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# Sub-diffraction-limit imaging system with two interfacing hyperbolic metamaterials

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It is demonstrated that a system of two interfacing hyperbolic metamaterials may be used for direct subwavelength imaging in the visible range. The proposed configuration consists of two anisotropic photonic crystals: a multilayered metal-dielectric structure and an adjoined wired structure. The analytical calculations and numerical modeling show results that the light emitted by a dipole placed on the top of the multilayered structure propagates within a narrow cone along the direction  $\mathbf{n}$ , where  $\text{Re} \varepsilon(\omega, \mathbf{n}) = 0$ . Due to impedance matching and negative refraction at the interface, a bright image with a maximum transverse size of  $\sim 50$  nm is focused in the wired structure at the wavelength  $\lambda = 670$  nm.

## I. INTRODUCTION

A perfect flat lens proposed by Veselago<sup>1</sup> and mathematically justified by Pendry<sup>2</sup> consists of a slab of metamaterial with  $n = -1$  surrounded by a medium with  $n = 1$ . It can produce an ideal image since it collects all propagating and evanescent waves emitted by a source and transfers them to the image without losses due to perfectly matching layers. Dispersion and absorption in real materials place a natural limit for the resolution<sup>3</sup> that makes the concept of perfect lens flawed. Nevertheless, a negative refractive index slab serves as a flat superlens breaking the subwavelength limit in optics<sup>4-6</sup>. Recently, a Veselago flat lens was experimentally realized in microwave region<sup>7</sup>, where negative refractive index  $n = -1$  was obtained with a slab of Weyl metacryystal.

Imaging in the far-field with subwavelength resolution requires transformation of evanescent modes radiated by an object in the near-field to propagating waves. This transformation was achieved by introducing a multilayered cylindrical,<sup>8-10</sup> or spherical<sup>11</sup> stack of hyperbolic metamaterial (HMM) into a projecting device. Application of HMM in optical devices allows realization of subwavelength interference pattern from multilayered slab<sup>12</sup> or array of metallic nanowires in dielectric<sup>13</sup>. While these studies demonstrate a possibility of manipulating with light patterns at subwavelength scales, they do not consider a question about imaging of an object at the focal plane. Two slit interference was applied for subwavelength photolithography for gratings fabrication<sup>12</sup>. Here we propose a structure of two planar HMMs that allows subwavelength imaging of light source. This focusing system allows photolithography of any image produced in the focus plane. Due to hyperbolic dispersion, the emitted light propagates in each HMM along narrow epsilon-near-zero channels, suffering negative refraction at the interface. However, the effects of dispersion and dissipation in the metallic constituents of the struc-

ture are explicitly taken into account. The parameters of the HMMs media are selected to satisfy the matching of impedances at the interface that strongly reduces losses at reflection. As a result, the record-high transmission is numerically achieved for silver-aluminum and silver-silica constituents allowing bright image with subwavelength resolution exceeding the values reported in the modern literature. Specifically, we got the focal spot size to wavelength ratio  $l/\lambda = 0.075$  versus the values 0.41, 0.37 reported in Refs. [10,11] respectively.

## II. IMAGING SYSTEM DESIGN

There are two types of hyperbolic media within the class of uniaxial optical crystals. For type I the isofrequency surfaces are of two sheets hyperboloids, and for type II they are of one sheet hyperboloids, schematically shown in Fig. 1. The optical axis is along axis  $z$  with the corresponding component of permittivity tensor  $\varepsilon_z = \varepsilon_{\parallel}$ . In the  $x - y$  plane the crystal is isotropic with  $\varepsilon_x = \varepsilon_y = \varepsilon_{\perp}$ .

In type I HMM the metallic properties dominate along axis  $z$ , therefore  $\varepsilon_{\parallel} < 0$  and  $\varepsilon_{\perp} > 0$ . The dispersion of the extraordinary wave is given by

$$\frac{k_x^2 + k_y^2}{|\varepsilon_{\parallel}|} - \frac{k_z^2}{\varepsilon_{\perp}} = -\frac{\omega^2}{c^2}. \quad (1)$$

In type II HMM metal conductivity dominates in the  $x - y$  plane, i.e.,  $\varepsilon_{\parallel} > 0$  and  $\varepsilon_{\perp} < 0$ . The dispersion relation for extraordinary wave is

$$\frac{k_x^2 + k_y^2}{\varepsilon_{\parallel}} - \frac{k_z^2}{|\varepsilon_{\perp}|} = \frac{\omega^2}{c^2}. \quad (2)$$

The ordinary wave propagates in a uniaxial crystal like in an isotropic medium with refractive index  $\sqrt{|\varepsilon_{\perp}|}$ .

Let us consider the refraction of an extraordinary plane wave at the horizontal interface  $z = 0$  between two hyperbolic media. Let the region  $z > 0$  is filled by type II

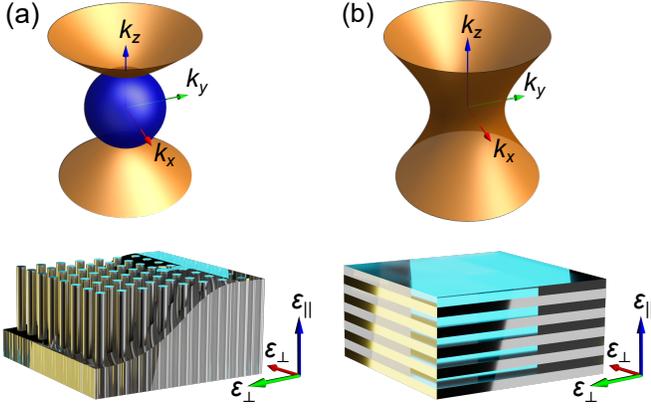


FIG. 1: **Two isofrequency surfaces of extraordinary wave with hyperbolic dispersion.** (a) Hyperboloid of two sheets corresponds to type I HMM. Can be realized as a photonic crystal of metallic rods in dielectric matrix. Blue sphere is an isofrequency surface of ordinary wave. (b) Hyperboloid of one sheet corresponds to type II HMM. Can be realized as a superlattice of metal and dielectric layers.

