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Phys. Rev. Applied **9**, 054011 — Published 8 May 2018

DOI: [10.1103/PhysRevApplied.9.054011](https://doi.org/10.1103/PhysRevApplied.9.054011)

1 **Magnetization Switching of a Co/Pt-Multilayer Perpendicular Nanomagnet**
2 **Assisted by a Microwave Field with Time-Varying Frequency**

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8 Abstract

9 Microwave-assisted magnetization switching (MAS) is attracting attention as a method for
10 reversing nanomagnets with a high magnetic anisotropy by using a small-amplitude magnetic
11 field. In this paper, we experimentally study MAS of a perpendicularly magnetized nanomagnet
12 by applying a microwave magnetic field with a time-varying frequency. Because the microwave
13 field frequency can follow the nonlinear decrease of the resonance frequency, larger
14 magnetization excitation than that in a constant-frequency microwave field is induced, which
15 enhances the MAS effect. The switching field decreases almost linearly as the start value of the
16 time-varying microwave field frequency increases, and becomes smaller than the minimum
17 switching field in a constant-frequency microwave field. To obtain this enhancement of the MAS
18 effect, the end value of the time-varying microwave field frequency needs to be almost the same
19 as or lower than the critical frequency for MAS in a constant-frequency microwave field. In
20 addition, the frequency change needs to take typically 1 ns or longer to make the rate of change
21 slow enough for the magnetization to follow the frequency change. This switching behavior is
22 qualitatively explained by the theory based on the macrospin model.

23

1 **1. INTRODUCTION**

2 Magnetization switching that utilizes ferromagnetic resonance (FMR) excitation has attracted
3 attention as a write method in next-generation magnetic recording [1]–[20]. To date,
4 experimental studies on this kind of magnetization switching have employed a microwave field
5 with a time-constant frequency and have shown that the switching field of a nanomagnet
6 substantially decreases by applying a microwave field with a frequency of the order of the FMR
7 frequency of the nanomagnet [5]. This switching method is called microwave-assisted
8 magnetization switching (MAS). Furthermore, magnetization switching induced solely by a
9 circularly polarized microwave field has been proposed and experimentally demonstrated
10 [10],[11]. FMR is a nonlinear phenomenon and the resonance frequency at which the
11 magnetization excitation becomes largest depends on the amplitude of the magnetization
12 excitation. Because the FMR-based magnetization switching methods utilize large magnetization
13 excitation, the nonlinearity plays an important role and needs to be taken into account to explain
14 the switching behavior [12]–[14]. At the same time, the nonlinearity of FMR suggests that a
15 microwave field with a time-varying frequency can induce larger magnetization excitation than a
16 microwave field with a time-constant frequency. Regarding nanomagnets with perpendicular
17 magnetic anisotropy, which are of interest in high-density magnetic recording applications, the
18 resonance frequency decreases as the amplitude of the magnetization excitation evolves.
19 Therefore, by gradually decreasing the frequency of the microwave field, the nonlinear decrease
20 of the resonance frequency can be followed and the magnetization excitation can be enhanced.
21 Theoretical and micromagnetic simulation studies have reported that this kind of microwave field
22 can efficiently induce magnetization switching [15]–[19]. However, no experimental studies
23 have yet been reported.

1 In magnetic recording applications, it has been proposed that a spin-torque oscillator (STO)
2 can be used as a microwave field source [21],[22]. One way to realize a varying-frequency
3 microwave field is to change the current injected into the STO [17]. Furthermore, it has been
4 reported that, in a certain geometry, the STO spontaneously changes the frequency during the
5 switching process because of the interaction with the media magnetization [19].

6 In this paper, we experimentally study magnetization switching of a Co/Pt nanomagnet with
7 perpendicular magnetic anisotropy by applying a microwave field with a time-varying frequency
8 and compare the switching behavior with that in a microwave field with a constant frequency.
9 For convenience, we introduce the following symbols for microwave field frequency (f_{rf}). In
10 constant-frequency MAS (CF-MAS), the microwave field frequency is constant and is referred to
11 as $f_{\text{rf}}^{\text{const}}$. In varying-frequency MAS (VF-MAS), the start and end values of the time-varying
12 microwave field frequency are referred to as $f_{\text{rf}}^{\text{start}}$ and $f_{\text{rf}}^{\text{end}}$, respectively. In CF-MAS, the
13 switching field of the nanomagnet decreases almost linearly with increasing $f_{\text{rf}}^{\text{const}}$, reaches a
14 minimum at the critical frequency, and then increases abruptly. In VF-MAS, the switching field
15 similarly decreases linearly with increasing $f_{\text{rf}}^{\text{start}}$ but continues to decrease even when $f_{\text{rf}}^{\text{start}}$
16 becomes higher than the critical frequency for CF-MAS. The switching field thus becomes lower
17 than the minimum switching field for CF-MAS, showing that the MAS effect is enhanced by a
18 microwave field with varying frequency. To obtain this enhancement of the MAS effect, $f_{\text{rf}}^{\text{end}}$
19 needs to be almost the same as or lower than the critical frequency for CF-MAS. In addition, the
20 f_{rf} change needs to take approximately 1 ns or longer when $f_{\text{rf}}^{\text{end}}$ is set to half of $f_{\text{rf}}^{\text{start}}$ to
21 make the rate of f_{rf} change sufficiently slow. The switching behavior of VF-MAS can be
22 explained qualitatively by the theory that describes the magnetization dynamics of a single spin
23 in a microwave magnetic field.

1

2 2. SAMPLE STRUCTURE AND EXPERIMENTAL SETUP

3 Figure 1(a) shows the sample structure and the measurement setup. A Ta bottom layer and
4 Co/Pt multilayer magnetic film are deposited on a sapphire substrate by using a magnetron
5 sputtering system. The film structure from bottom to top is Ta 200 / Pt 50 / (Co 13.6 / Pt 5) \times 5 /
6 Pt 50 / Ta 50 (thicknesses are given in angstroms). Figure 1(b) shows magnetization as a function
7 of the z -direction magnetic field (H_z) measured by using a vibrating sample magnetometer. The
8 average saturation magnetization (M_s) of the Co/Pt film is estimated to be 1200 emu/cm³,
9 assuming that the total thickness of the magnetic layer is from the bottommost Co layer to the
10 topmost Co layer. Figure 1(c) shows vector network analyzer (VNA)-FMR spectra of the film
11 sample as a function of H_z . At around $H_z = 0$ Oe, the FMR peak disappears because of the
12 formation of reversed magnetic domains, and the FMR frequency at $H_z = 0$ Oe is estimated to
13 be 5 GHz by linear extrapolation. This FMR frequency indicates that the effective perpendicular
14 anisotropy field ($H_{\text{ani}}^{\text{eff}}$) of the film, including the demagnetizing field, is approximately 1.8 kOe,
15 and the perpendicular anisotropy field (H_{ani}) is estimated to be 16.9 kOe from $H_{\text{ani}} = H_{\text{ani}}^{\text{eff}} +$
16 $4\pi M_s$. Figure 1(d) shows the linewidth of the FMR absorption peak (Δf_{FMR}) as a function of the
17 resonance frequency (f_{FMR}) obtained in the H_z range from -2.4 to -0.8 kOe. This
18 relationship can be expressed as $\Delta f_{\text{FMR}} = 2\alpha f_{\text{FMR}} + \Delta f_0$, where Δf_0 denotes linewidth
19 broadening due to the film inhomogeneity. From the fitting, the damping parameter (α) of the
20 film is estimated to be 0.035.

