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# Comprehensive solutions of the Bloch equations and dynamical models of open two-level systems

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The Bloch equation and its variants constitute the fundamental dynamical model for arbitrary two-level systems. Many important processes, including those in more complicated systems, can be modeled and understood through the two-level approximation. It is therefore of widespread relevance, especially as it relates to understanding dissipative processes in current cutting-edge applications of quantum mechanics. Although the Bloch equation has been the subject of considerable analysis in the seventy years since its inception, there is still, perhaps surprisingly, significant work that can be done. This paper extends the scope of previous analyses. It provides a framework for more fully understanding the dynamics of dissipative two-level systems. A solution is derived that is compact, tractable, and completely general, in contrast to previous results. Any solution of the Bloch equation depends on three roots of a cubic polynomial that are crucial to the time dependence of the system. The roots are typically only sketched out qualitatively, with no indication of their dependence on the physical parameters of the problem. Degenerate roots, which modify the solutions, have been ignored altogether. Here, the roots are obtained explicitly in terms of a single real-valued root that is expressed as a simple function of the system parameters. For the conventional Bloch equation, a simple graphical representation of this root is presented that makes evident the explicit time dependence of the system for each point in the parameter space. Several intuitive, visual models of system dynamics are developed. A Euclidean coordinate system is identified in which any generalized Bloch equation is separable, i.e., the sum of commuting rotation and relaxation operators. The time evolution in this frame is simply a rotation followed by relaxation at modified rates that play a role similar to the standard longitudinal and transverse rates. The Bloch equation also describes a system of three coupled harmonic oscillators, providing additional perspective on dissipative systems.

## I. INTRODUCTION

The Bloch equation needs little formal introduction. It was proposed originally as a classical, phenomenological model for the dissipative dynamics observed in magnetic resonance [1]. However, its impact has been more widespread. It is applicable to general quantum two-level systems, which can be modeled [2] by the classical torque equations that underpin Bloch's analysis. As a result, the Bloch equation is employed in such diverse fields as quantum optics, spin models, atomic collisions, condensed matter, and quantum computing. Quantum control theory (see, for example, reviews in [3–5]) is another field for which the Bloch equation is increasingly relevant. Dissipation must be minimized to meet its ambitious goal of manipulating quantum systems to desired ends. Dissipative processes are of special topical interest for quantum computing, where coherence must be preserved.

The dynamics of this fundamental model for arbitrary, dissipative two-level quantum systems is therefore a topic of more than passing interest. One might well expect the landscape of the Bloch equation to be fully explored after seventy years. However, existing solutions [6–9] share some or all of the following limitations, leaving room for further development. They (i) are not sufficiently gen-

eral to allow for arbitrary fields and relaxation models; (ii) depend on roots of a cubic polynomial that are not specified or related in any meaningful way to the physical parameters of the problem; (iii) divide by zero when the roots are degenerate, which occurs at values of the system parameters that are not specified; (iv) are cumbersome, conflated with the initial conditions and/or linked to tables of multiply nested variables with obscure connection to the physical parameters of the problem; (v) provide only a small measure of the physical insight that might be expected from an analytical solution.

In some respects, the complexity of the solutions make them only marginally better than a recipe for a numerical solution, which, in addition, is not completely general. As a separate issue, there are currently no intuitive visual models of system dynamics. Such models assist in the physical interpretation of the phenomena and often inspire further development in the field. Addressing the preceding matters might stimulate further advances towards understanding dissipative systems and controlling them for a desired outcome.

The paper proceeds as follows to address the aforementioned issues. A theoretical overview is provided in Sec. II. The intent is to give a fairly complete general understanding of the problem and the formal simplicity of the solution for arbitrary Bloch equation models. A benchmark for a more complete solution is defined at the outset by comparing previous Bloch equation solutions to the well-known solution for the damped harmonic oscillator. In addition, most previous treatments embed

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the initial conditions in the solution. The focus of the current solution is the propagator for the time evolution of the system. The initial conditions are disentangled from the dynamics. The physics does not depend on the initial conditions, so neither can the dynamics. Different initial conditions merely generate different trajectories for the system evolution, all driven by the same physics. The clarity provided in emphasizing the propagator contributed significant insight towards developing the intuitive dynamical models in the paper.

Section III is devoted to the explicit form of the propagator obtained formally in the previous section. A compact, complete solution to the Bloch equation is derived which is simpler than previous solutions, yet valid for arbitrary constant input parameters. The solutions are therefore applicable to more general but previously unsolved modified equations [10–22] proposed to address the failure of the original, conventional Bloch equation (OBE) to fully explain experimental data [23–25]. Moreover, the exact solutions are sufficiently simple that approximate limiting solutions [6–8] no longer provide any significant simplification. Conditions that result in division by zero in previous solutions are fully identified and addressed in the complete solution obtained here. A streamlined framework for obtaining and evaluating the roots of a cubic polynomial is developed that greatly facilitates the analysis. The roots required in the solution, i.e., system eigenvalues, are reduced to one real root obtained as a straightforward function of the physical parameters. Knowing this basic real root is sufficient to determine the others, simply and immediately. As is well known, the real parts of the roots are the dynamical relaxation rates, and the imaginary part, when it exists, is an oscillation frequency.

Section IV then focuses on the OBE. There, the dependence of the solutions on the physical parameters is characterized simply and in detail, neither of which have been done to date. The arithmetic difference between the spin-spin (transverse) and spin-lattice (longitudinal) relaxation rates provides a convenient and particularly useful frequency scale for representing system parameters in the analysis of the OBE. Quantitative bounds for oscillatory (underdamped) and non-oscillatory (critically damped and under damped) dynamics are derived. A simple graphical representation is obtained for the fundamental root as a function of the system parameters.

New models developed in Sec. V reveal the underlying simplicity of the dynamics. The Bloch equation is shown to represent a system of three mutually coupled damped harmonic oscillators. This model can also be cast in the form of frictionless coupled oscillators that are, nonetheless, damped. Both models provide new perspective on dissipative systems. The harmonic oscillator models are particular and explicit implementations of a more general result, namely, any quantum N-level system can be represented as a system of coupled harmonic oscillators [26, 27]. Although the dynamics are the same in either case, “there is a pleasure in recognizing

old things from a new point of view” [28]. A different perspective can open the door to new insights. This treatment sets the stage for a simple vector model of Bloch equation dynamics. The trajectory of a system state in the model coordinates is simply a rotation followed by relaxation, which is easily visualized without recourse to the detailed analytical solution. A modified system of relaxation rates that emerges from the dynamics plays a role analogous to standard longitudinal and transverse relaxation effects. The modified rates result from the interaction/coupling between the fields and the phenomenological relaxation parameters of the particular Bloch model under consideration. Additionally, and incidentally, a method for finding eigenvectors emerges that does not appear to be widely known or utilized.

Details of the results and calculations in the text are deferred to appendices. The concluding appendix checks the solutions by applying them to a representative set of cases whose solutions can be straightforwardly obtained by other methods. Finally, the acronym OBE used henceforth also includes the optical Bloch equation (e.g., [29]).

## II. THEORETICAL OVERVIEW

We first summarize the basic framework of the Bloch equation to recollect and define the fundamental parameters of the problem. The equation describes the dynamics of a magnetization  $\mathbf{M}$  subjected to a static polarizing magnetic field  $\mathbf{H}_0 = H_0 \hat{\mathbf{z}}$  and a sinusoidal alternating field  $2H_a \cos \omega_a t$  applied orthogonal to  $\mathbf{H}_0$ . For  $H_a \ll H_0$ , the equilibrium magnetization is not appreciably affected by the applied field and is therefore, to a good approximation, the time-independent value  $\mathbf{M}_0 = \chi H_0 \hat{\mathbf{z}}$  produced by the polarizing field.

