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Thermal Wave Diode

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Based on the spatiotemporal modulation of the thermal conductivity and volumetric heat capacity, we propose a thermal wave diode characterized by the rectification of the heat currents carried by thermal waves. By transforming the Fourier's law for the heat flux and the diffusion equation for the temperature into equations with constant coefficients, it is shown that: (i) the rectification effect is generated by the simultaneous wave-like modulation of both thermal properties, such that it disappears in absence of any of them. (ii) The rectification factor can be optimized and tuned by means of the speed and phase difference of the variations of the heat capacity and thermal conductivity. High rectification factors, greater than 86%, are obtained for lower frequencies driving the propagation of thermal waves. The proposed thermal wave diode is thus analogous to its electronic counterpart operating with modulated electrical currents and can open a vista for developing different types of thermal wave logic components.

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Nonlinear heat transport based on the metal-insulator transition of materials [1] and the coupling of dissimilar lattices [2–5] have recently attracted a great interest to control conductive and radiative heat currents [6–10]. This phenomenon is observed in materials with thermal and optical properties depending on temperature, which has been exploited to conceive and develop thermal diodes [6, 11–17], thermal transistors [18–21], thermal memories [22, 23], and thermal memristors [24, 25] that make possible to process information via thermal electrons, phonons and photons. The operation of these thermal devices is, however, usually limited to the temperature interval in which the material properties exhibit significant changes with temperature. Heat control with nonlinear materials is thus typically restricted to narrow temperature ranges.

Materials with properties periodically modulated in space and time are able to overcome the major drawbacks of nonlinear ones, given that they are able to operate at the required temperature, frequency and scale [26, 27]. This spatiotemporal modulation of the material properties has been theoretical and experimentally studied in elastic [8, 28, 29], acoustic [30–33], photonic [34, 35] and thermal [36–39] systems. As a result of the wave-like variation of their properties, these materials exhibit a nonreciprocal response for the propagation of waves, which provides an effective method to allow the flow of energy in a given direction and impede it in the opposite one. By considering the spatiotemporal modulation of the thermal conductivity and heat capacity in the form of a traveling wave, Torrent *et al.* [39] showed that a material behaves like an effective medium with constant thermal properties and an internal convection-like term in the diffusion equation describing its temperature profile. This convective term induces the nonreciprocal response of the

material for the heat flux, which takes different values depending on its direction parallel or anti-parallel to the traveling waves of the thermal properties. The authors thus demonstrated that materials with thermal conductivity and heat capacity periodically modulated in space and time can be used to develop thermal diodes operating with steady-state heat fluxes [39]. As this modulation of the thermal properties has a dynamical origin, its impact on the transient heat conduction regime is expected to be strong, but has not been studied yet. In particular, given that this dynamic regime is driven by the heat capacity, its spatiotemporal modulation may induce a nonreciprocal behavior on the heat flux carried by the thermal waves predicted by the Fourier's law [40]. These diffusion waves are periodic temperature fluctuations widely applied in thermal detection via photothermal and photoacoustic techniques [40–42] that could be implemented to generate and detect the rectification of their heat currents.

The purpose of this letter is to demonstrate the proof of principle of a thermal wave diode based on the spatiotemporal modulation of the thermal conductivity and volumetric heat capacity. This is done by determining and optimizing the rectification of the heat fluxes carried by the nonreciprocal thermal waves propagating in the forward and backward bias. In contrast to the steady-state thermal diodes, which typically operate with large temperature gradients [16, 17], this thermal wave diode functions with relatively small heat currents modulated in frequency, as is the case of its electronic counterpart.