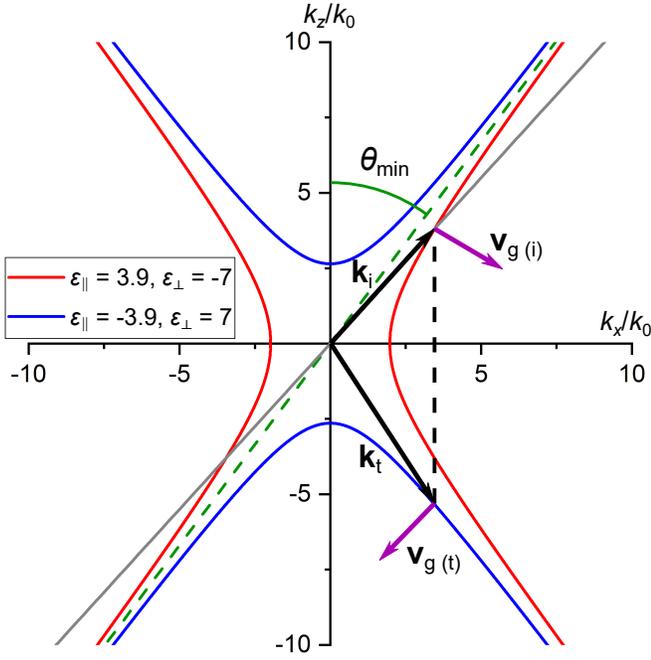


FIG. 2: **Scheme of negative refraction at the interface between two hyperbolic media.** The incident plane wave, characterized by wave vector  $\mathbf{k}_i$  and group velocity  $\mathbf{v}_{g(i)}$ , comes from type II HMM ( $z > 0$ ) with  $\epsilon_{\parallel} = 3.9$ ,  $\epsilon_{\perp} = -7$ . Red hyperbola shows dispersion in this medium given by Eq. (2), where  $k_0 = \omega/c$ . After negative refraction at the interface  $z = 0$ , the plane wave is transmitted to type I HMM ( $z < 0$ ) with  $\epsilon_{\parallel} = -3.9$ ,  $\epsilon_{\perp} = 7$  with dispersion shown by blue hyperbola, Eq. (1). The transmitted wave has the wave vector  $\mathbf{k}_t$  and group velocity  $\mathbf{v}_{g(t)}$ .

HMM with  $\epsilon_{\parallel} = 3.9$  and  $\epsilon_{\perp} = -7$  and the lower semi-space  $z < 0$  is filled by type I HMM with  $\epsilon_{\parallel} = -3.9$  and  $\epsilon_{\perp} = 7$ . The dielectric properties of the upper and lower media are mutually "conjugated" in order to minimize the reflection losses, as shown below.

The dispersion relations for these HMMs are given in Fig. 2 by red (HMM II) and blue (HMM I) hyperbolas. The wave vector  $\mathbf{k}_i$  in the incoming wave has components ( $k_{x(i)} > 0, k_{z(i)} > 0$ ). For this wave vector the group velocity  $\mathbf{v}_{g(i)} = \nabla\omega(\mathbf{k})|_{\mathbf{k}=\mathbf{k}_i}$  has a negative vertical projection that corresponds to energy propagation towards the interface. While the vertical component of  $\mathbf{k}_i$  is positive, i.e. the phase grows outward the interface, this wave transfers energy from upper to lower semi-space. A backward propagation regime is typical for waves in HMMs when phase and group velocities have opposite projections<sup>14</sup>.

The wave vector  $\mathbf{k}_t$  of the transmitted wave is obtained from the momentum conservation,  $k_{x(i)} = k_{x(t)}$ . From two points on the blue hyperbola, satisfying this conservation law, the one on the low branch corresponds to the refracted wave, since here the vertical projection of group velocity is negative.

Mutual orientation of the vectors of group velocities in the incident and refracted wave in Fig. 2 is a signature of negative refraction at the interface between two HMMs of different types. Here we show that due to negative refraction at the interface between two weakly absorbing HMMs a real subwavelength image is formed by converging rays, similarly to an image obtained with ideal Pendry's flat lens.

It follows from the plot in Fig. 2 that the incoming wave is a propagating mode if the angle of incidence  $\theta$  exceeds the critical value  $\theta_{min} = \arctan\sqrt{|\epsilon_{\parallel}/\epsilon_{\perp}|} = \arctan(\sqrt{3.9/7})$ . Here the angle  $\theta_{min}$  defines the hyperbola's asymptote  $k_z = \sqrt{|\epsilon_{\perp}/\epsilon_{\parallel}|} k_x$ .

We briefly remind the fundamental properties of monochromatic plane wave propagating in a medium with uniaxial anisotropy and hyperbolic dispersion. It follows from Maxwell's equations

$$(\omega/c)\mathbf{H} = \mathbf{k} \times \mathbf{E}, \quad (\omega/c)\mathbf{D} = -\mathbf{k} \times \mathbf{H} \quad (3)$$

that the mutual orientation of the vectors  $\mathbf{k}$ ,  $\mathbf{E}$ ,  $\mathbf{D}$ ,  $\mathbf{H}$ , and the Poynting vector  $\mathbf{S} = \frac{c}{4\pi}(\mathbf{E} \times \mathbf{H})$  is as shown in Fig. 3a. The four vectors,  $\mathbf{k}$ ,  $\mathbf{E}$ ,  $\mathbf{D}$ ,  $\mathbf{S}$  are coplanar since each of them is orthogonal to  $\mathbf{H}$ . The optical axis also lies in the same plane. The direction of propagation of electromagnetic energy is defined by the vector of group velocity  $\mathbf{v}_g = \partial\omega(\mathbf{k})/\partial\mathbf{k}$ , which coincides with the direction of the Poynting's vector  $\mathbf{S}$  for a transparent (or weakly absorbing) media.