One then considers a reference frame rotating about  $\mathbf{H}_0$  at an angular frequency  $\omega_a$  equal to the frequency of the applied field [30]. In this frame, the resulting effective field  $\mathbf{H}_e$  is also time-independent. The evolution of the magnetization in this frame, neglecting dissipative effects, is simply a rotation about the field at the Larmor frequency  $\omega_e = -\gamma \mathbf{H}_e$  due to the torque  $\gamma \mathbf{M} \times \mathbf{H}_e$  on  $\mathbf{M}$ , with  $\mathbf{H}_e = (H_a \cos \phi, H_a \sin \phi, H_0 - \omega_a/\gamma)$ . Here,  $\gamma$  is the gyromagnetic moment. An exact representation of the linearly polarized field  $2H_a \cos \omega_a t$  also requires a counter rotating component. The rotating frame (NMR) or rotating wave (optics) approximation safely neglects this other frame when  $H_a \ll H_0$ , since then  $\mathbf{H}_e \approx H_e \hat{\mathbf{z}}$  in the counter rotating frame and has negligible effect on the initial magnetization  $M_0 \hat{\mathbf{z}}$ . The phase  $\phi$  relative to the  $x$ -axis in the rotating frame is arbitrary in the context of a single applied field and has typically been set equal to zero in previous analyses of the Bloch equation. However, the relative phase is required for problems involving sequentially applied fields.

Relaxation rates  $R_i$  are then assigned to each component  $M_i$  to include dissipative processes. The torque can be written as a matrix-vector product [31], which,

174 together with relaxation, gives the matrix

$$\Gamma = \begin{pmatrix} R_1 & \omega_3 & -\omega_2 \\ -\omega_3 & R_2 & \omega_1 \\ \omega_2 & -\omega_1 & R_3 \end{pmatrix} \quad (1)$$

175 comprised of the rates and the components of  $\omega_e$ . In the  
176 original Bloch equation, the rates governing relaxation  
177 of the transverse magnetization components are equal,  
178  $R_1 = R_2$ . More generally, modified Bloch equations can  
179 be considered in which the  $R_i$  are not equal, and, more-  
180 over,  $\Gamma_{ij} \neq -\Gamma_{ji}$ , as occurs for sufficiently strong fields  
181 and intensity-dependent damping[10–22]. Including the  
182 initial polarization  $M_0$  or analogous equilibrium state rel-  
183 evant to a given application then gives a general Bloch  
184 equation of the form

$$\dot{\mathbf{M}}(t) + \Gamma \mathbf{M}(t) = \mathbf{M}_0 R_3. \quad (2)$$

185 The matrix  $\Gamma$  that drives the dynamics is completely  
186 general in what follows, within the context of time-  
187 independent fields and relaxation rates. Both  $\mathbf{H}_e$  and  
188  $\omega_e$  are referred to as fields in the OBE, since they are  
189 proportional. We further define the transverse field  $\omega_{12}$   
190 as a component of the total field  $\omega_e$ , with respective mag-  
191 nitudes (squared)

$$\begin{aligned} \omega_{12}^2 &= \omega_1^2 + \omega_2^2 \\ \omega_e^2 &= \omega_1^2 + \omega_2^2 + \omega_3^2. \end{aligned} \quad (3)$$

192 In the optical Bloch equation, the preceding fields be-  
193 come electric fields, magnetic moments are atomic dipole  
194 moments,  $\omega_1$  and  $\omega_2$  are proportional to the correspond-  
195 ing components of the applied electric field, and the reso-  
196 nance offset  $\omega_3$  is the difference between the atomic tran-  
197 sition frequency and the frequency of the applied electric  
198 field.

### 199 A. An instructive analogy

200 The damped harmonic oscillator can be used to illus-  
201 trate how the OBE solutions might be viewed as incom-  
202 plete, notwithstanding the need for a more generally ap-  
203 plicable solution. Consider first the original Torrey [6]  
204 solution. All other solutions to date are similar in con-  
205 tent. As mentioned in the Introduction, any solution will  
206 depend on the roots of a cubic polynomial. The formula  
207 for these roots is well-known, if somewhat unwieldy, giv-  
208 ing three roots of the form  $a$  and  $b \pm is$ , in Torrey's no-  
209 tation, with  $a, b$  real and  $s$  either real or imaginary. No  
210 further details of the roots are given. The magnetization  
211 components,  $M_i$ , can then be obtained as

$$M_i(t) = A_i e^{-at} + e^{-bt} \left[ B_i \cos st + \frac{C_i}{s} \sin st \right] + D_i. \quad (4)$$

212 The coefficients  $A_i, B_i, C_i, D_i$  are complicated functions  
213 of the physical parameters and the initial magnetization

214  $M_i(0)$ , typically listed in Tables in terms of multiply-  
215 nested variables. The  $D_i$  are the components of the  
216 steady-state magnetization. The roots are not specified  
217 further. In one instance [8], they are given in compli-  
218 cated form. Either way, none of the solutions provide  
219 any physical insight into the dependence of the decay  
220 and oscillation rates on the physical parameters of the  
221 problem. In addition,  $s = 0$  results in doubly degenerate  
222 roots. The further condition  $a = b$  gives a triple degen-  
223 eracy. These degeneracies have not been fully noted or  
224 addressed.

225 Consider next the equation of motion for a damped  
226 harmonic oscillator under the influence of a constant  
227 force such as gravity. It can be written in the form

$$\ddot{x} + 2b\dot{x} + \omega_0^2 x = g. \quad (5)$$

228 The natural frequency of the oscillator is  $\omega_0$ , with the  
229 velocity-dependent damping parameter  $b$  scaled by a fac-  
230 tor of 2 to eliminate this factor from the solution. The  
231 standard approach tries a solution of the form  $e^{rt}$  for  
232 the  $g = 0$  solution to the homogeneous equation, giv-  
233 ing a quadratic polynomial in  $r$ . The two roots of a  
234 second-order polynomial are known to be of the form  
235  $r_{\pm} = -a \pm is$ , with  $a$  real and  $s$  either real or imag-  
236 inary depending on the sign of the discriminant in the  
237 quadratic formula. The particular solution to Eq. (5) is  
238  $x(t) = g/\omega_0^2$ , by inspection. With this minimal analy-  
239 sis, the solution obtained from  $e^{r_{\pm}t}$  can be written in the  
240 form

$$x(t) = e^{-at} \left[ A_1 \cos st + \frac{A_2}{s} \sin st \right] + D. \quad (6)$$

241 The steady-state  $D = g/\omega_0^2$  is the constant displacement  
242 of the oscillator from the unperturbed,  $g = 0$ , equilib-  
243 rium position. The coefficients  $A_i$  determined from the  
244 initial conditions are considerably simpler than the cor-  
245 responding coefficients in Eq. (4).