Let us consider two thermal baths exchanging heat by conduction through a nonreciprocal material, due to their temperature difference $T_h - T_c + \delta T \cos(\omega t)$ periodically modulated in time t with a frequency ω , as shown in Figs. 1(a) and 1(b). In the forward configuration (Fig. 1(a)),

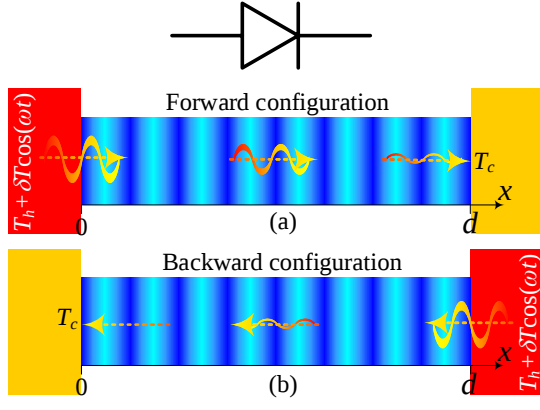


FIG. 1: Scheme of a thermal wave diode operating in the (a) forward and (b) backward configurations. The arrows along with their amplitude indicate the propagation direction and intensity of the thermal waves generated by the external excitation $\delta T \cos(\omega t)$.

the heat flux q_F is driven from left to right ($T_h > T_c$), while in the backward one (Fig. 1(b)), the heat flux q_B appears in the opposite direction. The magnitudes of q_F and q_B are expected to be different due to the periodic modulation in space x and time t of the material conductivity $k = k(x - vt)$ and volumetric heat capacity $C = C(x - vt)$, which are known to induce nonreciprocal heat transport [39]. These thermal properties thus behave like waves traveling at speed v and are periodic functions of $x - vt$ with period a . The working principle of the proposed diode is hence based on the propagation of thermal waves driven by the spatiotemporal modulation of thermal properties, which is different from the steady-state diodes based on the temperature dependence of the thermal conductivity [11] and nonlinear lattices [6]. Given that q_F and q_B will generally depend on position x , the ability of our thermal wave diode to rectify heat currents can be defined by the following rectification factor R [6, 11]

$$R = \frac{||q_F(x=d)| - |q_B(x=0)||}{\max(|q_F(x=d)|; |q_B(x=0)|)}. \quad (1)$$

The optimal rectification ($R \rightarrow 1$) is thus achieved when the reversal of the thermal gradient induces a sizeable variation of the heat flux magnitude. Considering that the diode length d and period a are much longer than the mean free path ($\sim 1 - 10^3$ nm [40]) of the material heat carriers and that the heat flux is determined at a time much longer than their relaxation time ($\sim 1 - 10^3$ ps [40]), the heat flux in each configuration is given by the Fourier's law $q = -k(x - vt)\partial T/\partial x$, where the temperature T is described by the diffusion equation [39, 43]

$$\frac{\partial}{\partial x} \left(k(x - vt) \frac{\partial T}{\partial x} \right) = C(x - vt) \frac{\partial T}{\partial t}. \quad (2)$$

The wave-like modulation of k and C can be implemented by means of materials that can be switched between low and high thermal conductivity and heat capacity states, as is the case of the azobenzene polymer [44, 45]. Under UV (375 nm) and green (530 nm) light illuminations, this light-responsive material undergoes a fully reversible transition of its thermal properties that occurs in a few seconds at room temperature [44]. The periodic illumination with UV and green light of a layered system made up of azobenzene polymer layers separated by thermal insulating plates can efficiently be used to generate the modulation of k and C (See Supplemental Material at [46] for details.). k and C can then be written as [28, 39]

$$k(x - vt) = k_0 [1 + \Delta_k \cos(\sigma(x - vt))], \quad (3a)$$

$$C(x - vt) = C_0 [1 + \Delta_c \cos(\sigma(x - vt + \varphi))], \quad (3b)$$

where $\sigma = 2\pi/a$, k_0 and C_0 are the respective thermal conductivity and volumetric heat capacity in absence of modulation, Δ_k and Δ_c are the modulation amplitudes of k and C , and φ is a phase shift that we introduce to tune the thermal response and rectification factor of the proposed diode, as shown below. Given that the Eq. (2) is a partial differential equation with oscillatory coefficients, it can be replaced by a homogenized differential equation with constant coefficients, as established by the homogenization theory of differential equations [43]. When the spatial variations of the temperature field are larger than the period a of k and C , the average temperature $\bar{T}$ and heat flux $\bar{q}$ are given by [46]