For the extraordinary wave the length of the wave vector  $k = (\omega/c)\sqrt{\epsilon(\theta)}$  depends on the angle  $\theta$  it makes with the optical axis, where angular dependence of the dielectric constant is given by the equation<sup>15</sup>

$$\frac{1}{\epsilon(\theta)} = \frac{\sin^2\theta}{\epsilon_{\parallel}} + \frac{\cos^2\theta}{\epsilon_{\perp}}. \quad (4)$$

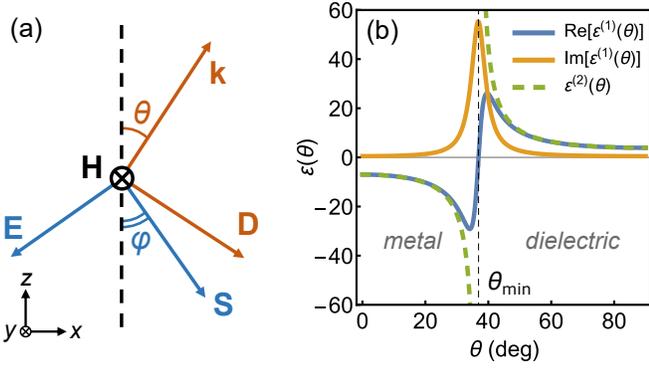


FIG. 3: a) Mutual orientation of the vectors in a plane wave propagating in a uniaxial crystal with optical axis along dashed line. Pairs of orthogonal vectors are marked by the same color. The direction of Poynting's vector  $\mathbf{S}$  corresponds to a medium with hyperbolic dispersion, as it follows from the direction of group velocity  $\mathbf{v}_{g(i)}$  in Fig. 2. Angles  $\theta$  and  $\varphi$  are related,  $\tan \varphi = \text{Re} \left( \frac{\varepsilon_{\perp}}{\varepsilon_{\parallel}} \right) \tan \theta$ .<sup>15</sup> b) Angular dependence of the dielectric permittivity in a dissipative hyperbolic medium with  $\varepsilon_{\perp}^{(1)} = -7 + i0.5$ ,  $\varepsilon_{\parallel}^{(1)} = 3.9 + i0.5$  and in a dissipationless one with  $\varepsilon_{\perp}^{(2)} = -7$ ,  $\varepsilon_{\parallel}^{(2)} = 3.9$ .

In a dissipationless type II HMM ( $\varepsilon_{\parallel} > 0$ ,  $\varepsilon_{\perp} < 0$ ) the dependence  $\varepsilon(\theta)$  has a point of singularity at  $\theta = \theta_{min}$  where  $\varepsilon(\theta_{min}) = \infty$ . At this point the function  $\varepsilon(\theta)$  changes its sign suffering an infinite discontinuity, see the green line in Fig. 3b. Dissipation removes this singularity. The real part of  $\varepsilon(\theta)$  changes its sign passing through zero, as shown by the blue line. In this case the angle  $\theta_{min}$  obtained from the equation  $\text{Re} \varepsilon(\theta) = 0$  is shifted by  $-\frac{\delta^2}{2} \frac{\varepsilon_{\parallel} - |\varepsilon_{\perp}|}{(\varepsilon_{\parallel} |\varepsilon_{\perp}|)^{3/2}}$  from the angle  $\arctan(\sqrt{|\varepsilon_{\parallel}|/|\varepsilon_{\perp}|})$ , where  $\delta = \text{Im} \varepsilon_{\perp} = \text{Im} \varepsilon_{\parallel}$ .

The line  $\theta = \theta_{min}$  divides space into two parts with metallic ( $\text{Re} \varepsilon(\theta) < 0$ ) and dielectric ( $\text{Re} \varepsilon(\theta) > 0$ ) response. It is known that surface plasmon-polariton is an eigenmode propagating along metal-dielectric interface<sup>15</sup>. Since the virtual boundary  $\theta = \theta_{min}$  separates metal region from dielectric region, a bulk plasmon-polariton mode, may propagate along it<sup>16,17</sup>. This mode is tightly localized and it serves as a carrier of the sub-wavelength image.

### III. SUBWAVELENGTH IMAGE OBTAINED FOR TWO HOMOGENEOUS HYPERBOLIC MEDIA

Let us consider two semi-infinite, homogeneous, hyperbolic media with interface at  $z = 0$ . The upper medium (a) is the type II HMM with  $\text{Re} \varepsilon_{\parallel}^a > 0$ ,  $\text{Re} \varepsilon_{\perp}^a < 0$ . The low medium (b) is the type I HMM with  $\text{Re} \varepsilon_{\parallel}^b < 0$ ,  $\text{Re} \varepsilon_{\perp}^b > 0$ . The optical axis in each medium coincides with axis  $z$ . The light source is a point dipole oriented perpendicular to axis  $z$  placed in the upper medium at

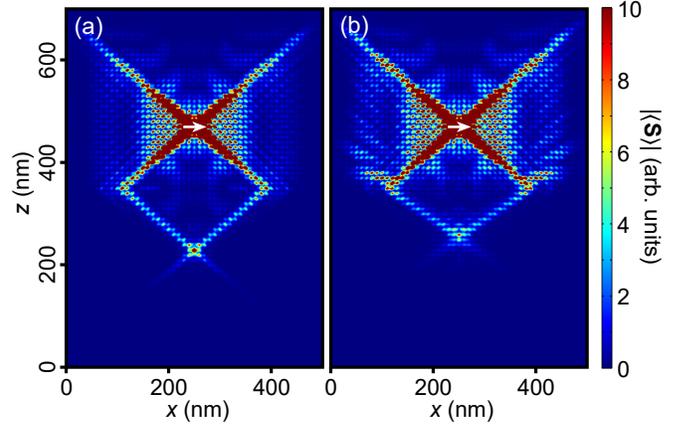


FIG. 4: Near-field subwavelength image of a point dipole (shown by white arrow) with  $\lambda = 670$  nm obtained by negative refraction at the interface between two HMM's. Color map shows spatial distribution of Poynting's vector. (a) The HMM's satisfy the condition (9) of minimum reflection:  $\varepsilon_{\parallel}^a = 3.9$ ,  $\varepsilon_{\perp}^a = -7 + 0.18i$ ,  $\varepsilon_{\parallel}^b = -3.9 + 0.18i$ , and  $\varepsilon_{\perp}^b = 7 + 0.26i$ . (b) Less dissipative HMM's with parameters not matching the condition of minimum reflection:  $\varepsilon_{\parallel}^a = 4$ ,  $\varepsilon_{\perp}^a = -7 + 0.1i$ ,  $\varepsilon_{\parallel}^b = -2 + 0.1i$ , and  $\varepsilon_{\perp}^b = 9 + 0.1i$ .

120 nm above the interface, as shown in Fig. 4. The dipole radiates at the wavelength  $\lambda = 670$  nm. Its image with subwavelength resolution is formed in the near-field zone.