246 Solutions for the Bloch equation proceed only this far.  
247 The damped oscillator is a much simpler system that is  
248 readily solved in more detail. The coordinates are typi-  
249 cally shifted to define  $D$  as the new equilibrium position.  
250 The quadratic formula gives simple expressions for the  
251 roots and immediately shows that the decay rate will be  
252 the physical damping factor  $b$ . One easily proceeds fur-  
253 ther to obtain  $s = (\omega_0^2 - b^2)^{1/2}$ , giving (i) underdamped  
254 ( $\omega_0^2 > b^2$ ), (ii) overdamped ( $\omega_0^2 < b^2$ ), and (iii) critically  
255 damped ( $\omega_0^2 = b^2$ ) solutions. The domain of applicabil-  
256 ity for each solution is clearly delineated as a function of  
257 the physical parameters  $b$  and  $\omega_0$ . When  $s = 0$ , there  
258 is a single doubly degenerate root. The second linearly  
259 independent solution is  $te^{-bt}$ , giving

$$x_{s=0}(t) = e^{-bt} [A_1 + A_2 t] + D, \quad (7)$$

260 The constants  $A_i$  and  $D$  are the same as before, which  
261 is consistent with Eq. (6) in the limit  $s \rightarrow 0$ , using  
262 L'Hopital's rule. We will show in Sec. III that the same  
263 limiting process is valid for Eq. (4) by more formally find-  
264 ing the linearly independent solutions in the case of de-  
265 generate roots.

The failure of the OBE solutions to match the completeness of the damped oscillator solution is not particularly surprising. The OBE appears to have five independent parameters (the elements of  $\Gamma$  in Eq. (1) with  $R_1 = R_2$ ). Analysis of the system is far more complex, appearing perhaps too complex for a more illuminating result. However, a simpler realization of cubic roots developed here and more detailed investigation of the roots resulting from the OBE shows only three independent parameters, two of which can be scaled in terms of the third to give a two-parameter problem similar to the damped oscillator.

One might also be intrigued by the similarity of the solutions for the damped oscillator and the Bloch equation. This correspondence is not accidental, and will be pursued further in Sec. V, where the Bloch equation is modeled exactly by a system of three coupled, damped harmonic oscillators. In addition, the dynamics of a single damped oscillator is known to be simple in the  $(x, \dot{x})$  phase plane (see, for example, Marion [32]). The underdamped trajectory is related to a logarithmic spiral, while the overdamped trajectory traces out a non-oscillatory asymptotic decay to zero. The analogous visual model for Bloch equation dynamics is developed in Sec. VC.

But first, we extend the Bloch equation solution to arbitrary (constant) parameter models. The new solution is simpler and more convenient to use than existing OBE solutions, which, in addition, are problematic for particular configurations of the parameter space.

## B. Bloch equation solution

A standard approach to solving a system of inhomogeneous equations such as Eq. (2) is to transform it to a homogeneous form [33] by appending the inhomogeneous term  $\mathbf{M}_0 R_3$  as a column to the right of  $\Gamma$  and then adding a correspondingly expanded row of zeros at the bottom. The vector  $\mathbf{M}$  would then be augmented by including a last element equal to one. Increasing the dimensionality of the problem in this way can be rather trivially avoided by defining

$$\mathcal{M}(t) \equiv \mathbf{M}(t) - \mathbf{M}_\infty, \quad (8)$$

where  $\mathbf{M}_\infty = \Gamma^{-1} \mathbf{M}_0 R_3$ . This is the same shift in coordinates to the equilibrium (steady-state) position that is commonly employed for the harmonic oscillator example of Eq. (5). There, the result of a constant force is a shifted equilibrium position  $x \rightarrow (\omega_0^2)^{-1} g$ , which gives a homogeneous equation in the shifted coordinates. Since  $\mathbf{M}_\infty$  is constant, we have

$$\dot{\mathcal{M}}(t) = -\Gamma \mathcal{M}(t) \quad (9)$$

with solution

$$\mathcal{M}(t) = e^{-\Gamma t} \mathcal{M}(0) \quad (10a)$$

$$\mathbf{M}(t) = e^{-\Gamma t} [\mathbf{M}(0) - \mathbf{M}_\infty] + \mathbf{M}_\infty \quad (10b)$$

$$= e^{-\Gamma t} \mathbf{M}(0) + (1 - e^{-\Gamma t}) \mathbf{M}_\infty \quad (10c)$$

as a function of the steady-state  $\mathbf{M}_\infty$  and transient  $\mathbf{M}(0)$  responses. The crux of the problem, then, is a solution for the propagator  $e^{-\Gamma t}$ . Framing the problem most generally to include arbitrary  $\Gamma$  might be expected to complicate the solution compared to previous treatments. However, emphasizing the solution for the propagator results in a compact and relatively simple solution.

## C. The propagator $e^{-\Gamma t}$

There are numerous methods, both analytical and numerical, for calculating a matrix exponential [Moler and van Loan [34] and references therein]. The Laplace transform will be employed here, both for historical reasons (it has been utilized in previous Bloch equation solutions) and because most of the other analytical methods can be derived from it. This is a topic worth developing in its own right that is beyond the scope of the present article.

The Laplace transform  $\mathcal{L}$  of  $e^{-at}$  is equal to  $(s+a)^{-1}$  for constant  $a$ . The matrix exponential  $e^{-\Gamma t}$  for constant  $\Gamma$  is then the inverse Laplace transform  $\mathcal{L}^{-1}[(s\mathbb{1} + \Gamma)^{-1}]$ , where  $\mathbb{1}$  is the identity element. The inverse Laplace transform of a function  $f(s)$  can be written in terms of the Bromwich integral as [see, for example, Arfken [35]]

$$\begin{aligned} \mathcal{L}^{-1}[f(s)] &= \frac{1}{2\pi i} \int_{\gamma-i\infty}^{\gamma+i\infty} f(s) e^{st} ds \\ &= F(t), \end{aligned} \quad (11)$$

where the real constant  $\gamma$  is chosen such that  $\text{Re}(s) < \gamma$  for all singularities of  $f(s)$ . Closing the contour by an infinite semicircle in the left half plane ensures convergence of the integral for  $t > 0$ . The desired  $F(t)$  is then the sum of the residues of the integrand.

For  $f(s) = (s\mathbb{1} + \Gamma)^{-1}$ , recall the textbook theorem for the inverse of a matrix  $A$ , with terms defined as follows:

- (i)  $A(i|j)$  is the matrix obtained by deleting row  $i$  and column  $j$  of  $A$ .
- (ii) The cofactor of  $A_{ij}$  is  $C_{ij} = (-1)^{i+j}$  times the determinant  $\det A(i|j)$ .
- (iii) The adjugate of  $A$  is the matrix  $(\text{adj } A)_{ij} = C_{ji}$ , i.e., the transpose of the cofactor matrix for  $A$ , which is the same as the cofactors of  $A$  transpose.

Then

$$A^{-1} = \text{adj } A / \det A. \quad (12)$$

The matrix

$$A(s) = s\mathbb{1} + \Gamma \quad (13)$$

gives

$$\det A(s) = p(s), \quad (14)$$

where  $p(s)$  is the characteristic polynomial of  $(-\Gamma)$ .

353 The desired solution for  $F(t) = e^{-\Gamma t}$  is then the sum  
 354 of the residues of the integrand in Eq. (11), with  $f(s) \rightarrow$   
 355  $(s\mathbb{1} + \Gamma)^{-1} = \text{adj } A(s)/p(s)$  giving

$$e^{-\Gamma t} = \sum_{\text{res}} \frac{\text{adj } A(s)}{p(s)} e^{st} \quad (15)$$

356 for any  $\Gamma$ . The poles clearly occur at the roots of  $p(s)$ ,  
 357 i.e., the eigenvalues of  $-\Gamma$ . The propagator is therefore  
 358 constructed fairly simply from  $\Gamma$  and its eigenvalues.