21 The Co/Pt film is then patterned into a nanomagnet with a diameter of 50 nm by electron-beam
22 lithography and Ar ion milling. The Ta bottom layer is patterned into a Hall cross to detect
23 switching of the nanomagnet by the anomalous Hall effect. After that, insulating layers of

1 20-nm-thick SiN and 80-nm-thick SiO₂ are sputter-deposited, and a coplanar waveguide (CPW)
2 made of 100-nm-thick Cu with thin adhesion layers is fabricated. The signal line of the CPW
3 passes above the nanomagnet with a separation of 100 nm. The widths of the CPW signal (S)
4 line, ground (G) lines and gaps are 1 μm, 2 μm, and 2 μm above the nanomagnet and gradually
5 expand to 80 μm, 80 μm, and 45 μm at the contact pads. These dimensions are chosen to make
6 the characteristic impedance roughly 50 Ω, as calculated by using AppCAD software. Note that
7 the CPW dimensions are the design values, and the actual dimensions deviate from them and
8 have a tapered cross-section. The length of the CPW is 750 μm. This length is approximately one
9 tenth of the wavelength of microwave signal travelling through the CPW at 16 GHz, which is the
10 highest in the studied frequency range. A transmission electron microscopy image of the
11 nanomagnet that has a slightly different Co thickness but is fabricated using the same process is
12 provided in Ref. [9].

13 We study switching of the nanomagnet by applying H_z and an in-plane microwave magnetic
14 field from the CPW. When no microwave field is applied, the switching z -direction dc magnetic
15 field (H_{sw}) of the nanomagnet is 5.7 kOe. Hereafter, this value is referred to as the intrinsic H_{sw} .
16 To generate a microwave field, a microwave signal is generated from Keysight M8195A
17 arbitrary waveform generator (AWG) with a 64-GHz sampling rate, amplified by RF-LAMBDA
18 RFLUPA00G22GA wide-band amplifier, and introduced to the CPW. The amplifier has a
19 bandwidth of 0.02–22 GHz, average gain of +30 dB, and a gain flatness of ±2.5 dB. Figure 1(e)
20 shows the microwave transmission between the cable end connected to the AWG and the cable
21 end connected to the input of the CPW as measured by the VNA. The variation from +22 to
22 +28 dB is due to the frequency dependence of the gain of the amplifier and the attenuation of
23 the cables. The microwave property of the CPW is also evaluated. Figure 1(f) shows the

1 microwave transmission between the input and the output of the CPW. The attenuation ranges
2 from -2 dB to -3 dB. The microwave reflection at the CPW input [Fig. 1(g)] is
3 approximately -14 dB, showing that there is no severe reflection point such as a large
4 impedance mismatch. Considering that the phase of the reflection is close to 0° (data not
5 shown), the characteristic impedance of the CPW is estimated to be approximately 75Ω . In this
6 estimation, multiple reflection in the CPW is neglected. In addition, the CPW is shorter than the
7 one tenth of the wavelength; thus impedance mismatch has a small effect on the microwave
8 transmission. We employ the sum of the microwave transmission from the AWG to CPW input
9 and half of the microwave transmission of the CPW as the microwave transmission from the
10 AWG to above the nanomagnet because the nanomagnet is located below the middle of the
11 CPW. This calculated microwave transmission is used to construct the waveform of the AWG.

12 The microwave field amplitude (H_{rf}) generated from the CPW is estimated by using the Biot–
13 Savart formula assuming a uniform current in the signal line. In this estimation, the tapered
14 cross-section of the CPW observed by transmission electron microscopy is considered. When a
15 microwave signal with a voltage (V_{rf}) of 1 V travels above the nanomagnet, a microwave field
16 with $H_{\text{rf}} = 85$ Oe is applied. The microwave signal is modulated into pulses of
17 nanosecond-order duration to avoid heating the sample and is emitted repeatedly from the AWG
18 at 122 kHz.

19 Figure 2 (a) shows the waveform of a constant-frequency microwave signal that has 5-ns
20 rise/fall time, 10-ns plateau time, $V_{\text{rf}} = 1.0$ V, and $f_{\text{rf}}^{\text{const}} = 12$ GHz. The rise and fall times are
21 fixed to 5 ns throughout the experiments, and the plateau time is 10 ns except when the plateau
22 time dependence is measured in Section 3D . The measured voltage is larger than 1 V because
23 this signal waveform is measured by disconnecting the cable end from the CPW input and

1 connecting it to an oscilloscope with an 80-GHz sampling rate. The signal amplitude, therefore,
 2 further attenuates by half of the microwave transmission in Fig. 1(f) and becomes almost 1 V
 3 above the nanomagnet. Figure 2(d) shows the instantaneous f_{rf} estimated from the zero-cross
 4 intervals of the waveform, which confirms that f_{rf} is actually 12 GHz. Similarly, a
 5 varying-frequency microwave signal is generated that takes into account the frequency
 6 dependence of the microwave transmission. Figure 2(b) shows the waveform of a
 7 varying-frequency microwave signal with $V_{\text{rf}} = 1.0$ V, $f_{\text{rf}}^{\text{start}} = 12$ GHz, and $f_{\text{rf}}^{\text{end}} = 0.02$ GHz.
 8 During the rise/fall time, f_{rf} is constant, and during the plateau time, f_{rf} decreases. The signal
 9 amplitude is almost the same as that with the constant frequency [Fig. 2(a)], although it fluctuates
 10 because the frequency-dependent microwave transmission is not perfectly compensated for.
 11 Regarding the f_{rf} change, we think that the rate of f_{rf} change should be faster when f_{rf} is
 12 higher because it takes a shorter time for a microwave field to induce magnetization excitation
 13 when f_{rf} is higher. To realize such f_{rf} change, we employ the following function:

$$f_{\text{rf}}(t) = f_{\text{rf}}^{\text{start}} \exp\left(-\frac{t}{t_{\text{plateau}}} \ln \frac{f_{\text{rf}}^{\text{start}}}{f_{\text{rf}}^{\text{end}}}\right), \quad (1)$$

14 where t_{plateau} denotes the plateau time. This function is derived from $df_{\text{rf}}/dt \propto f_{\text{rf}}$, where the
 15 rate of f_{rf} change is proportional to f_{rf} . This function is one example of f_{rf} change, and further
 16 study is necessary to optimize f_{rf} change for efficient MAS. Note that Ref. [15] reported a
 17 function in which f_{rf} always matches the resonance frequency when α is small. Figure 2(e)
 18 shows the estimated instantaneous f_{rf} of the waveform in Fig. 2(b), which confirms that f_{rf}
 19 changes as designed. Figures 2(c) and 2(f) show a constant-frequency signal waveform with V_{rf}
 20 = 1.5 V and $f_{\text{rf}}^{\text{const}} = 12$ GHz and the instantaneous f_{rf} , which we mention later in the next
 21 section.