$$\frac{\partial^2 \bar{T}}{\partial x^2} = \frac{1}{\alpha} \frac{\partial \bar{T}}{\partial t} + \frac{1}{L} \frac{\partial \bar{T}}{\partial x} + \frac{1}{V} \frac{\partial^2 \bar{T}}{\partial x \partial t}, \quad (4a)$$

$$\bar{q} = -k^* \left(\frac{\partial \bar{T}}{\partial x} + \frac{1}{2V} \frac{\partial \bar{T}}{\partial t} \right), \quad (4b)$$

where the effective thermal conductivity k^* and thermal diffusivity α along with the characteristic length L and speed V are defined as follows

$$k^* = k_0 \left(1 - \frac{0.5\Delta_k^2}{1 + \Gamma^2} \right), \quad (5a)$$

$$\alpha^{-1} = \frac{1}{\alpha_0} \frac{1 + \Gamma^2 - 0.5(\Delta_c \Gamma)^2}{1 + \Gamma^2 - 0.5\Delta_k^2}, \quad (5b)$$

$$L^{-1} = \frac{\sigma \Delta_k \Delta_c}{2} \frac{\Gamma [\cos(\varphi) + \Gamma \sin(\varphi)]}{1 + \Gamma^2 - 0.5\Delta_k^2}, \quad (5c)$$

$$V^{-1} = \frac{\Delta_k \Delta_c}{\sigma \alpha_0} \frac{\sin(\varphi) + \Gamma \cos(\varphi)}{1 + \Gamma^2 - 0.5\Delta_k^2}, \quad (5d)$$

with $\Gamma = vC_0/\sigma k_0 = v/\sigma \alpha_0$ and $\alpha_0 = k_0/C_0$ being the normalized speed of modulation and intrinsic thermal diffusivity of the considered material, respectively. Equation (4a) establishes that the averaged temperature is driven by a conduction-convection-like equation with an additional term (V^{-1}) analogous to the Willis coefficient found in elastodynamics of inhomogeneous media

[47, 48]. According to Eqs. (4a) and (4b), this term is relevant to the transient (thermal wave) heat conduction regime considered in this work and appears due to the spatiotemporal modulation of both k and C , as indicated in Eq. (5d). Note that $\bar{q}$ involves not only a spatial derivative of temperature, as is the case of the Fourier's law, but also a time derivative, which gives birth to interesting thermal phenomena. In the absence of modulation ($\Delta_k = \Delta_c = 0 = \Gamma$), $k = k_0$, $\alpha = \alpha_0$, $L \rightarrow \infty$, $V \rightarrow \infty$ and Eqs. (4a) and (4b) reduce to their standard counterparts, as expected. In the presence of modulation, k^* and α are both independent of φ and even functions of Γ , which means that reversing the direction of the modulation has no effect on their values. By contrast, the dependence of L and V on Γ is driven by φ . For instance, when $\varphi = 0$, both L and V are odd functions of Γ , while they become even ones of Γ for $\varphi = \pi/2$. The nonreciprocal thermal response of the material can thus be activated, nullified or tuned by means of the characteristic length and speed with $\varphi = 0$, $\varphi = \pi/2$ or $0 < \varphi < \pi/2$, respectively. Note that the reciprocity is recovered not only in absence of the traveling modulation ($\Gamma = 0$), but also for very high speeds ($\Gamma \rightarrow \pm\infty$). In this latter case, the oscillations of $k = k(x - vt)$ and $C = C(x - vt)$ are so fast that their spatial variations tend to disappear and hence their spatiotemporal modulation reduces to a temporal one. This is the reason why the modulation effect appears (disappears) on the effective thermal diffusivity $\alpha = \alpha_0 / (1 - 0.5\Delta_c^2)$ (conductivity $k^* = k_0$) that drives the time (spatial) variations of temperature, as established by Eq. (4a) (Eq. (4b)). It is thus clear that there exists an optimal speed (Γ value) that maximizes the material nonreciprocity, as shown below. Note that the coefficient (L^{-1}) of the convective term in Eq. (4a) is generated by the coupling between the spatiotemporal modulation of k and C , which indicates that this term of dynamical origin (via C) has a direct impact on the average temperature $\bar{T}$, even under steady-state conditions, as predicted by Eq. (4a).