359 Recall for reference in what follows that for a function  
 360  $g(s)$  with a pole of order  $k$  at  $s = s_0$ , the coefficient of  
 361  $(s - s_0)^{-1}$  in the Laurent series expansion of  $g(s)$  about  
 362  $s = s_0$ , i.e., the residue at  $s_0$ , is

$$\text{res}(s_0) = \frac{1}{(k-1)!} \lim_{s \rightarrow s_0} \frac{d^{k-1}}{ds^{k-1}} [(s - s_0)^k g(s)] \quad (16)$$

### 363 III. SOLUTIONS FOR THE PROPAGATOR

364 The results obtained so far provide the basis for a com-  
 365 plete, compact, general solution of the Bloch equation,  
 366 developed in detail, next. The solution for the matrix  
 367 exponential  $e^{-\Gamma t}$  is valid for any time-independent  $3 \times 3$   
 368 matrix  $\Gamma$ . Degenerate roots of the characteristic poly-  
 369 nomial, which give rise to division by zero in previous  
 370 solutions, are fully addressed in the form of the solution  
 371 given in Eq. (15).

#### 372 A. Roots of the characteristic polynomial

373 The solution for  $e^{-\Gamma t}$  given in Eq. (15) requires the  
 374 roots of  $p(s)$  in Eq. (14). The resulting third degree poly-  
 375 nomial is

$$p(s) = c_0 + c_1 s + c_2 s^2 + s^3 \quad (17)$$

376 with coefficients

$$\begin{aligned} c_0 &= \prod_j R_j - \frac{1}{2} \sum_{j \neq k \neq l} R_j \Gamma_{kl} \Gamma_{lk} + \\ &\quad \Gamma_{12} \Gamma_{23} \Gamma_{31} + \Gamma_{21} \Gamma_{32} \Gamma_{13} \\ &\xrightarrow{\text{OBE}} \prod_j R_j + \sum_j R_j \omega_j^2 \\ c_1 &= - \sum_{\substack{j \neq k \\ j < k}} \Gamma_{jk} \Gamma_{kj} + \sum_{j < k} R_j R_k \\ &\xrightarrow{\text{OBE}} \omega_e^2 + R_1 R_2 + R_1 R_3 + R_2 R_3 \\ &= \omega_e^2 + \sum_{j < k} R_j R_k \\ c_2 &= \sum_i R_i. \end{aligned} \quad (18)$$

377 As well known, the substitution  $s = z - c_2/3$  reduces  
 378 Eq. (17) to the standard canonical form

$$\begin{aligned} p(z - c_2/3) &= z^3 + \tilde{c}_1 z + \tilde{c}_0 \\ &= q(z), \end{aligned} \quad (19)$$

379 where

$$\begin{aligned} \tilde{c}_0 &= 2 \left( \frac{c_2}{3} \right)^3 - c_1 \left( \frac{c_2}{3} \right) + c_0 \\ \tilde{c}_1 &= c_1 - c_2^2/3 \end{aligned} \quad (20)$$

380 Solutions for the roots  $z_i$  are then available as functions  
 381 of  $\tilde{c}_0$  and  $\tilde{c}_1$  from standard formulas. However, these for-  
 382 mulas are relatively complicated functions of the polyno-  
 383 mial coefficients (and hence, the physical parameters in  
 384 the Bloch equation), which hinders physical insight. In  
 385 Appendix C, simpler expressions are derived for the roots  
 386 that reduce their complexity compared to previous treat-  
 387 ments. The fundamental results are summarized below.

388 Any polynomial with real coefficients has at least one  
 389 real root, assigned here to  $z_1$ . The solutions can then be  
 390 consolidated in a convenient form that does not appear  
 391 to have been employed before. The other two roots are  
 392 written as a function of  $z_1$ ,

$$\begin{aligned} z_{2,3} &\equiv z_{\pm} \\ &= -\frac{1}{2} z_1 \pm i \varpi, \end{aligned} \quad (21)$$

393 in terms of a discriminant

$$\varpi^2 = 3[(z_1/2)^2 + \tilde{c}_1/3], \quad (22)$$

394 which will be positive, negative, or zero depending on the  
 395 value of  $z_1$ , the sign of  $\tilde{c}_1$ , and their relative magnitudes.

396 The roots are further characterized here in terms of  
 397 the positive parameter

$$\gamma = \frac{|\tilde{c}_0/2|}{|\tilde{c}_1/3|^{3/2}}, \quad (23)$$

398 leading to the following delineation of the roots:

399 (i)  $\tilde{c}_1 > 0$ , or,  $\tilde{c}_1 < 0$  and  $\gamma > 1$

400 3 distinct roots (1 real, 2 complex conjugate)

401 (ii)  $\tilde{c}_1 < 0$  and  $\gamma < 1$

402 3 distinct real roots

403 (iii)  $\tilde{c}_1 < 0$  and  $\gamma = 1$

404 2-fold degenerate roots  $z_+ = z_- = -\frac{1}{2} z_1$

405 (iv)  $\tilde{c}_0 = 0 = \tilde{c}_1$

406 3-fold degenerate roots  $z_i = 0$

407 The physical parameters that define these effective do-  
 408 mains for the roots are derived for the OBE in Sec. IV.

409 In addition, we will find that the sign of  $\tilde{c}_0$  determines  
 410 the sign of  $z_1$ . Thus, in all cases, the set of three roots for  
 411 a given  $\tilde{c}_0 < 0$  is equal and opposite to the set obtained

412 for parameters that flip the sign of  $\tilde{c}_0$ . The case  $\tilde{c}_0 = 0$   
 413 (i.e.,  $\gamma = 0$ ) reduces simply to  $z_1 \sim \text{sgn}(0) = 0$ . From  
 414 Eqs. (21) and (22), there are then two additional real or  
 415 imaginary roots depending on the sign of  $\varpi^2$ .

416 The roots of  $p(s = z - c_2/3)$  are then

$$s_i = z_i - c_2/3, \quad (24)$$

417 where, referring to Eq. (18),

$$\frac{c_2}{3} = \frac{1}{3} \sum_i R_i \equiv \bar{R} \quad (25)$$

418 is the average of the relaxation rates.

## 419 B. Cayley-Hamilton Theorem

420 The expression for  $e^{-\Gamma t}$  in Eq. (15) also depends on  
 421  $\text{adj } A(s)$ . The elements of  $\text{adj } A(s)$ , are simple  $(2 \times 2)$   
 422 determinants, giving

$$\text{adj } A(s) = A_0 + A_1 s + \mathbb{1} s^2, \quad (26)$$

423 a polynomial in  $s$  with coefficient matrices

$$A_0 = c_1 \mathbb{1} - c_2 \Gamma + \Gamma^2, \quad A_1 = c_2 \mathbb{1} - \Gamma, \quad (27)$$

424 as shown in Appendix A. The result can be readily gen-  
 425 eralized to higher dimensional matrices, but this exceeds  
 426 the scope of the present work.

427 Substituting Eq. (27) into Eq. (26) and rearranging  
 428 terms gives

$$\begin{aligned} \text{adj } A(s) &= (c_1 + c_2 s + s^2) \mathbb{1} + (c_2 + s)(-\Gamma) + \Gamma^2 \\ &= \sum_{j=0}^2 p_j(s) (-\Gamma)^j, \end{aligned} \quad (28)$$

429 which defines the polynomial coefficients  $p_j(s)$ . Further  
 430 defining

$$a_j(t) = \sum_{\text{res}} \frac{p_j(s)}{p(s)} e^{st}, \quad j = 0, 1, 2 \quad (29)$$

431 then yields a solution for the propagator in the form

$$\begin{aligned} e^{-\Gamma t} &= \sum_{j=0}^2 a_j(t) (-\Gamma)^j \\ &= (\mathbb{1}, -\Gamma, \Gamma) \begin{bmatrix} a_0(t) \\ a_1(t) \\ a_2(t) \end{bmatrix} \end{aligned} \quad (30)$$

432 where the sum has been expressed as multiplication of  
 433 a row and column matrix. We therefore have a concise  
 434 implementation of the Cayley-Hamilton theorem, which  
 435 states that every square matrix is a solution to its char-  
 436 acteristic equation. As a consequence,  $-\Gamma$  is a solution of  
 437 Eq. (17). One can solve for  $\Gamma^3$ , and subsequently for all  
 438 higher powers of  $\Gamma$ , in terms of the set  $\{\mathbb{1}, -\Gamma, \Gamma^2\}$ . The

series expansion of  $e^{-\Gamma t}$  can then be expressed in terms  
 440 of the same set, as above.