The parameters of the hyperbolic media must be optimized to minimize reflection losses for the extraordinary (TM) wave. While the field emitted by the dipole also contains the TE mode (with electric field parallel to the interface), it does not propagate in the upper medium where  $\varepsilon_{\perp}^a < 0$ . The fields of the incident TM wave propagating in the upper medium are oriented as shown in Fig. 3a. The fields of the reflected wave and refracted wave are calculated from the electrodynamics boundary conditions. The details of calculation are given in Appendix. The following formula gives the reflection coefficient defined as  $R = |H_r|^2/|H_i|^2$ :

$$R(\theta) = \left| \frac{\cos \theta \sqrt{\varepsilon_{\perp}^b \varepsilon^a(\theta)} + \varepsilon_{\perp}^a \sqrt{1 - \frac{\varepsilon^a(\theta)}{\varepsilon_{\parallel}^a} \sin^2 \theta}}{\cos \theta \sqrt{\varepsilon_{\perp}^b \varepsilon^a(\theta)} - \varepsilon_{\perp}^a \sqrt{1 - \frac{\varepsilon^a(\theta)}{\varepsilon_{\parallel}^a} \sin^2 \theta}} \right|^2. \quad (5)$$

Here  $\varepsilon^a(\theta) = \varepsilon_{\parallel}^a |\varepsilon_{\perp}^a| / (|\varepsilon_{\perp}^a| \sin^2 \theta - \varepsilon_{\parallel}^a \cos^2 \theta)$  is the angular dependence of permittivity in medium  $a$  given by Eq. (4). Note that for  $\theta > \theta_{min}$  the function  $\varepsilon^a(\theta)$  takes only positive values.

The condition of total transmission,  $R(\theta) = 0$  is satisfied if

$$\cos \theta \sqrt{\varepsilon_{\perp}^b \varepsilon^a(\theta)} + \varepsilon_{\perp}^a \sqrt{1 - \frac{\varepsilon^a(\theta)}{\varepsilon_{\parallel}^a} \sin^2 \theta} = 0. \quad (6)$$

If the dielectric constants of both hyperbolic media are

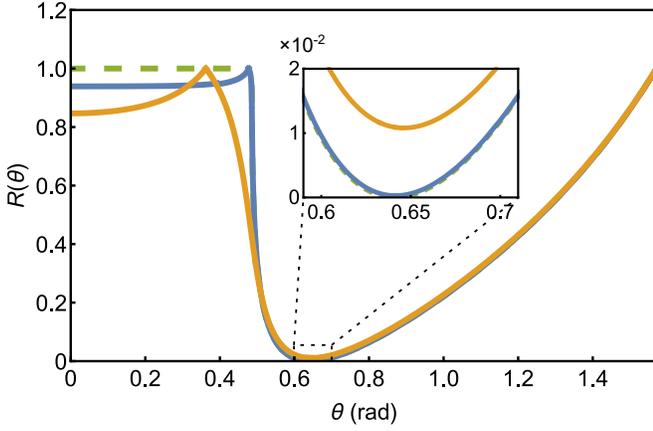


FIG. 5: Reflection coefficient vs angle of incidence. Green line is for nondissipative media:  $\varepsilon_{\parallel}^a = 3.9$ ,  $\varepsilon_{\perp}^a = -7$ ,  $\varepsilon_{\parallel}^b = -3.9$ , and  $\varepsilon_{\perp}^b = 7$ . Blue line is for weakly dissipative media:  $\varepsilon_{\parallel}^a = 3.9$ ,  $\varepsilon_{\perp}^a = -7 + 0.18i$ ,  $\varepsilon_{\parallel}^b = -3.9 + 0.18i$ , and  $\varepsilon_{\perp}^b = 7 + 0.26i$ . Yellow line is for moderately dissipative media:  $\varepsilon_{\parallel}^a = 3.9 + 0.5i$ ,  $\varepsilon_{\perp}^a = -7 + 0.7i$ ,  $\varepsilon_{\parallel}^b = -3.9 + 0.2i$ , and  $\varepsilon_{\perp}^b = 7 + 0.3i$ . Blowup of the region near the minimum is shown in insert.

real, this equation has the root

$$\theta_B = \arctan \left( \frac{\varepsilon_{\parallel}^a |\varepsilon_{\parallel}^b|}{|\varepsilon_{\perp}^a|^2} \cdot \frac{|\varepsilon_{\perp}^a| + \varepsilon_{\perp}^b}{\varepsilon_{\parallel}^a + |\varepsilon_{\parallel}^b|} \right)^{1/2}, \quad (7)$$

which is the Brewster angle for the interface between two uniaxial media. Note that the angle  $\theta$  defines the direction of the wave vector  $\mathbf{k}$ , which is different from the direction of Poynting vector  $\mathbf{S}$ , see Fig. 3. For two isotropic media with linear dispersion Eq. (7) is reduced to the well-known result,  $\theta_B = \arctan(\sqrt{\varepsilon^b/\varepsilon^a})$ .

If the light source is placed in the upper medium (medium (a) in Fig. 4) the emitted radiation propagates within a narrow cone<sup>20</sup> along the line  $\varphi_0$  defined from  $\tan \varphi_0 = (|\varepsilon_{\perp}^a|/\varepsilon_{\parallel}^a) \tan \theta_{min}$ , see Fig. 3. Thus, to realize the condition of minimum reflection, the angle of incidence  $\theta_{min}$  must be the Brewster angle:  $\theta_B = \theta_{min}$ . This occurs for symmetrically conjugated media, when  $\varepsilon_{\parallel}^a = |\varepsilon_{\parallel}^b|$  and  $|\varepsilon_{\perp}^a| = \varepsilon_{\perp}^b$ . Since the function  $\varepsilon^a(\theta) \rightarrow \infty$  at  $\theta \rightarrow \theta_{min}$ , the value of the reflection coefficient is calculated by L'Hôpital's rule that gives,  $\lim R(\theta)_{\theta \rightarrow \theta_{min}} = 0$ . According to Fig. 2, in a nondissipative hyperbolic medium the wave incident at  $\theta = \theta_{min}$  has  $k_i \rightarrow \infty$ . The latter means that total transmission cannot be realized at  $\theta = \theta_{min}$ . However almost total transmission occurs for the angle slightly exceeding  $\theta_{min}$  and finite wave vector, if the media are dissipative. Angular dependence of the reflection coefficient (5) is shown in Fig. 5 for dissipationless (green line), weakly dissipative (blue line), and moderately dissipative (yellow line) structures. Even in the latter case the reflection remains very weak near  $\theta_{min} = \arctan \sqrt{3.9/7} \approx 0.641 \approx 36.74^\circ$  and the minimum is slightly shifted towards larger angles.