Taking into account that the operation of the thermal wave diode depicted in Fig. (1) is driven by the temperature difference $T_h - T_c + \delta T \text{Re}(e^{i\omega t})$ modulated in time and that Eq. (4a) is a linear differential equation, the general solutions for $\bar{T}$ and $\bar{q}$ have the following forms

$$\bar{T}(x, t) = \psi(x) + \text{Re}(\theta(x) e^{i\omega t}), \quad (6a)$$

$$\bar{q}(x, t) = Q_{ss}(x) + \text{Re}(Q(x) e^{i\omega t}), \quad (6b)$$

where the steady-state (ψ, Q_{ss}) and modulated (θ, Q) components are associated to $T_h - T_c$ and δT , respectively. In practice, the temperature oscillations of the hotter thermal bath can be set with a Peltier cell, while the other bath is kept at constant temperature with a second Peltier cell. These cells typically operate with a resolution better than 0.1 K and modulation frequencies from 0.1 to 100 Hz [49]. According to Fig. (1),

($\psi(0), \psi(d)$) = (T_h, T_c) and ($\theta(0), \theta(d)$) = ($\delta T, 0$), for the forward configuration, while for the backward one, ($\psi(0), \psi(d)$) = (T_c, T_h) and ($\theta(0), \theta(d)$) = ($0, \delta T$). After inserting Eq. (6a) into Eq. (4a), one obtains ordinary differential equations for ψ and θ , whose solutions for the two diode configurations are

$$\psi_F(x) = \frac{T_h e^{d/L} - T_c - (T_h - T_c) e^{x/L}}{e^{d/L} - 1}, \quad (7a)$$

$$\psi_B(x) = \frac{T_c e^{d/L} - T_h + (T_h - T_c) e^{x/L}}{e^{d/L} - 1}, \quad (7b)$$

$$\theta_F(x) = \delta T \frac{e^{-(d-x)\sigma_-} - e^{-(d-x)\sigma_+}}{e^{-d\sigma_-} - e^{-d\sigma_+}}, \quad (7c)$$

$$\theta_B(x) = \delta T \frac{e^{x\sigma_+} - e^{x\sigma_-}}{e^{d\sigma_+} - e^{d\sigma_-}}, \quad (7d)$$

where the wavenumbers $\sigma_{\pm} = 1/2L \pm \chi_{\pm} + i(1/r \pm \chi_{\pm})$ are determined by the three lengths L , $r = 2V/\omega$ and $\mu = \sqrt{2\alpha/\omega}$ involved in $\chi_{\pm} = \sqrt{\sqrt{y^2 + z^2} \pm y}$, being $y = 0.5((2L)^{-2} - r^{-2})$ and $z = \mu^{-2} + 1/2rL$. Furthermore, according to Eqs. (4b), (6b) and (7), the steady-state ($Q_{ss} = -k^* d\psi/dx$) and modulated ($Q = -k^* (d\theta/dx + i\theta/r)$) components of the heat flux read

$$Q_{ss,F} = -Q_{ss,B} = k^* \frac{(T_h - T_c)}{L} \frac{e^{x/L}}{e^{d/L} - 1}, \quad (8a)$$

$$\frac{Q_F}{k^* \delta T} = \frac{(\sigma_+ + i/r) e^{-(d-x)\sigma_+} - (\sigma_- + i/r) e^{-(d-x)\sigma_-}}{e^{-d\sigma_-} - e^{-d\sigma_+}}, \quad (8b)$$

$$\frac{Q_B}{k^* \delta T} = \frac{(\sigma_- + i/r) e^{x\sigma_-} - (\sigma_+ + i/r) e^{x\sigma_+}}{e^{d\sigma_+} - e^{d\sigma_-}}. \quad (8c)$$