441 The coefficient polynomial  $p_j(s)$  multiplying  $(-\Gamma)^j$  can  
 442 be defined recursively as

$$\begin{aligned} p_{-1}(s) &\equiv p(s) \\ p_j(s) &= \frac{p_{j-1}(s) - c_j}{s}, \end{aligned} \quad (31)$$

443 i.e.,  $p_j(s)$  is obtained by dividing  $p(s)$  by  $s^{j+1}$  and remov-  
 444 ing all terms with  $s$  in the denominator from the result.  
 445 The matrix exponential given in Eq. (30) is then readily  
 446 generalized to matrices of arbitrary dimension.

## 447 C. A convenient matrix partitioning

448 We first seek to avoid transforming the characteris-  
 449 tic polynomial to canonical form, solving for these roots,  
 450 then transforming back to obtain the roots of the origi-  
 451 nal polynomial. The result of this endeavor leads to  
 452 additional simplifications in what follows.

453 Partition  $\Gamma$  as the sum of commuting matrices

$$\begin{aligned} \Gamma &= \mathcal{R} + \Gamma_p \\ &= \bar{R} \mathbb{1} + \begin{pmatrix} R_{1p} & \Gamma_{12} & \Gamma_{13} \\ \Gamma_{21} & R_{2p} & \Gamma_{23} \\ \Gamma_{31} & \Gamma_{32} & R_{3p} \end{pmatrix}, \end{aligned} \quad (32)$$

454 where, as before,  $\bar{R}$  is the average of the  $R_i$  as in Eq. (25),  
 455 and the diagonal elements of  $\Gamma_p$  are

$$\begin{aligned} R_{ip} &= R_i - \bar{R} \\ &= \frac{2}{3} R_i - \frac{1}{3} \sum_{j \neq i} R_j. \end{aligned} \quad (33)$$

456 The coefficients  $c_{ip}$  in the characteristic polynomial for  
 457  $-\Gamma_p$  are obtained from Eq. (18) with  $R_i \rightarrow R_{ip}$ . Then,  
 458  $c_{2p} = \sum_i R_{ip} = 0$ , and  $p(s)$  is in the standard canonical  
 459 form  $q(z)$  of Eq. (19), with coefficients  $c_{ip} \equiv \tilde{c}_i$ . We then  
 460 have

$$e^{-\Gamma t} = e^{-\bar{R} t} e^{-\Gamma_p t}. \quad (34)$$

461 The focus henceforth will be the solution for  $e^{-\Gamma_p t}$   
 462 using Eq. (30), with the obvious substitutions  $\Gamma \rightarrow \Gamma_p$ ,  
 463  $p_j \rightarrow q_j$ , and  $c_j \rightarrow \tilde{c}_j$ . The roots  $s_i = z_i$  are given in  
 464 Eq. (C6).

## 465 D. Simple pole solution

466 When the roots  $z_i$  of  $q(z)$  are distinct, the residues  
 467 are due to simple first-order poles,  $z_n$ . Factor  $q(z)$  as  
 468  $\prod_i (z - z_i)$ . Then  $(z - z_n)/q(z) = \prod_{i \neq n} (z - z_i)$ , as  
 469 needed to evaluate the residue at  $z_n$ . The derivative  
 470  $q'(z) = \sum_j \prod_{i \neq j} (z - z_i)$  evaluated at  $z_n$  is also equal

471 to  $\prod_{i \neq n} (z_n - z_i)$ , since the other terms in the sum van-  
 472 ish at  $z = z_n$ . Summing the residues in Eq. (29) at the  
 473 three roots gives

$$a_j(t) = \sum_{i=1}^3 \frac{q_j(z_i)}{q'(z_i)} e^{z_i t} \quad (35)$$

474 The derivative of the characteristic polynomial can be  
 475 calculated from either the factored form involving the  
 476 roots or the polynomial form in Eq. (17). Each provides  
 477 information that might be useful for different applica-  
 478 tions. The matrix exponential  $e^{-\Gamma_p t}$  can then be written  
 479 compactly as matrix multiplication in the form

$$\begin{aligned} e^{-\Gamma_p t} &= (\mathbb{1}, -\Gamma_p, \Gamma_p^2) \begin{bmatrix} a_0(t) \\ a_1(t) \\ a_2(t) \end{bmatrix} \\ &= (\mathbb{1}, -\Gamma_p, \Gamma_p^2) [W_1(z_1) \mathbf{u}_1(t)], \\ W_1(z_1) &= \begin{pmatrix} z_1^2 + \tilde{c}_1 & z_2^2 + \tilde{c}_1 & z_3^2 + \tilde{c}_1 \\ z_1 & z_2 & z_3 \\ 1 & 1 & 1 \end{pmatrix} \\ \mathbf{u}_1(t) &= \begin{pmatrix} e^{z_1 t}/q'(z_1) \\ e^{z_2 t}/q'(z_2) \\ e^{z_2 t}/q'(z_2) \end{pmatrix}. \end{aligned} \quad (36)$$

480 For parameter values

481 (i)  $\tilde{c}_1 > 0$  or  $\tilde{c}_1 < 0$  and  $\gamma > 1$ ,

482  $\varpi$  is real from Eqs. (C6a) and (C6b), so two of the roots  
 483 are complex conjugates. Although Eq. (36) is the most  
 484 straightforward form of the solution and readily used in  
 485 numerical calculations, individual terms are complex. A  
 486 more transparently real-valued expression is obtained by  
 487 performing the sum in Eq. (35) after rationalizing com-  
 488 plex denominators and writing the roots  $z_{2,3}$  in terms of  
 489  $z_1$  using Eqs. (21) and (22), as detailed in Appendix D.  
 490 The result is of the form in Eq. (36) with

$$\begin{aligned} W_1(z_1) &\rightarrow \frac{1}{3z_1^2 + \tilde{c}_1} \begin{pmatrix} z_1^2 & 2z_1^2 & -\tilde{c}_1 z_1 \\ z_1 & -z_1 & \frac{3}{2}z_1^2 + \tilde{c}_1 \\ 1 & -1 & -\frac{3}{2}z_1 \end{pmatrix} \\ \mathbf{u}_1(t) &\rightarrow \begin{pmatrix} e^{z_1 t} \\ e^{-z_1 t/2} \frac{\cos \varpi t}{\varpi} \\ e^{-z_1 t/2} \frac{\sin \varpi t}{\varpi} \end{pmatrix}. \end{aligned} \quad (37)$$

491 The coefficient  $\tilde{c}_1$  can be found in terms of the roots  $z_i$   
 492 upon expanding the factored form for  $q(z)$  to obtain  $\tilde{c}_1 =$   
 493  $z_1 z_2 + z_1 z_3 + z_2 z_3$ . The solution for the matrix exponential  
 494 is thus separable into a term that depends directly on the  
 495 physical parameters of the problem through  $\Gamma_p$ , a term  
 496 that depends on the roots  $z_i$ , and a term that gives the  
 497 time dependence, which in turn is solely a function of the  
 498 roots.