The interface between two hyperbolic dissipationless

media remains perfectly reflective for the angles of incidence  $0 \leq \theta \leq \theta_c$ , where

$$\theta_c = \arctan \sqrt{\frac{\varepsilon_{\parallel}^a |\varepsilon_{\parallel}^b|}{|\varepsilon_{\perp}^a| (\varepsilon_{\parallel}^a + |\varepsilon_{\parallel}^b|)}} \quad (8)$$

is the root of the equation  $\varepsilon_{\parallel}^b = \varepsilon^a(\theta) \sin^2 \theta$ . For the selected parameters of the media the critical angle is  $\theta_c = \arctan \sqrt{3.9/14} \approx 0.486 \approx 27.83^\circ$ . It is shown in Appendix that at  $\theta = \theta_c$  the  $z$ -component of  $\mathbf{k}_t$  vanishes. For  $\theta \leq \theta_c$  the wave vector in medium (b) becomes pure imaginary. Since  $\theta_c < \theta_{min}$  the wave vector for the wave incident at angle  $\theta_c$  is also pure imaginary. Thus, an interesting optical phenomenon – total internal reflection of evanescent wave at the interface between two hyperbolic media occurs for  $\theta_c < \theta_{min}$ . This is the reason for  $R = 1$  at  $\theta < \theta_c$  for the green-dashed curve in Fig. 5. The dependence  $R(\theta)$  exhibits a singularity, at  $\theta = \theta_c$ , which is related to vanishing Poynting vectors in both media when  $\theta \rightarrow \theta_c$ .

At  $\theta > \theta_c$  the  $z$ -component of transmitted wave becomes real, giving rise to a sharply increasing transmission, which becomes perfect ( $R = 0$ ) at  $\theta = \theta_{min}$  due to excitation of bulk plasmon-polariton. For larger angles,  $\theta > \theta_{min}$  both media exhibit a dielectric behavior and the reflection coefficient growth, approaching 1 for  $\theta = \pi/2$ . Note that for two hyperbolic media the effect of total internal reflection takes place for small angles of incidence, unlike the same effect in dielectrics, where the angle of incidence must exceed some critical value. If both media are isotropic Eq. (8) for  $\theta_c$  is reduced to the well-known result  $\theta_c = \arcsin \sqrt{\varepsilon^b/\varepsilon^a}$ .

Finite dissipation smoothes the singularity of  $R(\theta)$  at  $\theta = \theta_c$  but the behavior of this function remain practically the same, as it is seen from the plots in Fig. 5. The minimum of reflection HMM's with conjugated parameters:

$$|\operatorname{Re} \varepsilon_{\perp}^a| = \operatorname{Re} \varepsilon_{\perp}^b, \quad \operatorname{Re} \varepsilon_{\parallel}^a = |\operatorname{Re} \varepsilon_{\parallel}^b|. \quad (9)$$

This condition is satisfied for the imaging system shown in Fig. 4a and it is broken for the system in Fig. 4b. Both figures demonstrate the distribution of Poynting's vector  $\mathbf{S}$  of a point dipole radiation obtained by Comsol Multiphysics. While the structure in Fig. 4a is more dissipative, it produces a brighter image with better resolution. Losses due to reflection at the interface seen in Fig. 4b render a more negative effect on the quality of the image than stronger dissipative losses existing in the system in Fig. 4a. The impedance matching in design of subwavelength hyperlens was achieved in Ref. [18], where image magnification was numerically realized using principles of transformation optics.

The effect of negative refraction at the interface results in the focusing of emitted radiation in the second slab, similarly to image formation in Pendry's lens. Due to two paths with equal optical length, the local field at the focus

is enhanced by constructive interference. An estimate for the characteristic size of the image is limited by the pixel size,  $\sim 10$  nm in Fig. 4. Additional calculations with the pixel size about 5 nm indicates, that the waist size at the focal point for the image in Fig. 4 does not exceed  $10 \pm 5$  nm, i.e. it lies in a deeply subwavelength range.

It is clearly seen in Fig. 4 that electromagnetic energy radiated by the dipole is concentrated asymptotically within two narrow cones along the lines separating the regions with metallic and dielectric response. While the interface is in the near zone, the tendency for concentration of energy along these lines is already clearly seen. Radiation of a dipole in an uniaxial dielectric medium was calculated in Ref. [19]. Detailed distribution of the field pattern in a homogeneous hyperbolic medium was studied in Ref. [20]. Distribution of light intensity in each half-plane in Fig. 4 coincides qualitatively with that obtained in Ref. [20] for a dipole oriented perpendicular to

the optical axis.

#### IV. EFFECTIVE PARAMETERS OF LAYERED AND WIRED STRUCTURES

Homogeneous media  $a$  with  $\varepsilon_{\perp}^a < 0$ ,  $\varepsilon_{\parallel}^a > 0$  and  $b$  with  $\varepsilon_{\perp}^b > 0$ ,  $\varepsilon_{\parallel}^b < 0$  can be considered as long-wavelength limits of periodic layered and wired structure respectively. Their dielectric properties in the homogenization limit can be calculated analytically. The selected layered structure consists of layers of silver with dielectric function  $\varepsilon_m(\lambda)$  and thickness  $p$  separated by layers of silicon oxide with parameters  $\varepsilon_d$  and  $q$ . In the long-wavelength limit,  $d = p + q \ll \lambda$ , where  $\lambda$  is the wavelength in vacuum, the effective dielectric function  $\varepsilon_{\parallel}^a(\lambda)$  corresponding to plasmonic-like mode is obtained from the equation<sup>21</sup>

$$\begin{aligned} & \cos\left(\frac{2\pi p}{\lambda} \sqrt{\frac{\varepsilon_m}{\varepsilon_{\parallel}^a} - 1}\right) \cos\left(\frac{2\pi q}{\lambda} \sqrt{\frac{\varepsilon_d}{\varepsilon_{\parallel}^a} - 1}\right) \\ & - \frac{1}{2} \left( \frac{\varepsilon_d}{\varepsilon_m} \sqrt{\frac{\varepsilon_m - \varepsilon_{\parallel}^a}{\varepsilon_d - \varepsilon_{\parallel}^a}} + \frac{\varepsilon_m}{\varepsilon_d} \sqrt{\frac{\varepsilon_d - \varepsilon_{\parallel}^a}{\varepsilon_m - \varepsilon_{\parallel}^a}} \right) \sin\left(\frac{2\pi p}{\lambda} \sqrt{\frac{\varepsilon_m}{\varepsilon_{\parallel}^a} - 1}\right) \sin\left(\frac{2\pi q}{\lambda} \sqrt{\frac{\varepsilon_d}{\varepsilon_{\parallel}^a} - 1}\right) = 1. \end{aligned} \quad (10)$$