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3. EXPERIMENTAL RESULTS

A. Comparison between constant-frequency MAS and varying-frequency MAS, and effect of the start frequency on varying-frequency MAS

In this section, we first study switching of the nanomagnet in a constant-frequency microwave field, and then apply a varying-frequency microwave field to study the effect of $f_{\text{rf}}^{\text{start}}$.

Figure 3(a) shows the dependence of H_{sw} on $f_{\text{rf}}^{\text{const}}$ for CF-MAS. These data, and this kind of frequency dependence of H_{sw} as shown later in this paper, are measured as follows: at each frequency the nanomagnet is initialized to the $-z$ direction, and H_z is increased in steps of 10 Oe per 0.3 s until magnetization switching is detected. During this H_z increase, a pulsed microwave field is applied repeatedly. Each curve in Fig. 3(a) is obtained by setting V_{rf} to 0.5–2.0 V, which generates H_{rf} of 43–170 Oe. As $f_{\text{rf}}^{\text{const}}$ increases, H_{sw} decreases almost linearly until H_{sw} takes a minimum at the critical frequency, and then H_{sw} increases abruptly to the intrinsic H_{sw} of 5.7 kOe. This kind of switching behavior has been reported by previous experimental studies on MAS [5], which can be understood as follows. When H_z is applied in the opposite direction to the magnetization, the FMR frequency decreases. Therefore, the resonance condition in which the FMR frequency is near $f_{\text{rf}}^{\text{const}}$ results in a $H_{\text{sw}}-f_{\text{rf}}^{\text{const}}$ curve with a negative slope. However, when $f_{\text{rf}}^{\text{const}}$ becomes higher than the critical frequency, matching H_z becomes so small that a microwave field cannot induce magnetization excitation large enough to induce magnetization switching. As H_{rf} increases, the critical frequency increases and the corresponding H_{sw} decreases, showing that a larger MAS effect is obtained by applying a microwave field with larger H_{rf} .

Figure 3(b) shows the dependence of H_{sw} on $f_{\text{rf}}^{\text{start}}$ for VF-MAS. To focus on the effect of

1 $f_{\text{rf}}^{\text{start}}$, $f_{\text{rf}}^{\text{end}}$ is set as low as 0.02 GHz. When $f_{\text{rf}}^{\text{start}}$ is smaller than the critical frequency of
 2 CF-MAS, the H_{sw} versus $f_{\text{rf}}^{\text{start}}$ curves almost coincide with the H_{sw} versus $f_{\text{rf}}^{\text{const}}$ curves
 3 for CF-MAS. This coincidence indicates that magnetization switching in the varying-frequency
 4 microwave field occurs in the same manner as CF-MAS because the frequencies of the two kinds
 5 of microwave field are almost the same at the beginning of the f_{rf} change. When $f_{\text{rf}}^{\text{start}}$
 6 becomes higher than the critical frequency, H_{sw} continues to decrease and becomes smaller
 7 than the minimum value for CF-MAS, showing that the MAS effect is enhanced. We now
 8 confirm that this enhancement of the MAS effect actually originates from the varying-frequency
 9 microwave field by examining the waveform of the microwave signals. In VF-MAS, H_{sw} for
 10 $V_{\text{rf}} = 1.0$ V decreases to 3.05 kOe at $f_{\text{rf}}^{\text{start}} = 12$ GHz. In CF-MAS, no MAS effect is obtained
 11 for $V_{\text{rf}} = 1.0$ V at $f_{\text{rf}}^{\text{const}} = 12$ GHz because $f_{\text{rf}}^{\text{const}}$ is above the critical frequency, and the
 12 MAS effect is obtained by increasing V_{rf} to 1.5 V, where the critical frequency is at 12.5 GHz.
 13 Waveforms of these signals are shown in Figs. 2(a), 2(b), and 2(c). The amplitude of the
 14 varying-frequency microwave signal for $V_{\text{rf}} = 1.0$ V [Fig. 2(b)] is clearly smaller than that of the
 15 constant-frequency microwave signal for $V_{\text{rf}} = 1.5$ V [Fig. 2(c)]. The fact that these two signals
 16 achieve almost the same MAS effect is evidence that the enhancement in the MAS effect is due
 17 to the varying-frequency microwave field.

18 As $f_{\text{rf}}^{\text{start}}$ increases, the H_{sw} curves for $V_{\text{rf}} = 0.5, 1.0,$ and 1.5 V take the minimum and
 19 increase abruptly. For $V_{\text{rf}} = 2.0$ V, such an abrupt H_{sw} increase does not appear, probably
 20 because its frequency is above 16 GHz. This abrupt increase in H_{sw} cannot be explained by
 21 considering only f_{rf} . For example, H_{sw} for $V_{\text{rf}} = 1.0$ V and $f_{\text{rf}}^{\text{start}} = 12$ GHz (below the
 22 abrupt increase) is smaller than that for $V_{\text{rf}} = 1.0$ V and $f_{\text{rf}}^{\text{start}} = 12.5$ GHz (above the abrupt
 23 increase), which is inconsistent with the fact that the f_{rf} change for $f_{\text{rf}}^{\text{start}} = 12.5$ GHz passes

1 through $f_{\text{rf}}^{\text{start}} = 12$ GHz and decreases to $f_{\text{rf}}^{\text{end}} = 0.02$ GHz. This indicates that the rate of f_{rf}
 2 change needs to be taken into account, and the switching behavior can be explained as follows.
 3 When $f_{\text{rf}}^{\text{start}}$ is too high, the rate of f_{rf} change becomes too fast for the magnetization
 4 excitation to follow. As a result, the varying-frequency microwave field can no longer enhance
 5 the MAS effect. Above the abrupt increase, H_{sw} becomes approximately the same as H_{sw} at
 6 the critical frequency for CF-MAS. This result indicates that magnetization switching occurs in
 7 the same manner as CF-MAS when f_{rf} decreases and matches the critical frequency for
 8 CF-MAS.