499 For the case

500 (ii)  $\tilde{c}_1 < 0$  and  $\gamma < 1$ ,

501  $\varpi$  is imaginary, as given by Eq. (C6c), so there are  
 502 three real roots. There is no oscillatory behavior in  
 503 the straightforward result given in Eq. (36). The solu-  
 504 tion can be written alternatively in terms of  $\mu = |\varpi|$   
 505 using Eq. (37), with  $\varpi = i\mu$  giving  $\cos \varpi t \rightarrow \cosh \mu t$   
 506 and  $\sin \varpi t / \varpi \rightarrow \sinh \mu t / \mu$ .

## 507 E. Second-order pole solution

508 For

509 (iii)  $\tilde{c}_1 < 0$  and  $\gamma = 1$ ,

510 we have  $\varpi = 0$  in either Eq. (C6b) or Eq. (C6c), which  
 511 implies  $\tilde{c}_1 \rightarrow -3(z_1/2)^2$  according to Eq. (22). Then two  
 512 of the three real roots are equal, giving a doubly degen-  
 513 erate root  $z_2 = z_3 = -z_1/2$ . The characteristic polyno-  
 514 mial  $q(z) \rightarrow (z - z_1)(z - z_2)^2$ . The contribution from  
 515 the first-order pole at  $z_1$  is obtained as before, i.e., the  
 516 first column of  $W_1(z_1)$  and the first element of  $\mathbf{u}_1(t)$  in  
 517 Eq. (37) remain the same. The residue at  $z_2$  is calculated  
 518 in Appendix D, leading to a solution

$$e^{-\Gamma_p t} = (\mathbb{1}, -\Gamma_p, \Gamma_p^2) [W_2(z_1) \mathbf{u}_2(t)],$$

$$W_2(z_1) = \begin{pmatrix} \frac{1}{9} & \frac{8}{9} & \frac{1}{3}z_1 \\ \frac{4}{9}z_1^{-1} & -\frac{4}{9}z_1^{-1} & \frac{1}{3} \\ \frac{4}{9}z_1^{-2} & -\frac{4}{9}z_1^{-2} & -\frac{2}{3}z_1^{-1} \end{pmatrix}$$

$$\mathbf{u}_2(t) = \begin{pmatrix} e^{z_1 t} \\ e^{-z_1 t/2} \\ t e^{-z_1 t/2} \end{pmatrix}. \quad (38)$$

519 There is thus a term linear in the time,  $t$ . Note that  
 520 Eq. (38) is also the limit of Eq. (37) as  $\varpi \rightarrow 0$  and  
 521  $\tilde{c}_1 \rightarrow -3(z_1/2)^2$ , providing an independent verification of  
 522 the simple-pole result. One could anticipate on physical  
 523 grounds that the separate solutions obtained for distinct  
 524 and degenerate roots should be continuous in this limit.  
 525 However, it is an assumption that is verified by properly  
 526 calculating the solution for a second-order pole.

## 527 F. Third-order pole solution

528 The case

529 (iv)  $\tilde{c}_0 = 0 = \tilde{c}_1$

530 gives a triply degenerate, real root  $z_1 = 0$  for  $q(z) \rightarrow z^3$ .  
 531 The  $a_j(t)$  are evaluated in Appendix D, giving  $a_0(t) = 1$ ,  
 532  $a_1(t) = t$ , and  $a_2(t) = t^2/2$ , so that

$$e^{-\Gamma_p t} = \mathbb{1} - \Gamma_p t + \frac{1}{2} \Gamma_p^2 t^2. \quad (39)$$

533 There is now a term that is quadratic in the time. The  
 534 same result is obtained from Eq. (38) in the limit  $z_1 \rightarrow 0$   
 535 upon series expansion of the exponential terms. In ad-  
 536 dition, the Cayley-Hamilton theorem is simple to apply  
 537 directly in this case, since  $q(-\Gamma_p) = -\Gamma_p^3 = 0$ . The se-  
 538 ries expansion of  $e^{-\Gamma_p t}$  is therefore truncated, giving the  
 539 Eq. (39) result directly and verifying the self-consistency  
 540 of the solutions.

### 541 G. Steady state solution

542 The steady state response  $\mathbf{M}_\infty$  defined in Eq. (10) is  
 543 equal to  $\Gamma^{-1}\mathbf{M}_0R_3$ , with  $\Gamma^{-1} = \text{adj } \Gamma / \det(\Gamma)$ . The de-  
 544 pendence on  $\text{adj } \Gamma$  is only in the third column, since  $\mathbf{M}_0$   
 545 is along  $\hat{z}$ , with  $\det(\Gamma) = p(0)$  given by  $c_0$  in Eq. (18).  
 546 Then

$$547 \mathbf{M}_\infty = \frac{M_0 R_3}{c_0} \begin{bmatrix} \Gamma_{12}\Gamma_{23} - \Gamma_{13}\Gamma_{22} \\ \Gamma_{13}\Gamma_{21} - \Gamma_{23}\Gamma_{11} \\ -\Gamma_{12}\Gamma_{21} + R_1R_2 \end{bmatrix} \quad (40a)$$

$$\xrightarrow{\text{OBE}} \frac{\chi H_0 R_3}{R_1 R_2 R_3 \left(1 + \sum_{i \neq j \neq k} \frac{\omega_i^2}{R_j R_k}\right)} \begin{bmatrix} \omega_1 \omega_3 + \omega_2 R_2 \\ \omega_2 \omega_3 - \omega_1 R_1 \\ \omega_3^2 + R_1 R_2 \end{bmatrix} \quad (40b)$$

547 Letting  $R_1 = R_2 = 1/T_2$  and  $R_3 = 1/T_1$  gives

$$548 \mathbf{M}_\infty \xrightarrow{\text{OBE}} \frac{\chi H_0}{1 + T_1 T_2 \omega_{12}^2 + T_2^2 \omega_3^2} \begin{bmatrix} T_2 (\omega_1 \omega_3 T_2 + \omega_2) \\ T_2 (\omega_2 \omega_3 T_2 - \omega_1) \\ 1 + T_2^2 \omega_3^2 \end{bmatrix}, \quad (41)$$

548 which reduces to Bloch's result [1], obtained for  $\omega_2 = 0$ .

549 For the specific case of the OBE on resonance ( $\omega_3 =$   
 550 0), Lapert *et al.* [36] give a geometric interpretation of  
 551 the steady state as points on the surface of an ellipsoid  
 552 satisfying the equation

$$553 \frac{M_x^2 + M_y^2}{T_2} + \frac{(M_z - 1/2)^2}{T_1} = \frac{1}{4T_1}. \quad (42)$$

554 We note here that the result is more general. The com-  
 555 ponents of  $\mathbf{M}_\infty$  in Eq. (41) for the off resonance OBE  
 556 also satisfy Eq. (42), as does the result in Eq. (40a) when  
 557  $\Gamma_{ji} = -\Gamma_{ij}$  and  $R_1 = R_2$ . The magic plane defined in  
 558 that work is also independent of resonance offset,  $\omega_3$ .

