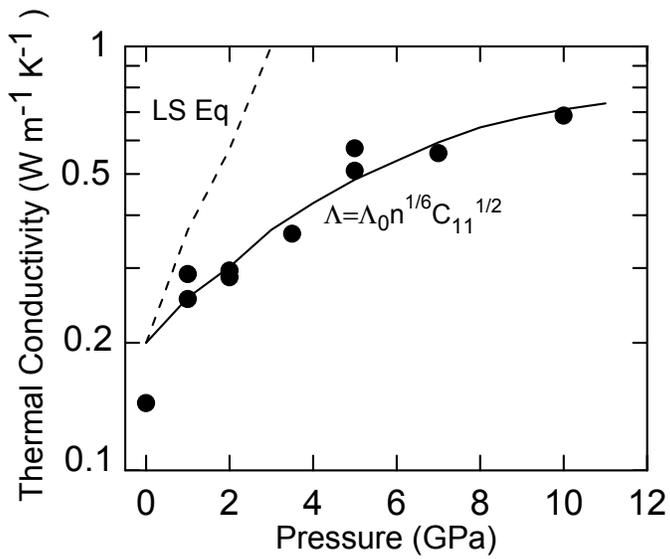


FIG. 3. Pressure dependence of the thermal conductivity of polystyrene by molecular dynamics simulations (solid circles). The solid line shows the predicted thermal conductivity by the model of the minimum thermal conductivity. The pressure dependence of the thermal conductivity predicted by the Leibfried-Schlömann equation using the scaling $\omega_D \propto \sqrt{C_{11}}$ is shown as the dashed line.

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