9

10 **B. Effect of the end frequency on varying-frequency MAS**

11 We next examine the effect of $f_{\text{rf}}^{\text{end}}$ on VF-MAS. As shown in the previous section,
 12 enhancement of the MAS effect was not apparent for $V_{\text{rf}} = 2.0$ V because the critical frequency
 13 is already close to the upper limit of the studied frequency range. Thus, we show the results for
 14 $V_{\text{rf}} = 0.5, 1.0,$ and 1.5 V. We fix $f_{\text{rf}}^{\text{start}}$ to 8, 12, and 15 GHz, respectively, for $V_{\text{rf}} = 0.5, 1.0,$
 15 and 1.5 V, at which H_{sw} takes the minimum in Fig. 3(b), and $f_{\text{rf}}^{\text{end}}$ is varied. Figures 4(a) to
 16 4(d) show the waveforms and estimated instantaneous f_{rf} of signals with $V_{\text{rf}} = 1.0$ V, $f_{\text{rf}}^{\text{start}} =$
 17 12 GHz, and $f_{\text{rf}}^{\text{end}} = 1$ and 11 GHz, respectively, which confirm that the signals have the
 18 designed amplitude and frequency regardless of the amount of f_{rf} change. Figure 4(e) shows the
 19 dependence of H_{sw} on $f_{\text{rf}}^{\text{end}}$. As already shown in the previous section, H_{sw} becomes smaller
 20 than H_{sw} at the critical frequency for CF-MAS when $f_{\text{rf}}^{\text{end}} = 0.02$ GHz, because the
 21 varying-frequency microwave field enhances the MAS effect. As $f_{\text{rf}}^{\text{end}}$ increases, H_{sw} is first
 22 constant and then abruptly increases to the intrinsic H_{sw} , showing that the MAS effect
 23 disappears when $f_{\text{rf}}^{\text{end}}$ is too high. Waveforms of the signals for $f_{\text{rf}}^{\text{end}}$ below and above the

1 abrupt H_{sw} increase [Figs. 4(a) and 4(b)] confirm that this drastic change of the switching
2 behavior originates from the different f_{rf}^{end} . The frequency at which H_{sw} increases is almost
3 the same as the corresponding critical frequency. This result shows that f_{rf}^{end} needs to be
4 approximately the same as or lower than the critical frequency for CF-MAS to enhance the MAS
5 effect by applying a varying-frequency microwave field.

6

7 **C. Minimizing the switching field by applying a varying-frequency microwave field**

8 In Section 3A, the H_{sw} curves for VF-MAS exhibited the abrupt increase because the rate of
9 f_{rf} change became too fast. This suggests that H_{sw} can be even smaller when the rate of f_{rf}
10 change is sufficiently slow. To determine the minimum H_{sw} that can be achieved by VF-MAS,
11 we again measure the dependence of H_{sw} on f_{rf}^{start} . In Section 3B, it was found that f_{rf}^{end}
12 needs to be almost the same as or lower than the critical frequency for CF-MAS. Based on this
13 finding, f_{rf}^{end} is set to the critical frequencies of 7, 9.5, and 12.5 GHz, respectively, for $V_{rf} =$
14 0.5, 1.0, and 1.5 V. As shown in Fig. 5, H_{sw} gradually decreases with increasing f_{rf}^{start} , and
15 then H_{sw} becomes almost constant with no abrupt increase. This constant H_{sw} means that
16 magnetization switching occurs in the same manner in this f_{rf}^{start} range because the f_{rf} change
17 for a certain f_{rf}^{start} passes through the f_{rf} change for a lower f_{rf}^{start} . The constant H_{sw} also
18 means that the rate of f_{rf} change is sufficiently slow. Therefore, the obtained H_{sw} is
19 considered to be the minimum that can be achieved by VF-MAS. The difference between the
20 minimum H_{sw} for CF- and VF-MAS is the largest for $V_{rf} = 1.0$ V followed by 1.5 V and 0.5 V,
21 showing that a varying-frequency microwave field can enhance the MAS effect most efficiently
22 for a certain H_{rf} . This H_{rf} dependence is theoretically discussed in Section 4.

23

1 **D. Effect of rate of change in microwave field frequency**

2 In this section, we study the effect of the rate of f_{rf} change by varying t_{plateau} . We set $f_{\text{rf}}^{\text{start}}$
3 to 8, 12, and 15 GHz respectively for $V_{\text{rf}} = 0.5, 1.0, \text{ and } 1.5 \text{ V}$, which were used for measuring
4 the $f_{\text{rf}}^{\text{end}}$ dependence [Fig. 4(e)], and we set $f_{\text{rf}}^{\text{end}}$ to half of $f_{\text{rf}}^{\text{start}}$. Figures 6(a) and 6(b) show
5 the waveform and estimated instantaneous f_{rf} of a signal with $V_{\text{rf}} = 1.0 \text{ V}$, $f_{\text{rf}}^{\text{start}} = 12 \text{ GHz}$,
6 $f_{\text{rf}}^{\text{end}} = 6 \text{ GHz}$, and $t_{\text{plateau}} = 2 \text{ ns}$, which confirm that the signal has the designed amplitude
7 and frequency even for the short t_{plateau} . Figure 6(c) shows the dependence of H_{sw} on t_{plateau} .
8 When t_{plateau} is 2 ns, H_{sw} is the same as that for the slow f_{rf} change [Fig. 5], showing that
9 the rate of f_{rf} change is sufficiently slow at 2 ns. As t_{plateau} decreases, H_{sw} is first constant
10 and then increases abruptly. This increase appears at $t_{\text{plateau}} = 1.0 \text{ ns} - 1.2 \text{ ns}$, depending on
11 V_{rf} . Below these t_{plateau} values, the rate of f_{rf} change becomes too fast and the enhancement
12 of the MAS effect disappears. Immediately after this abrupt increase, H_{sw} becomes almost the
13 same as H_{sw} at the critical frequency for CF-MAS. As already discussed in Section 3A, this is
14 because magnetization switching occurs in the same manner as CF-MAS when f_{rf} decreases to
15 the critical frequency. As t_{plateau} further decreases, H_{sw} gradually increases. This t_{plateau}
16 dependence is explained as follows. As the rate of f_{rf} change becomes faster, the time duration
17 in which f_{rf} is near the critical frequency becomes shorter. Because the magnetization excitation
18 is still developing on this timescale, the MAS effect weakens, and thus H_{sw} increases.

19

20 **4. THEORY OF MAGNETIZATION SWITCHING IN A VARYING-FREQUENCY** 21 **MICROWAVE FIELD BASED ON THE MACROSPIN MODEL**

22 The magnetization dynamics of a single spin in a rotating microwave field can be described by
23 the Landau–Lifshitz–Gilbert (LLG) equation formulated in a rotating frame, and the switching

1 condition can be derived by examining the stability of the steady state solutions of the LLG
2 equation [12]. Although issues such as spatially non-uniform magnetization excitation [6], a
3 quasiperiodic magnetization motion [12], and thermally activated magnetization switching [14]
4 are not accounted for, it is known that the switching behavior of CF-MAS is qualitatively
5 reproduced by this approach. In this section, we explain the switching behavior of VF-MAS
6 using this approach. We employ the following normalization, which is applicable to
7 magnetization with uniaxial anisotropy, regardless of the strength of the anisotropy field. The
8 rotating microwave field and z-direction dc magnetic field are normalized in units of the
9 anisotropy field (H_{ani}): $h_{\text{rf}} = H_{\text{rf}}^{\text{rot}}/H_{\text{ani}}$, $h_z = H_z/H_{\text{ani}}$. Note that $H_{\text{rf}}^{\text{rot}}$ here means the
10 amplitude of the rotating microwave field, whereas H_{rf} in the experiments meant the amplitude
11 of the microwave field alternating in one direction. It has been reported that a rotating microwave
12 field induces the same MAS effect at half the microwave field amplitude in comparison with an
13 alternating microwave magnetic field [8],[9]. This is because an alternating microwave field is
14 decomposed into two rotating microwave fields that rotate in the opposite direction and have half
15 the amplitude, and only the rotating microwave field that rotates in the same direction as the
16 FMR precession induces magnetization excitation. The microwave field frequency is normalized
17 in units of the FMR frequency: $\omega_{\text{rf}} = (2\pi f_{\text{rf}})/(\gamma H_{\text{ani}})$, where γ denotes the gyromagnetic ratio.
18 Similarly, time is normalized as $\tau = t(\gamma H_{\text{ani}})$. The LLG equation that describes the dynamics of
19 the magnetization direction $\tilde{\mathbf{m}}$ in the rotating frame (\tilde{x} , \tilde{y} , \tilde{z}) is given by [14]