### 559 IV. THE CONVENTIONAL BLOCH EQUATION

560 The solutions can be further simplified when applied  
 561 to the specific parameters of the OBE. The approach  
 562 taken here allows us to delve deeper than previous anal-  
 563 yses to obtain additional insight into the nature of the

563 solutions and the constraints that determine root multi-  
 564 plicities. Substituting  $R_1 = R_2$  gives the rates  $R_{ip}$  in  $\Gamma_p$   
 565 of Eq. (32). Define

$$566 R_\delta = \frac{R_2 - R_3}{3} \geq 0, \quad (43)$$

567 since the transverse relaxation rate  $R_2$  is greater than  
 568 or equal to the longitudinal rate  $R_3$  in physical systems.  
 569 Then

$$570 R_{1p} = R_{2p} = R_\delta, \quad R_{3p} = -2R_\delta. \quad (44)$$

571 The coefficients of the characteristic polynomial for  $-\Gamma_p$   
 572 then simplify to

$$573 \tilde{c}_0 = R_\delta [\omega_e^2 - 2R_\delta^2 - 3\omega_3^2] \\ \tilde{c}_1 = \omega_e^2 - 3R_\delta^2. \quad (45)$$

574 The rate  $R_\delta$  provides a convenient and simplifying fre-  
 575 quency scale for characterizing the solutions in the sec-  
 576 tions which follow.

### 577 A. Criteria for the existence of degenerate roots

578 The resulting simpler form for the polynomial coeffi-  
 579 cients makes possible a straightforward analysis of the  
 580 conditions for which there are degeneracies in the roots.  
 581 As discussed in section III A, there is a two-fold degen-  
 582 eracy in the roots for  $\gamma = 1$ . This is equivalent, using  
 583 Eq. (23) for  $\gamma$ , to

$$584 D(\tilde{c}_0, \tilde{c}_1) = (\tilde{c}_0/2)^2 + (\tilde{c}_1/3)^3 \\ = 0. \quad (46)$$

585 The trivial solution  $\tilde{c}_1 = 0 = \tilde{c}_0$  gives a three-fold degen-  
 586 erate root  $z_i = 0$ .

587 Details are deferred to Appendix E, where the exis-  
 588 tence of degenerate roots is characterized in terms of

$$589 \omega_3^2 = \lambda_3 R_\delta^2/3 \quad \text{and} \quad \omega_{12}^2 = \lambda_{12} R_\delta^2/3. \quad (47)$$

590 For each  $\omega_3$  defined by the range  $0 \leq \lambda_3 \leq 1$ , one finds  
 591 two solutions for  $\lambda_{12}$  that satisfy  $D(\tilde{c}_0, \tilde{c}_1) = 0$  and give  
 592 real values for  $\omega_{12}$ . Thus, for each  $\omega_3 \in [0, R_\delta^2/3]$ , there  
 593 are two values of  $\omega_{12}$  that produce degeneracies in the  
 594 roots  $z_i$ . The two solutions for  $\lambda_{12}$  can be expressed  
 595 concisely in the form

$$596 \lambda_{12,i} = \eta_i - \lambda_3 + \frac{9}{4} \quad i = 1, 2 \\ \eta_i = \frac{9}{2} \sqrt{8\lambda_3 + 1} \sin \vartheta_i \\ \vartheta_1 = \text{sgn}(\lambda_3 - \lambda_b) \frac{1}{3} \sin^{-1} \frac{|8\lambda_3^2 + 20\lambda_3 - 1|}{(8\lambda_3 + 1)^{3/2}} \\ \vartheta_2 = \pi/3 - \vartheta_1 \quad (48)$$

597 for  $\lambda_b = \frac{3}{4}(\sqrt{3} - \frac{5}{3})$ . The solutions converge at  $\lambda_3 = 1$  to  
 598  $\eta_1 = \eta_2 = 27/4$ , giving  $\omega_{12}^2 = 8(R_\delta^2/3)$ . Then  $\tilde{c}_1 = 0 = \tilde{c}_0$   
 599 from Eq. (45), giving the three-fold degenerate root  $z_i =$   
 600 0 of Eq. (19) mentioned above.

601 The following simple and explicit criteria characterize  
 602 the poles in Eqs. (15) and (29):

597 (i)  $\omega_3^2 > R_\delta^2/3$

598 There is no real-valued solution for  $\omega_{12}^2$  such that  $\gamma = 1$ ,  
599 i.e.,  $D(\tilde{c}_0, \tilde{c}_1) = 0$ , and, hence, the roots  $z_i$  are dis-  
600 tinct.

601 (ii)  $\omega_3^2 < R_\delta^2/3$

602 There are two different real-valued solutions for  $\omega_{12}^2$  as  
603 a function of  $\lambda_3$  that each give a two-fold degeneracy in  
604 the roots  $z_i$ , requiring the second-order pole solution of  
605 Eq. (38). Otherwise, the roots are distinct.

606 (iii)  $\omega_3^2 = R_\delta^2/3$

607 gives  $\omega_{12}^2 = 8(R_\delta^2/3)$  for  $\lambda_3 = 1$ , resulting in a three-fold  
608 degenerate root  $z_i = 0$  which requires the third-order  
609 pole solution of Eq. (39).

## 610 B. Characterization of the damping

611 Solutions for the roots  $z_i$  are characterized according  
612 to whether the discriminant  $\varpi^2$  of Eq. (22) is positive,  
613 negative, or zero, and can be described, respectively, as  
614 underdamped, overdamped, or critically damped, analo-  
615 gous to a damped harmonic oscillator.

616 The solution for the propagator in the case of degener-  
617 ate roots ( $\gamma = 1$ ) has a term linear in time, characteristic  
618 of a critically damped harmonic oscillator. For a three-  
619 fold degeneracy in the roots, there is an additional term  
620 that is quadratic in the time. The values of  $\omega_3^2$  that allow  
621 degeneracies are restricted to the narrow range paramete-  
622 rized according to  $0 \leq \lambda_3 \leq 1$ , as discussed in the  
623 previous section. The two solutions  $\omega_{12,1}^2$  and  $\omega_{12,2}^2$  for  
624 each  $\omega_3^2$ , as determined from Eqs. (47) and (48), are the  
625 solid curves plotted in Fig. 1.

626 Using the same scaling of  $\omega_3$  and  $\omega_{12}$  as in Eq. (47), we  
627 also have

$$\begin{aligned} \tilde{c}_0(\lambda_{12}, \lambda_3) &= (\lambda_{12} - 2\lambda_3 - 6) R_\delta^3/3 \\ \tilde{c}_1(\lambda_{12}, \lambda_3) &= (\lambda_{12} + \lambda_3 - 9) R_\delta^2/3 \\ \gamma(\lambda_{12}, \lambda_3) &= \frac{9}{2} \frac{|\lambda_{12} - 2\lambda_3 - 6|}{|\lambda_{12} + \lambda_3 - 9|^{3/2}} \end{aligned} \quad (49)$$

628 Solutions in the range  $\omega_{12,1}^2 < \omega_{12}^2 < \omega_{12,2}^2$  bounded by  
629 the critical damping parameters give  $\tilde{c}_1 < 0$  and  $\gamma < 1$ ,  
630 resulting in three distinct real roots and overdamped evo-  
631 lution. The range of bounding values is fairly narrow, be-  
632 coming increasingly so with increasing  $\lambda_3$  and converging  
633 to a single value  $\omega_{12}^2 = 8R_\delta^2/3$  as  $\lambda_3 \rightarrow 1$ , as shown in the  
634 figure.

635 Underdamped, oscillatory solutions are obtained for  
636 all other field values, either  $\omega_3^2 > R_\delta^2/3$  (i.e.,  $\lambda_3 > 1$ ) or  
637  $\omega_{12}^2 \geq \omega_{12,1}^2$  and  $\omega_{12}^2 \leq \omega_{12,2}^2$  for  $\lambda_3 \leq 1$ .