The effective dielectric function  $\varepsilon_{\perp}^a(\lambda)$  is explicitly given by the following formula<sup>21</sup>:

$$\begin{aligned} \varepsilon_{\perp}^a(\lambda) &= \frac{\lambda^2}{2(\pi d)^2} \left[ 1 - \cos\left(\frac{2\pi p}{\lambda} \sqrt{\varepsilon_m}\right) \cos\left(\frac{2\pi q}{\lambda} \sqrt{\varepsilon_d}\right) \right. \\ & \left. + \frac{1}{2} \left( \sqrt{\frac{\varepsilon_m}{\varepsilon_d}} + \sqrt{\frac{\varepsilon_d}{\varepsilon_m}} \right) \sin\left(\frac{2\pi p}{\lambda} \sqrt{\varepsilon_m}\right) \sin\left(\frac{2\pi q}{\lambda} \sqrt{\varepsilon_d}\right) \right]. \end{aligned} \quad (11)$$

The wired structure of period  $d$  consists of silver cylinders of radius  $R$  imbedded in a silicon dioxide background. The effective dielectric function  $\varepsilon_{\parallel}^b$  is the weighted average of  $\varepsilon_m$  and  $\varepsilon_d$

$$\varepsilon_{\parallel}^b = f\varepsilon_m + (1-f)\varepsilon_d, \quad (12)$$

where  $f = \pi R^2/d^2$  is the filling fraction of metal. The other effective dielectric function is expressed through a series over the reciprocal lattice vectors  $\mathbf{G}^{22}$ ,

$$\varepsilon_{\perp}^b = \left\{ \bar{\eta} - \frac{1}{2} \sum_{\mathbf{G}, \mathbf{G}' \neq 0} \mathbf{G} \cdot \mathbf{G}' \eta(\mathbf{G}) \eta(-\mathbf{G}') M^{-1}(\mathbf{G}, \mathbf{G}') \right\}^{-1} \quad (13)$$

Here  $\bar{\eta} = f/\varepsilon_m + (1-f)/\varepsilon_d$  and

$$\eta(\mathbf{G}) = \frac{1}{A_c} \int_{A_c} \varepsilon^{-1}(\mathbf{r}) \exp(-i\mathbf{G} \cdot \mathbf{r}) d\mathbf{r} \quad (14)$$

is the Fourier component of periodic function  $1/\varepsilon(\mathbf{r})$ , integration runs over the unit cell with area  $A_c = d^2$ , and  $M^{-1}(\mathbf{G}, \mathbf{G}')$  is the inverse of the matrix

$$M(\mathbf{G}, \mathbf{G}') = \mathbf{G} \cdot \mathbf{G}' \eta(\mathbf{G}' - \mathbf{G}). \quad (15)$$

Using Eqs. (10)-(15) the parameters of any layered or wired nanostructure can be easily calculated. It takes some effort to optimize the parameters of the both structures to satisfy Eq. (9). The following values for the effective dielectric constants were found for the wavelength  $\lambda = 670$  nm:

$$\varepsilon_{\perp}^a = -7.05 + i0.18, \quad \varepsilon_{\parallel}^a = 3.90, \quad (16)$$

$$\varepsilon_{\perp}^b = 7.05 + i0.26, \quad \varepsilon_{\parallel}^b = -3.89 + i0.18. \quad (17)$$

These values are obtained for  $p = 4$  nm,  $q = 6$  nm ( $f = p/(p+q) = 0.4$ ),  $R = 5$  nm,  $d = 16.45$  nm ( $f = \pi R^2/d^2 = 0.29$ ). The dielectric properties of the constituents at  $\lambda = 670$  nm were collected from Ref. [23]:  $\varepsilon_{Ag} = -20.86 + i0.43$ ,  $\varepsilon_{SiO_2} = 2.18$ ,  $\varepsilon_{Al_2O_3} = 3.07 + i0.07$ . Note that the value of  $\varepsilon_{\parallel}^a$  is pure real since the corresponding imaginary part does not exceed  $10^{-2}$  and can be neglected.

For both structures the ratio  $d/\lambda \sim 10^{-2}$  corresponds to deeply subwavelength limit. Therefore, the obtained values of the effective dielectric constants are quite close to that obtained in the quasi-static limit or in Maxwell-Garnet approximation.

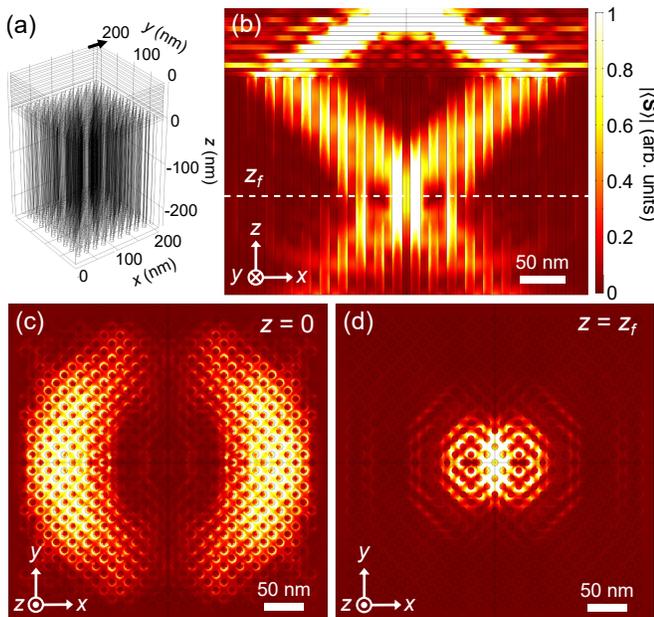


FIG. 6: a) Proposed scheme of the imaging system with layered and wired structures. Black arrow at the top corner is a dipole radiating at  $\lambda = 670$  nm; b) distribution of averaged Poynting  $|\langle \mathbf{S} \rangle|$  in the  $x-z$  plane where the dipole is displaced (at  $y = 200$  nm); c) and d) distribution of  $|\langle \mathbf{S} \rangle|$  in the  $x-y$  cross-section at the interface  $z = 0$  and at the focal plane  $z = z_f$ , respectively.