The exponential dependence on position of the temperatures in Eqs. (7a) and (7b) reduces to the usual linear one for $d \ll L$. The steady-state heat fluxes in Eq. (8a), on the other hand, depends on position due to the spatiotemporal modulation of k , such that they reduce to their usual constant expression ($Q_{ss,F} = -Q_{ss,B} = k^* (T_h - T_c)/d$) in absence of modulation ($L \rightarrow \infty$), as expected. Note that $Q_{ss,F}$ and $Q_{ss,B}$ are different at an equivalent position with respect to the modulated thermal excitation (x for $Q_{ss,F}$ and $d - x$ for $Q_{ss,B}$), and hence, according to Eqs. (1) and (8a), the rectification factor of the steady-state heat fluxes is given by

$$R = 1 - e^{-d/L}. \quad (9)$$

Equation (9) is consistent with the result obtained by Torrent *et al.* [39], for a pure steady-state problem, and shows that for a given material length d , the optimal rectification factor is given by the maximum of L^{-1} [46]: $(L^{-1})_{\max} = (\sigma \Delta_k \Delta_c / 4) \left(\sin(\varphi) + \sqrt{\sin^2(\varphi) + \lambda^{-1} \cos^2(\varphi)} \right)$, with $\lambda = 1 - 0.5\Delta_k^2$. This latter expression thus confirms that

the rectification of the steady-state heat fluxes can be tuned with the phase shift φ and increases with the spatiotemporal variation factor $\Delta_k \Delta_c$ of both the thermal conductivity and volumetric heat capacity.

The modulated temperature and heat flux profiles are thermal waves whose spatial attenuation and propagation are respectively determined by the real and imaginary parts of the wavenumbers $\sigma_{\pm}$, as established by Eqs. (7c), (7d), (8b) and (8c). In the limit of no spatiotemporal variations ($\Delta_k = \Delta_c = 0 = \Gamma$), these wavenumbers reduce to $\sigma_{\pm} = \pm(1+i)/\mu_0$, which are their standard expressions with $\mu_0 = \sqrt{2\alpha_0/\omega}$ being the classical diffusion length of the thermal waves propagating along the $\mp x$ directions [42]. In presence of the spatiotemporal modulation, Eqs. (6)-(8) establish that the thermal waves in the forward and backward configurations are driven by $\exp[x\sigma_{\pm}] = \exp[x(1/2L \pm \chi_{\pm}) + i(\omega t + x(1/r \pm \chi_{\pm}))]$, which indicates that σ_{+} (σ_{-}) is related to a wave propagating in the $-x$ ($+x$) direction, given that $1/r < \chi_{-}$. For both configurations, the propagation length of the thermal waves depends on the direction and is defined by $\Lambda_{\pm} = (\chi_{\pm} \pm 1/2L)^{-1}$. As χ_{+} and L are, in general, not even functions of the normalized speed Γ , this latter relation establishes that the propagation of the thermal waves can be tuned by changing the direction of the thermal properties' modulation, that is to say, by replacing Γ by $-\Gamma$. The propagation length Λ_{-} (Λ_{+}) is typically greater (smaller) than the diffusion length μ_0 , such that its maximum (minimum) value shows up at a speed Γ that increases with the phase shift φ , as shown in Fig. 2(a). Calculations in this and other figures were done for the typical amplitudes [28, 39] $\Delta_k = 2\Delta_c = 2/3$ and $d = 5a$. The fact that $\Lambda_{-} > d$ and $\Lambda_{+} < d$ indicates that the thermal wave energy in both configurations is mainly determined by the thermal waves propagating in the direction parallel to the wave-like modulation of the material thermal properties. At very low speeds ($\Gamma \ll 0$), the modulation effect disappears and both propagation lengths reduce to the standard diffusion length of thermal waves ($\Lambda_{\pm} = \mu_0$), as shown by the dashed line in Fig. 2(a). For $f = f_c$, $\mu_0 = d\sqrt{1-0.5\Delta_k^2} < d$ and hence the $\Lambda_{\pm}/d$ converges to values smaller than unity for $\Gamma \rightarrow 0$. More importantly, the fact that $\Lambda_{+} \neq \Lambda_{-}$, for $\Gamma > 0$, induces deviations from the mirror-like behavior of the temperature profiles around $x = 5a/2 = d/2$ and $\theta_n = \delta T/2$, as shown in Fig. 2(b) for the forward ($n = F$) and backward ($n = B$) configurations. This asymmetrical behavior of θ_n is expected to give rise to the rectification effect of the thermal wave heat fluxes.