$$\frac{d\tilde{\mathbf{m}}}{d\tau} = -\tilde{\mathbf{m}} \times [h_{\text{rf}} \mathbf{e}_{\tilde{x}} + (-h_z + \tilde{m}_{\tilde{z}} - \omega_{\text{rf}}) \mathbf{e}_{\tilde{z}} + \alpha \omega_{\text{rf}} \tilde{\mathbf{m}} \times \mathbf{e}_{\tilde{z}}] + \alpha \tilde{\mathbf{m}} \times \frac{d\tilde{\mathbf{m}}}{d\tau} . \quad (2)$$

20 Note that the damping constant α is the only remaining parameter as a result of the
21 normalization.

1 Figures 7(a) and 7(b) show the cone angle of the steady state solutions obtained by setting
 2 $d\tilde{\mathbf{m}}/d\tau = 0$ and analytically solving Eq. 2. The stability of the solution—stable, saddle, and
 3 unstable—evaluated by introducing a small deviation is also shown. Parameters $\alpha = 0.17$ and
 4 $h_{\text{rf}} = 0.05$ are chosen to reproduce the experimentally obtained CF- and VF-MAS results for V_{rf}
 5 $= 1.0$ V, which we discuss later in detail. For clarity, the cone angle is shown up to 90° , and
 6 there is always a stable state near 180° , which corresponds to the switched state. Here, stable
 7 state means that the magnetization can stay in the state and rotates in synchronization with the
 8 microwave field. The magnetization cannot stay in unstable and saddle states and move to the
 9 stable state. Figure 7(a) corresponds to the critical frequency ($\omega_{\text{rf}} = 0.32$) for CF-MAS. As h_z
 10 increases from zero, the magnetization follows the line of the stable state and the cone angle
 11 gradually increases because h_z approaches the resonance condition. At around $h_z = 0.5$
 12 (dashed line), the stable state disappears, which means that the induced magnetization excitation
 13 overcomes the barrier for switching. Thus, the magnetization moves to the other stable state near
 14 180° , and MAS occurs. The solution shows hysteresis like a protrusion toward the lower right
 15 direction. In CF-MAS, however, this hysteresis is saddle or unstable and has no effect on
 16 magnetization switching.

17 Figure 7(b) shows calculation results for ω_{rf} values higher than the critical frequency. At ω_{rf}
 18 $= 0.58$, a peak appears in the cone angle due to FMR. As ω_{rf} decreases to 0.5 , hysteresis
 19 appears and two stable states exist in a narrow h_z range near 0.3 . These two stable states are
 20 referred to as a lower-angle branch and higher-angle branch. As shown in the inset, the
 21 magnetization follows the higher-angle branch in the downward h_z sweep, and the cone angle
 22 abruptly decreases at the edge of the higher-angle branch. Similarly, the magnetization follows
 23 the lower-angle branch in the upward h_z sweep, and the cone angle abruptly increases at the

1 edge of the lower-angle branch. This is called the foldover effect [23]. In the experiments, h_z is
 2 swept only in the upward direction. Thus, in CF-MAS where ω_{rf} is fixed, the magnetization is
 3 always in the lower angle branch. At $\omega_{\text{rf}} = 0.45$, this hysteresis becomes more obvious. In these
 4 three conditions, MAS does not occur because one or more stable states exist. At $\omega_{\text{rf}} = 0.39$, an
 5 unstable state appears around the edge of the higher-angle branch. In CF-MAS, this condition is
 6 still higher than the critical frequency, and magnetization switching does not occur because of
 7 one or more stable states. As seen in Fig. 7(a), this unstable state expands as ω_{rf} further
 8 decreases. Now we apply a varying-frequency microwave field. In the experiments, f_{rf} is
 9 changed on the nanosecond timescale while H_z is changes on the second time scale. Therefore,
 10 we consider that the magnetization moves on the curves for different ω_{rf} at constant h_z . As the
 11 magnetization moves on the curves from higher ω_{rf} to lower, the magnetization is able to stay
 12 on the higher-angle branch. This is in contrast to CF-MAS where the magnetization is always in
 13 the lower-angle branch. When the higher-angle branch becomes unstable at $\omega_{\text{rf}} = 0.39$, the
 14 magnetization can move to the stable state near 180° instead of the stable lower-angle branch,
 15 which results in the enhanced MAS by a varying-frequency microwave field.

16 The unstable state in the higher-angle branch appears when ω_{rf} is slightly higher than the
 17 critical frequency, which indicates that ω_{rf} needs to decrease to a slightly higher value than the
 18 critical frequency to induce VF-MAS. This result explains the experimentally obtained
 19 dependence on $f_{\text{rf}}^{\text{end}}$ [Fig. 4(e)] in which the MAS effect appears when $f_{\text{rf}}^{\text{end}}$ is almost the
 20 same as or lower than the critical frequency. The dependence on $f_{\text{rf}}^{\text{start}}$ can be explained by
 21 using Figs. 7(a) and 7(b). The switching condition for CF-MAS is determined by the edge of the
 22 lower-angle branch, where the stable state disappears. In VF-MAS, the cone angle first increases
 23 at the edge of the lower-angle branch. As f_{rf} decreases, the magnetization stays on the

1 higher-angle branch until it become unstable. In other words, both CF- and VF-MAS are initiated
2 by the transition of the magnetization excitation at the edge of the lower-angle branch. Because
3 this edge shows an almost linear relationship with respect to ω_{rf} , the H_{sw} curves for CF- and
4 VF-MAS show the same linear relationship with respect to f_{rf}^{const} and f_{rf}^{start} , regardless of the
5 fact that magnetization switching occurs in a different manner.

6 The dependence on the rate of f_{rf} change can be understood as follows. When ω_{rf} changes
7 fast, the cone angle of the magnetization becomes smaller than the calculated value because the
8 calculated value is a steady state solution and f_{rf} changes faster than the relaxation time of the
9 magnetization. When the magnetization cannot keep staying on the higher angle branch and falls
10 to the lower-angle branch, MAS cannot be enhanced. As shown in Fig. 6(c), even when the rate
11 of f_{rf} change becomes so fast that the enhancement of MAS disappears, H_{sw} is still smaller
12 than the intrinsic H_{sw} . This is because MAS occurs when f_{rf} decreases below the critical
13 frequency. This kind of MAS occurs for faster f_{rf} change in comparison with the enhancement
14 of MAS by VF-MAS. We explain this using Fig. 7(c), which shows calculation results for ω_{rf}
15 values slightly lower than the critical frequency. At around $h_z = 0.6$ (dashed line) there is no
16 stable state for both $\omega_{rf} = 0.28$ and 0.24 . When ω_{rf} changes in this range, the magnetization
17 moves to the switched state. This is in contrast to Fig. 7(b) (ω_{rf} is higher than the critical
18 frequency) in which the magnetization can fall to the lower angle branch. Because the
19 magnetization moves one-way to the switched state during the ω_{rf} change, this kind of MAS
20 occurs when the rate of f_{rf} change is relatively fast.