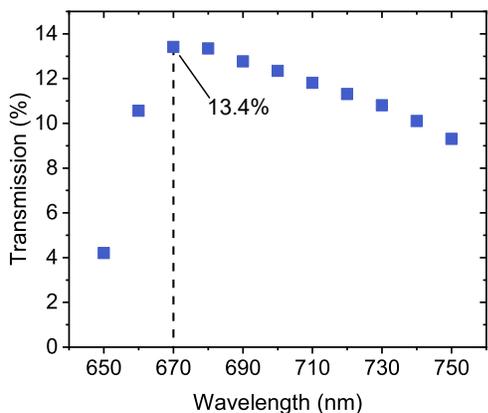


FIG. 7: Transmission of emitted light vs wavelength.

## V. SUBWAVELENGTH IMAGING WITH LAYERED AND WIRED STRUCTURES

We propose a finite size realistic imaging system with the materials and geometrical parameters mentioned above. Medium  $a$  (upper slab) contains 7 periods of Ag/SiO<sub>2</sub> bilayer with an extra layer of SiO<sub>2</sub> on the top. Medium  $b$  is a slab of photonic crystal of vertical Ag nanowires in Al<sub>2</sub>O<sub>3</sub> matrix of total thickness approximately 240 nm. The distribution of light emitted by a dipole in this structure is shown in Fig. 6.

It is clear from Fig. 6 that the general pattern of light

distribution is similar to that obtained for the uniform slabs in Fig. 4. Namely, light emitted by the dipole propagates within a narrow cone, along the straight lines making angles  $\pm\varphi(\theta_{min})$  with axis  $x$ . After negative refraction at the interface, two waves interfere at the focal point. However, one can emphasize some features specific for the structured slabs in Fig. 6. In the multi-layer slab each beam extends along the metal-dielectric boundaries due to surface plasmon-polariton excitation. Similarly, the beams extend along the wires in the second slab, where bright areas appear in the space between the wires, and darker areas are the metallic wires. Due to beam extension in two orthogonal directions in the wired and layered medium, the symmetry between the source of light and its image, which is obvious from Fig. 4, is lost. Note that the metallic inclusions are practically transparent for light since the optical skin depth  $c/\omega_p \approx 22$  nm exceeds their thickness. Here  $\omega_p = 8.9$  eV is plasma frequency for silver. Due to inequality  $c/\omega_p \ll R$ , the magnetization of silver wires in the ac field emitted by the dipole can be neglected<sup>24</sup>. Distribution of intensity in Fig. 6 supports interpretation of hyperbolic metamaterials as a medium that supports propagation of coupled surface plasmon modes<sup>25</sup>.

Figure 6c demonstrates the spatial distribution of light intensity in the interface plane  $z = 0$ . The maximum intensity is observed in the plane of polarization of propagating TM-wave ( $x-y$ -plane) within the base of the resonance cone. The intensity is minimal along axis  $z$ , where the evanescent TE-wave is polarized. The distribution of intensity in the focal plane  $z = z_f$  is shown in Fig. 6d. The position of the focal plane is obtained as a half height on the curve of intensity distribution over  $z$ . Wired structure with higher intensity in the dielectric background is clearly seen in Figs. 6c,d. To estimate the size of the image we used a standard procedure. The image size  $l$  is calculated as the full width of intensity distribution in the  $x-y$  plane taken at half maximum. It gives  $l_x \approx 35$  nm along axis  $x$  and  $l_y \approx 50$  nm along axis  $y$ . These subwavelength values exceed the resolutions reported in previous studies performed at shorter wavelengths. For example, the ratio  $l/\lambda = 0.075$  for the image shown in Fig. 6d. The reported in Refs. [10,11,26] results for  $l/\lambda$  are respectively 0.41, 0.37, 0.55. At the same time much higher image resolution,  $\lambda/117$ , was obtained in the microwave region<sup>27</sup>. In the microwave experiment with Weyl metacrystal the obtained resolution of 0.2 was relatively low<sup>7</sup>.

The efficiency of the proposed imaging system depends on the wavelength. The main factor is the transmission ratio  $T$ , which is the ratio of intensities at the focus and near the source. The plot of transmission ratio for the wavelength interval 650-750 nm is shown in Fig. 7. Appropriate choice of the filling factor of silver in both hyperbolic media makes it possible that each point in the graph fulfilled the matching conditions Eq. (9). The maximum at 670 nm is due to competition between the resonant enhancement of electromagnetic field in a col-

lection of metallic nanoparticles<sup>28</sup> and Joule dissipation. Both these factors vary with the wavelength that leads to the maximum of transmission at  $\lambda = 670$  nm. Higher than 10% transmission is predicted for the bandwidth 660-740 nm.

The proposed scheme needs a combination of layered and wired hyperbolic media to produce a focused image of an object in the near field. Optical hyperlens proposed in Ref. [8] and experimentally realized in Ref. [10] transfers subwavelength pattern in the far field using hyperbolic medium with cylindrical symmetry without focusing. Due to curved geometry the hyperlens magnifies the image, while the image clarity deteriorates. In the spherical hyperlens realized in Ref. [11] the sub-diffractive image is formed by narrow weakly-divergent beams. Almost nonspreading propagation is realized due to flattened isofrequency contours with relatively large curvature. This spherical hyperlens produces subwavelength image in two lateral dimensions. A flat lens with  $n \approx -1$  has been fabricated in Ref. [26]. It produces high-quality images with subwavelength resolution in the ultraviolet.