Based on the amplitudes of the thermal wave heat fluxes, Eq. (1) takes the form $R = 1 - |Q_B(0)|/|Q_F(d)|$, which exactly reduces to Eq. (9), as established by Eqs. (8b) and (8c). This indicates that the rectification of the heat fluxes at the arrival positions ($x = d$ for Q_F and $x = 0$ for Q_B) is independent of the modulation frequency and its maximum occurs at the highest value of L^{-1} , as is the case of the rectification factor of the

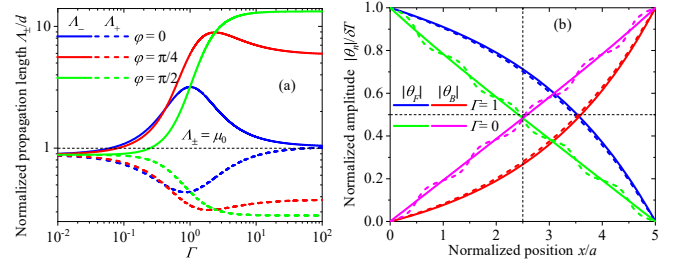


FIG. 2: Propagation length of a thermal wave propagating in the $+x$ (Λ_{+}) and $-x$ (Λ_{-}) directions as a function of the normalized speed Γ , for three representative phase shifts. (b) Amplitude profiles of the temperature field for the forward and backward configurations. Calculations were done for $f = f_c = \alpha_0/\pi d^2$ and the dashed lines in (b) represent the numerical solution of Eq. (2) obtained through the finite difference method (FDM)[46].

steady-state heat fluxes. By contrast, in terms of the amplitudes of the heat fluxes at the excitation (departure) positions, the rectification factor in Eq. (1) reads $R_d = 1 - |Q_B(d)|/|Q_F(0)|$, which in combination with Eqs. (8b) and (8c), yields

$$R_d = 1 - \frac{(1/2L + 2i/r) \tanh[(\chi_{+} + i\chi_{-})d] - (\chi_{+} + i\chi_{-})}{(1/2L + 2i/r) \tanh[(\chi_{+} + i\chi_{-})d] + (\chi_{+} + i\chi_{-})}. \quad (10)$$

Taking into account the proportionality of L^{-1} and r^{-1} to the product $\Delta_k \Delta_c$, Eq. (9) establishes that the rectification ($R > 0$) of the thermal wave heat fluxes is generated by the simultaneous spatiotemporal modulation of both k and C , such that it disappears in absence of any of them ($R = 0$ for $\Delta_k \Delta_c = 0$). In the low-frequency limit ($f = \omega/2\pi \ll f_c = \alpha_0/\pi d^2$), Eq. (10) reduces to Eq. (9), as expected for the steady-state regime.