21 The minimum switching h_z obtained for VF-MAS is 0.33, as indicated by the dashed line in
22 Fig. 7(b). This h_z corresponds to the limit where the higher-angle branch always exists during
23 the f_{rf} change, which is necessary for the cone angle to gradually increase until switching

1 occurs.

2 We compare the experimental results with the calculation, and for this purpose, we estimate
3 the H_{sw} without microwave fields as follows. The intrinsic H_{sw} of 5.7 kOe reflects thermally
4 activated magnetization switching. Although MAS is also thermally activated, the thermal effect
5 acts effectively only during the microwave field application which has a duty ratio of
6 approximately 0.001 (10-ns plateau time and 122-kHz repetition). Owing to the difference in the
7 timescale of thermal effect, MAS above the intrinsic H_{sw} is screened, and the H_{sw} versus
8 f_{rf}^{const} curves change a slope at around $f_{rf}^{const} = 3$ GHz in Fig. 3(a). If the thermal effect was
9 reduced to that of the time scale of MAS, the H_{sw} versus f_{rf}^{const} curves would have a constant
10 slope and the intercept at $f_{rf}^{const} = 0$ Hz would be H_{sw} in the static in-plane field with an
11 amplitude of H_{rf} . Thus, the intercept of the extrapolated H_{sw} versus f_{rf}^{const} curve for $V_{rf} =$
12 0.5 V, which is approximately 7 kOe, is employed as the H_{sw} with no microwave field under
13 the reduced thermal effect. The ratios of the minimum H_{sw} for $V_{rf} = 1.0$ V obtained by CF-
14 and VF- MAS [3.8 kOe in Fig. 3(b) and 2.6 kOe in Fig. 5] to this H_{sw} value are 0.54 and 0.37,
15 respectively, which approximately coincide with the calculation results of 0.5 and 0.33.

16 We would like to comment on α and the microwave field amplitude. The damping parameter
17 $\alpha = 0.17$ is larger than the value estimated from the VNA-FMR measurement of the film. This
18 deviation may originate from the facts that MAS involves large-amplitude magnetization
19 excitation, whereas VNA-FMR measurement uses small-amplitude magnetization precession.
20 Increase of α by a factor of 5 in large-amplitude magnetization excitation has been reported [24].
21 In addition, α is affected by the fact that the nanomagnet has non-uniform demagnetizing field,
22 whereas the film has uniform demagnetizing field. When we use the H_{sw} of 7 kOe without
23 microwave field as H_{ani} for a rough estimation, $h_{rf} = 0.05$ corresponds to $H_{rf}^{rot} = 350$ Oe for a

1 rotating microwave field and $H_{\text{rf}} = 700$ Oe for an alternating microwave field, which is much
2 larger than $H_{\text{rf}} = 85$ Oe in the experiments. This disagreement is because the fact that the
3 calculation does not include thermal activation and spatially non-uniform magnetization
4 excitation. According to the study using macrospin model with thermal activation, [14] thermal
5 effect alone cannot explain the disagreement, and spatially non-uniform magnetization excitation
6 may make a large contribution. The issue of non-uniform magnetization excitation is presented in
7 Ref. [6], which discusses a comparison of experimental results, macrospin simulations, and
8 micromagnetic simulations.

9 Figures 8(a) and 8(b) show the calculation results for $h_{\text{rf}} = 0.075$. Similar to the case of h_{rf}
10 $= 0.05$, enhancement of the MAS effect by varying-frequency microwave field appears.
11 According to this approach, the enhancement of the MAS effect becomes larger as h_{rf}
12 increases, which cannot explain the experimental result in which the enhancement of the MAS
13 effect is the largest for $V_{\text{rf}} = 1.0$ V. Because α is the only parameter in Eq. 2, the experimental
14 result can be understood as increased damping in large magnetization excitation. As shown in
15 Figs 8(c) and 8(d), the hysteresis becomes less evident as α is increased to 0.22. Because
16 CF-MAS does not utilize the hysteresis, the MAS effect of CF-MAS is almost unchanged.
17 However, because VF-MAS utilizes the hysteresis, the enhancement of the MAS effect by
18 VF-MAS decreases as α increases. This α dependence is consistent with previous theoretical
19 and simulation studies [16],[20]. This result implies that the effective damping of the
20 nanomagnet that includes the intrinsic damping of the material, the spatial inhomogeneity of the
21 magnetic anisotropy and demagnetizing field, the spatially non-uniform magnetization
22 excitation, and the spin pumping, may increase as the magnetization excitation becomes larger,
23 which reduces the enhancement of the MAS effect in a varying-frequency microwave field.

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5 SUMMARY

We studied switching of a perpendicularly magnetized nanomagnet in a microwave field with time-varying frequency and explained the switching behavior by using the theory based on the macrospin model. When the frequency of the microwave field gradually decreases, a larger MAS effect than that in a constant-frequency microwave field is obtained because the microwave field frequency follows the nonlinear decrease of the resonance frequency and induces larger magnetization excitation. The switching field decreases almost linearly as the start frequency of the microwave field increases up to a certain frequency, beyond which further increase in the start frequency does not change the switching field. To obtain enhancement of the MAS effect, the end frequency of the microwave field needs to be approximately the same as or lower than the critical frequency for constant-frequency MAS. In addition, frequency change of a microwave field needs to take approximately 1 ns to make the rate of change sufficiently slow so that the magnetization excitation can follow the varying-frequency microwave field.

ACKNOWLEDGEMENTS

We thank Canon ANELVA Corp. for technical support. This work was supported by Strategic Promotion of Innovative Research and Development from Japan Science and Technology Agency, JST.