The lenses proposed in Refs. [8,10,26] allow subwavelength patterning beyond the near field. Our scheme produces image at the near-field with higher resolution. For the image in Fig. 6d the resolution  $l/\lambda = 0.075$  exceeds much the results  $l/\lambda = 0.41, 0.37, 0.55$  reported respectively in Refs. [10,11,26]. Higher resolution is achieved due to presence of two hyperbolic media, that guarantees preservation of the subwavelength components up to the focal point. The proposed near-field scheme is valid for subwavelength photolithography<sup>12</sup>.

A possibility of imaging using two hyperbolic media was proposed by Zhao *et al.*<sup>29</sup>. The imaging system proposed there consists of two layered structures with the same metallic (silver) and different dielectric (air and high refractive index polymer) constituents. An ultraviolet image of an object of two subwavelength slits was obtained by numeric modelled. Our scheme is also based on two metamaterials as that in Ref. [29]. However, in our case a combination of layered and wired structures allows to naturally achieve conjugate hyperbolic media with different signs for  $\varepsilon_{\parallel}^a$  and  $\varepsilon_{\parallel}^b$  as well as different signs for  $\varepsilon_{\perp}^a$  and  $\varepsilon_{\perp}^b$ . In our scheme the conditions of perfect transmission through the interface (9) can be easily satisfied. For two layered media with the same metal these conditions cannot be fulfilled at a reasonable filling fractions of metal leading to essential losses at reflection.

## VI. CONCLUSIONS

We proposed an optical near-field imaging system with deeply subwavelength resolution based on interfaced type I and type II hyperbolic media. The subwavelength image of a point source is formed by two interfering beams propagating along symmetric optical paths separating the regions with metallic and dielectric response. The hyperbolic media with the necessary optical param-

eters can be realized as metal-dielectric composites with layered and wired structures operating in the regime of homogenization. Light radiated by a source in the layered medium suffers negative refraction at the interface and is focused at the symmetric point in the wired medium. The proposed imaging system produces an image of about 50 nm wide of a point dipole radiating at the wavelength of 670 nm. The proposed imaging scheme may be applied for construction of flat hyperlenses with subwavelength resolution and other devices of subwavelength optics.

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## VIII. APPENDIX

Let a plane wave with TM-polarization and amplitude  $\mathbf{E}_0$  is incident on an interface between two uniaxial optical crystals. Orientation of the vectors  $\mathbf{k}$ ,  $\mathbf{E}$ , and  $\mathbf{S} \parallel \mathbf{v}_g$  in the incident and refracted wave is clear from Figs 2 and 3a. Magnetic field  $H$  is parallel to axis  $y$  and tangential component of electric field  $E_x = (ck_z/\omega\varepsilon_{\perp})H$ . Continuity of magnetic field  $H$  and electric field  $E_x$  at the interface  $z = 0$  leads to the set of linear equations

$$\begin{cases} H_i + H_r = H_t \\ \frac{1}{\varepsilon_{\perp}^a} (k_{(i)z} H_i + k_{(r)z} H_r) = \frac{k_{(t)z}}{\varepsilon_{\perp}^b} H_t. \end{cases} \quad (18)$$

Here indices  $i, r$ , and  $t$  label the components of the incident, reflected and transmitted wave, respectively. Solving these equation with respect to  $H_r$  and  $H_t$  we get the following Fresnel formulas:

$$H_r = \frac{\varepsilon_{\perp}^b k_{(i)z} - \varepsilon_{\perp}^a k_{(t)z}}{\varepsilon_{\perp}^a k_{(t)z} - \varepsilon_{\perp}^b k_{(r)z}} H_i, \quad H_t = \frac{\varepsilon_{\perp}^b (k_{(i)z} - k_{(r)z})}{\varepsilon_{\perp}^a k_{(t)z} - \varepsilon_{\perp}^b k_{(r)z}} H_i. \quad (19)$$

The  $x$ -component of the wave vector is conserved at reflection and refraction

$$k_{(i)x} = k_{(r)x} = k_{(t)x} = \frac{\omega}{c} \sqrt{\varepsilon^a(\theta)} \sin \theta. \quad (20)$$

Here  $\varepsilon(\theta)$  is defined by Eq. (4) with  $\varepsilon_{\perp} = \varepsilon_{\perp}^a$  and  $\varepsilon_{\parallel} = \varepsilon_{\parallel}^a$ . The  $z$ -components of the wave vector in the incident and reflected wave are equal by modulus but have opposite signs

$$k_{(i)z} = -k_{(r)z} = \frac{\omega}{c} \sqrt{\varepsilon^a(\theta)} \cos \theta \quad (21)$$

The  $z$ -component of  $\mathbf{k}_t$  in the transmitted wave is obtained from the dispersion relation (2). It follows from

Fig. 2 that  $\text{Re } k_{(t)z} < 0$ , i.e.

$$k_{(t)z} = -\frac{\omega}{c} \sqrt{\varepsilon_{\perp}^b \left( 1 - \frac{\varepsilon^a(\theta)}{\varepsilon_{\parallel}^b} \sin^2 \theta \right)}. \quad (22)$$

The reflection coefficient is defined as

$$R = \frac{|H_r|^2}{|H_i|^2} = \left| \frac{\varepsilon_{\perp}^a k_{(t)z} - \varepsilon_{\perp}^b k_{(i)z}}{\varepsilon_{\perp}^a k_{(t)z} + \varepsilon_{\perp}^b k_{(i)z}} \right|^2, \quad (23)$$

where the components of the wave vectors are given by Eqs. (21) and (22).

If both media are dissipationless the reflection coefficient equal to 1 at  $\theta = \theta_c$ . The critical angle  $\theta_c$ , which is the angle of total internal reflection, is obtained from the condition of vanishing  $k_{(t)z}$ , i.e. vanishing of the transmitted wave. It is clear that  $R = 1$  if  $k_{(t)z} = 0$  in Eq. (23). Moreover, for conjugate media (9) this remains true even for  $\theta < \theta_c$  since the components  $k_{(i)z}$ ,  $k_{(r)z}$ , and  $k_{(t)z}$  become pure imaginary and the phase of each square root in Eqs. (21) and (22) is obtained from the condition of exponential decay of the corresponding evanescent wave. To avoid singularity 0/0 in calculation of the reflection coefficient the dielectric functions should be taken with infinitesimally small imaginary parts.

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