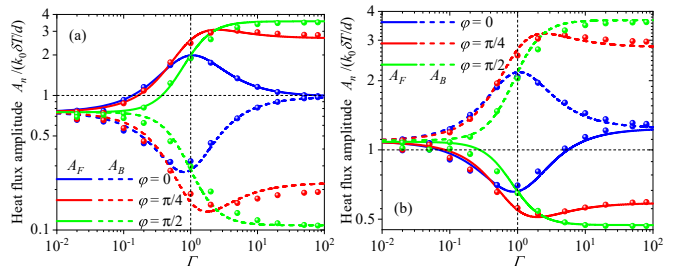


FIG. 3: Speed Γ dependence of the heat flux amplitudes at the (a) arrival and (b) departure positions for the forward and backward configurations. Calculations were done for $f = f_c$ and three representative phase shifts. Points represent the numerical solution of Eq. (2) obtained by FDM[46].

The analytical predictions of Eqs. (8b) and (8c) for the heat flux amplitudes at the arrival and departure positions are in good agreement with their correspond-

ing numerical counterparts, as shown in Figs. 3(a) and 3(b), respectively. Note that, at the arrival position $x = d$ ($x = 0$), the amplitude A_F (A_B) follows the behavior of Λ_- (Λ_+), as shown in Fig. 2(a). The opposite applies for the amplitudes at the departure positions, as shown in Fig. 3(b). For both positions, there exists an optimal normalized speed $\Gamma_{\text{opt}} \gtrsim 1$ that increases with the phase shift φ , for which the amplitude difference $|A_F - A_B|$ takes its highest value. This indicates that the rectification factor is maximized at $\Gamma_{\text{opt}} = \lambda \tan(\varphi) + \lambda \sqrt{\tan^2(\varphi) + \lambda^{-1}}$, as predicted by Eq. (9) and is shown in Fig. 4(a) for the rectification of the heat fluxes at the arrival positions. For the departure positions, on the other hand, the rectification factor R_d exhibits a similar dependence on Γ than R , however its values decrease as the thermal wave frequency increases, as displayed in Fig. 4(b). When φ is changed from 0 to $\pi/2$, R_d takes lower values for $\Gamma = 0.1$, equal values for $\Gamma = 1$, and higher values for $\Gamma = 10$. The fact that the same propagation lengths (Fig. 2(a)), heat fluxes (Fig. 3) and rectification factors (Fig. 4(a)) can be obtained by different sets of values of Γ and φ is because of the dependences of L and V on Γ are driven by the particular values of φ . This phase shift thus provides a degree of freedom to optimize the diode rectification factor.

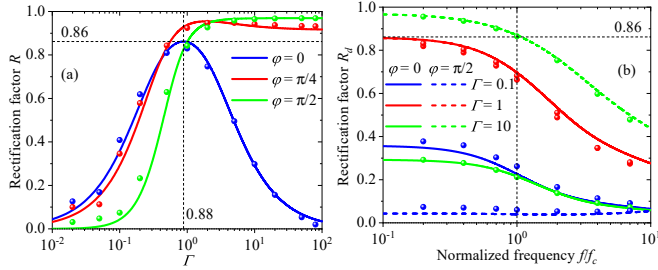


FIG. 4: Rectification factors for the heat fluxes carried by thermal waves at the (a) arrival and (b) departure positions, as functions of the normalized speed and frequency, respectively. Points represent the numerical solution of Eq. (2) obtained by FDM[46].

In summary, the proof of principle of a thermal wave diode has been demonstrated by exploiting the spatiotemporal modulation of the thermal conductivity and volumetric heat capacity in a wave-like fashion. This has been done by deriving explicit expressions for the average temperature and heat flux carried by the thermal waves propagating in the forward and backward configurations of the diode. It has been shown that the rectification effect is generated by the simultaneous spatiotemporal variations of both the heat capacity and thermal conductivity, such that their modulation speed and phase difference drive the diode rectification factor. The highest rectification factor, greater than 86%, is reached at low modulation frequencies and an optimal speed that increases with the phase shift. Considering the unique

features of the proposed thermal wave diode, the developed theory and our findings can open research avenues in thermal computing, unconventional thermal phenomena, and material science.

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