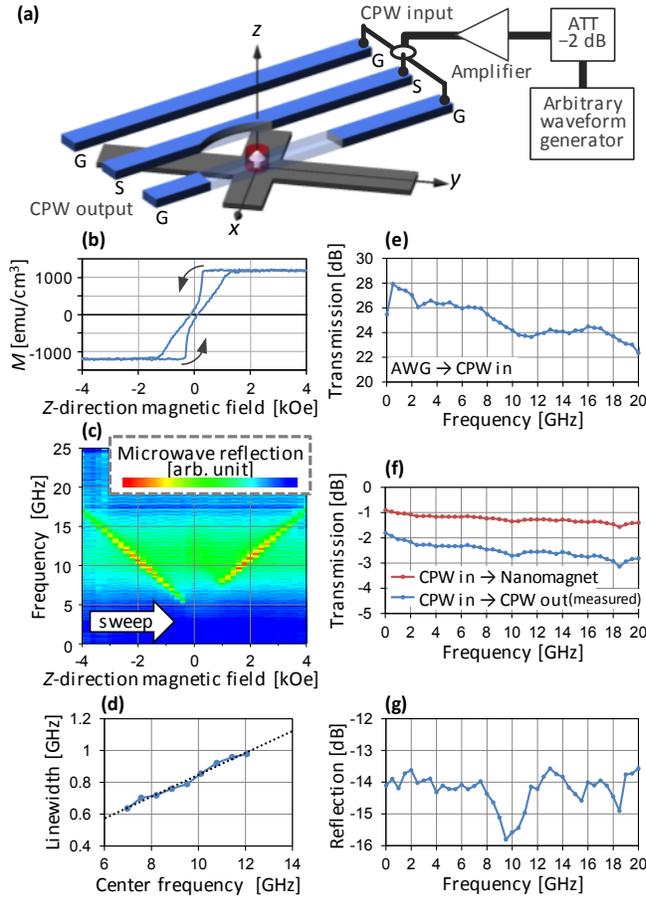
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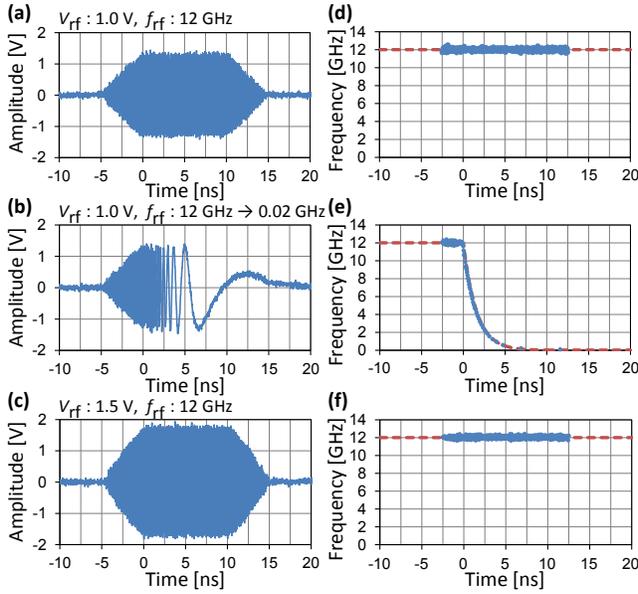
1 FIG 1



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 4 FIG. 1. (a) Sample structure and experimental setup. (b) $M-H_z$ loop obtained for the film sample
 5 having an area of 1 cm^2 . (c) VNA-FMR spectra versus H_z obtained for the film sample. (d)
 6 Linewidth of the FMR absorption peak versus FMR frequency. The dotted line depicts the linear
 7 fit. (e) Microwave transmission between the cable end connected to the AWG and the cable end
 8 connected to the CPW input. (f) Microwave transmission between the input and output of the
 9 CPW. Half of the measured value is employed as microwave transmission between the CPW
 10 input and above the nanomagnet. (g) Microwave reflection at the CPW input.

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1 FIG 2



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4 FIG. 2. (a), (b), and (c) Waveforms of signals for the following parameter sets: ($V_{rf} = 1.0 \text{ V}$,

5 $f_{rf}^{\text{const}} = 12 \text{ GHz}$), ($V_{rf} = 1.0 \text{ V}$, $f_{rf}^{\text{start}} = 12 \text{ GHz}$, $f_{rf}^{\text{end}} = 0.02 \text{ GHz}$), and ($V_{rf} = 1.5 \text{ V}$, f_{rf}^{const}

6 $= 12 \text{ GHz}$). These waveforms are measured at the cable end connected to the CPW input, and the

7 amplitude further attenuates by half of the microwave transmission in Fig. 1(f) when above the

8 nanomagnet. Because this attenuation is from -1 to -1.5 dB , the signal amplitude becomes

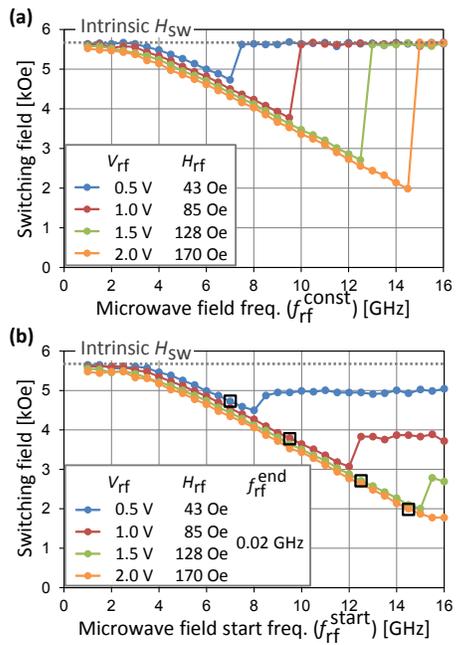
9 89% to 84% of the measured voltage. (d), (e), and (f) Instantaneous f_{rf} estimated from the

10 zero-cross intervals of the waveforms. Each dot corresponds to one zero-cross interval. The dots

11 overlap the designed f_{rf} depicted by dashed lines.

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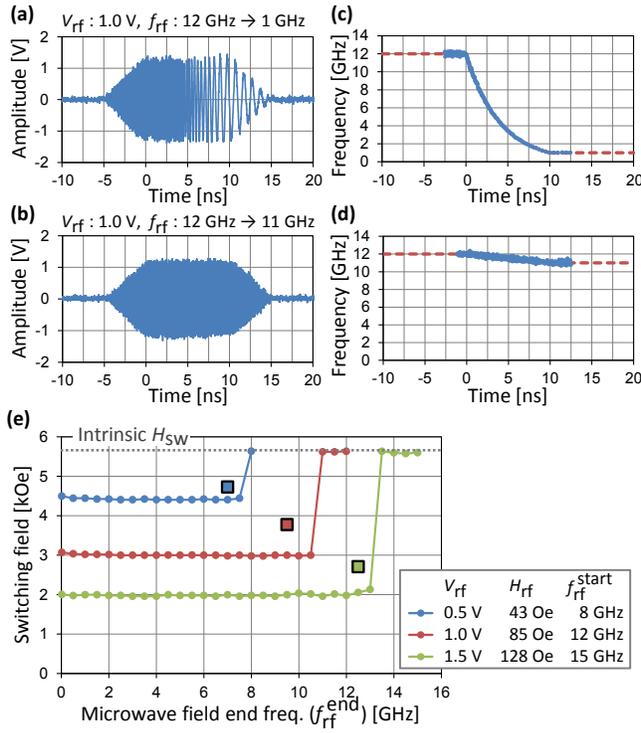
1 FIG. 3



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4 FIG. 3. (a) H_{sw} versus f_{rf}^{const} for CF-MAS. (b) H_{sw} versus f_{rf}^{start} for VF-MAS obtained by
5 setting $f_{rf}^{end} = 0.02$ GHz. Squares show the corresponding critical frequency and H_{sw} for
6 CF-MAS.

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1 FIG 4



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4 FIG. 4. (a) and (b) Waveforms of signals for the following parameter sets: ($V_{rf} = 1.0 \text{ V}, f_{rf}^{\text{start}} =$

5 $12 \text{ GHz}, f_{rf}^{\text{end}} = 1 \text{ GHz}$) and ($V_{rf} = 1.0 \text{ V}, f_{rf}^{\text{start}} = 12 \text{ GHz}, f_{rf}^{\text{end}} = 11 \text{ GHz}$). (c) and (d)

6 Instantaneous f_{rf} estimated from the zero-cross intervals of the waveforms. (e) H_{sw} versus

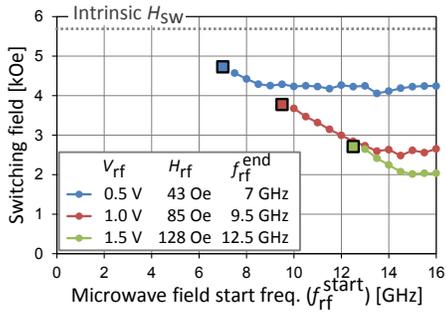
7 f_{rf}^{end} for VF-MAS obtained by setting $f_{rf}^{\text{start}} = 8, 12,$ and 15 GHz respectively for $V_{rf} = 0.5,$

8 $1.0,$ and 1.5 V . Squares show the corresponding critical frequency and H_{sw} for CF-MAS.

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4 FIG. 5. H_{sw} versus f_{rf}^{end} for VF-MAS obtained by setting $f_{rf}^{end} = 7, 9.5,$ and 12.5 GHz
 5 respectively for $V_{rf} = 0.5, 1.0,$ and 1.5 V. Squares show the corresponding critical frequency and

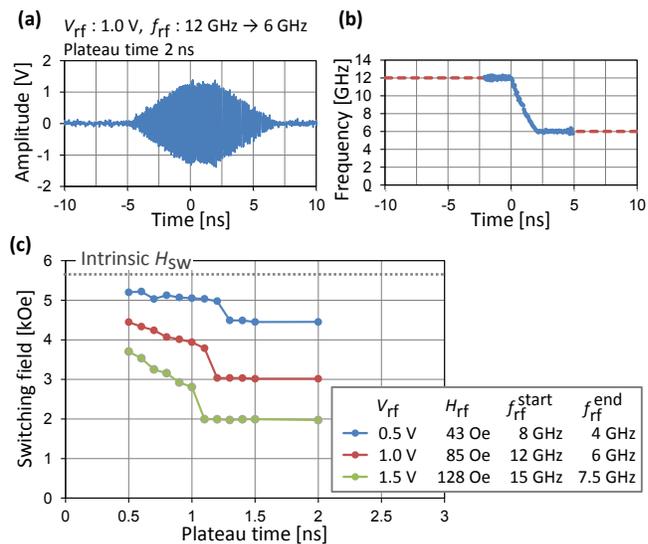
6 H_{sw} for CF-MAS.

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1 FIG 6



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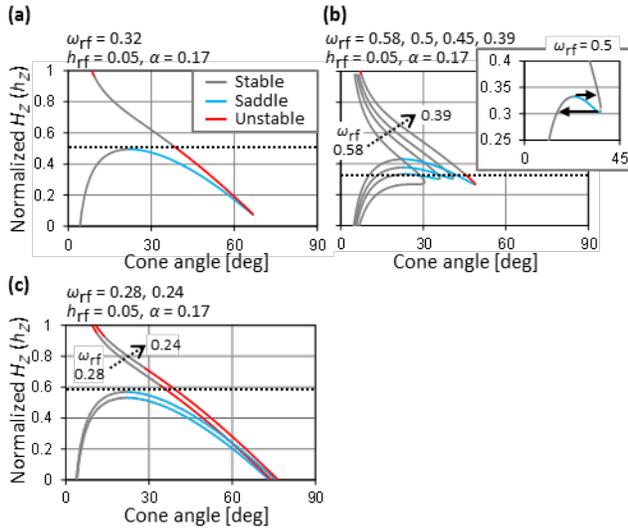
4 FIG. 6. (a) and (b) Waveform and instantaneous f_{rf} of a signal with $V_{rf} = 1.0 \text{ V}$, $f_{rf}^{\text{start}} = 12$

5 GHz, $f_{rf}^{\text{end}} = 6 \text{ GHz}$, $t_{\text{plateau}} = 2 \text{ ns}$. (c) H_{sw} versus t_{plateau} for VF-MAS obtained by setting

6 $f_{rf}^{\text{end}} = f_{rf}^{\text{start}}/2$.

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1 FIG 7



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4 FIG. 7. (a) Cone angle and stability of the magnetization excitation for $h_z = 0.05$ and $\alpha = 0.17$

5 at the critical frequency ($\omega_{rf} = 0.32$), (b) at higher ω_{rf} values, and (c) at lower ω_{rf} values. In

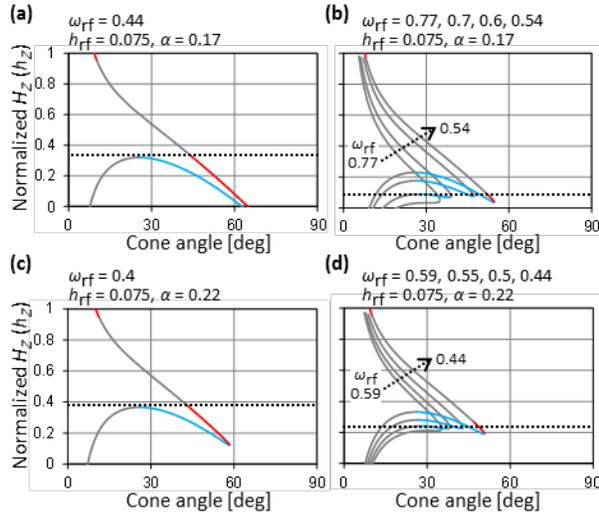
6 (b), ω_{rf} is 0.58, 0.5, 0.45, and 0.39 from the curve with the smallest cone angle to the one with

7 the largest cone angle. The inset shows an enlarged view of the data for $\omega_{rf} = 0.5$. In (c), ω_{rf} is

8 0.28 and 0.24 from the curve with the smaller cone angle to the one with the larger cone angle.

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5 FIG. 8. (a) and (b) Cone angle and stability of the magnetization for $h_z = 0.075$ and $\alpha = 0.17$ at
6 the critical frequency ($\omega_{rf} = 0.44$) and at higher ω_{rf} values. In (b), ω_{rf} is 0.77, 0.7, 0.6, and
7 0.54 from the curve with the smallest cone angle to the one with the largest cone angle. (c) and
8 (d) Cone angle and stability of the magnetization for $h_z = 0.075$ and $\alpha = 0.22$ at the critical
9 frequency ($\omega_{rf} = 0.4$) and at higher ω_{rf} values. In (d), ω_{rf} is 0.59, 0.55, 0.5, and 0.44 from the
10 curve with the smallest cone angle to the one with the largest cone angle. Dashed lines show the
11 minimum switching h_z for CF- and VF-MAS.

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