## 638 C. Characterization of the roots

639 The solution to the Bloch equation has a relatively sim-  
640 ple form and can be expressed in terms of a single root,

641  $z_1$ , of the characteristic polynomial for  $-\Gamma_p$ . Although  
642 the solutions for  $z_1$  have also been expressed in relatively  
643 simple functional form, these forms provide little physical  
644 insight. It remains to shed some light on the dependence  
645 of this root on the field  $\omega_e$  and the relaxation rates.

### 646 1. Physical limits of the roots

647 Since the roots  $z_i$  are functions of  $\tilde{c}_0, \tilde{c}_1$  and  $\gamma$ , they  
648 also scale as  $R_\delta$ . The associated decay rates are  $\text{Re}(s_i) =$   
649  $\text{Re}(z_i) - \bar{R}$ , from Eq. (24). Defining

$$\lambda_z = \text{Re}(z_i)/R_\delta. \quad (50)$$

650 and using Eq. (43) for  $R_\delta$  gives the decay rates

$$\begin{aligned} \text{Re}(s_i) &= \lambda_z R_\delta - \bar{R} \\ &= -\frac{(2 - \lambda_z)}{3} R_2 - \frac{(1 + \lambda_z)}{3} R_3. \end{aligned} \quad (51)$$

651 The limiting rates are  $R_2$  and  $R_3$ , which therefore con-  
652 strains  $\lambda_z$  to the range

$$-1 \leq \lambda_z \leq 2. \quad (52)$$

653 The damping has equal contributions from  $R_2$  and  $R_3$   
654 for  $\lambda_z = 1/2$ , with a larger contribution from either  $R_2$   
655 or  $R_3$  if  $\lambda_z$  is less than or greater than  $1/2$ , respectively.

656 The dependence of  $z_1$  on  $\omega_e$  and  $R_\delta$ , calculated accord-  
657 ing to Eqs. (C6), is shown in Fig. 2, where contours of  $\lambda_z$   
658 are plotted as a function of  $\lambda_{12}$  and  $\lambda_3$ . As discussed  
659 earlier, there is only one real root for  $\lambda_3 > 1$ . When  
660  $\lambda_3 \leq 1$ , there is also a single real root for values of  $\lambda_{12}$   
661 outside the narrow bounds that define critical damping.  
662 Within these bounds where the solutions represent over-  
663 damping, any of the three real roots can be designated  
664 as  $z_1$ , with  $z_\pm$  from Eq. (C6c) giving the other two. For  
665  $\omega_{12} = 0$ , the relaxation rate is  $R_3$  (i.e.,  $\lambda_z = 2$ ), indepen-  
666 dent of the offset parameter  $\lambda_3$ , as is well-known. As  $\omega_{12}$   
667 increases for fixed  $\omega_3$ , the relaxation rate approaches  $R_2$   
668 ( $\lambda_z = -1$ ), with the drop-off from  $\lambda_z = 2$  becoming in-  
669 creasingly steep at lower values of  $\omega_3$ . For the other roots  
670 in which  $\text{Re}(z_\pm) = -1/2 z_1$ , the upper limit in Eq. (52)  
671 becomes  $1/2$ .

### 672 2. A linear relation for the roots

673 Equation (19) evaluated at the real root  $z_1$  yields the  
674 linear relation

$$\tilde{c}_0 = -z_1 \tilde{c}_1 - z_1^3. \quad (53)$$

675 The slope and intercept are determined by  $z_1$ . Substi-  
676 tuting the expressions for  $\tilde{c}_0$  and  $\tilde{c}_1$  given in Eq. (49),  
677 rearranging, and collecting terms after writing  $9\lambda_z =$   
678  $6\lambda_z + 3\lambda_z$  gives

$$\lambda_{12} = m_s \lambda_3 + \lambda_{12}^{\text{int}} \quad (54)$$

679 with slope  $m_s$  and intercept  $\lambda_{12}^{\text{int}}$  given by

$$m_s = \frac{2 - \lambda_z}{1 + \lambda_z}, \quad y_{12}^{\text{int}} = 3(2 - \lambda_z)(1 + \lambda_z). \quad (55)$$

680 There is thus a simple graphical representation for the  
681 value of the root  $z_1$  as a function of the physical param-  
682 eters  $\omega_{12}, \omega_3, R_\delta$ . There are a continuum of field values for  
683 a given  $R_\delta$  that give the same  $z_1$ . Lines of constant  $z_1$  as a  
684 function of  $\lambda_{12}$  and  $\lambda_3$  become hyperbolas when Eq. (54)  
685 is rewritten in terms of  $\omega_{12}^2, \omega_3^2, R_\delta^2$  using Eq. (47). A  
686 similar graphical analysis for any cubic polynomial with  
687 real coefficients reveals the parameter space yielding ei-  
688 ther one real and two complex conjugate roots, three real  
689 roots, or degenerate roots.

## 690 V. INTUITIVE REPRESENTATIONS OF 691 SYSTEM DYNAMICS

692 There are few, if any, simple models that interpret the  
693 solutions. In this section, we develop four, three of which  
694 are completely general. The reader is also referred to an  
695 abstract model for the on-resonance ( $\omega_3 = 0$ ) geometrical  
696 structure of OBE dynamics [36].

697 In most cases, the parameters of the Bloch equation  
698 yield three distinct roots for the characteristic polyno-  
699 mial  $p(s)$  of Eq. (17), described as cases (i) and (ii) in  
700 Sec. III A. Exceptions were considered in more detail in  
701 Sec. IV for the OBE. To provide additional physical in-  
702 sight, we develop a straightforward vector model for the  
703 trajectory of  $M(t)$  given by Eq. (10). The model is the  
704 3D analogue to the dynamics of a single damped har-  
705 monic oscillator. As noted in section II A, a parametric  
706 plot of  $\dot{x}(t)$  as a function of  $x(t)$  is a decaying spiral in

707 the phase plane (for underdamped motion). To make  
708 this connection more explicit, we first develop a damped  
709 oscillator model for the Bloch equation. Modeling dis-  
710 sipative processes in this manner provides a new per-  
711 spective within the context of well-understood coupled  
712 harmonic oscillations. Fresh perspectives can yield new  
713 insights. Conversely, the dynamics of a damped oscillator  
714 can be represented by a Bloch-like equation for a single  
715 rotor in two dimensions. The comparison provides insight  
716 towards developing an easily visualized vector model of  
717 Bloch equation dynamics. An alternative vector model  
718 is then also considered.

### 719 A. The Bloch equation as a system of coupled 720 oscillators

721 Any quantum N-level system can be represented as a  
722 system of coupled harmonic oscillators [26], albeit requir-  
723 ing negative or even antisymmetric couplings. The Bloch  
724 equation is perhaps particularly interesting, since it in-  
725 corporates dissipation for the most elementary case, i.e.,  
726 2-level systems.

727 To compare the Bloch equation to Eq. (5) for the  
728 damped harmonic oscillator, first eliminate the inhomog-  
729 eneous term from either equation by the appropriate  
730 shift of coordinates, as discussed previously. Differenti-  
731 ating Eq. (9) with respect to time, writing  $\Gamma$  as the sum  
732 of diagonal matrix  $(\Gamma_d)_{ii} = R_i$  and off-diagonal elements  
733  $\Gamma_{od}$ , and substituting  $\dot{M} = -\Gamma M$  in the resulting  $\Gamma_{od}$   
734 term gives, for  $\Lambda^2 \equiv -\Gamma_{od}\Gamma$ ,

$$\ddot{M}(t) + \Gamma_d \dot{M} + \Lambda^2 M = 0 \quad (56)$$

735 with

$$\Lambda^2 = - \begin{bmatrix} \Gamma_{12}\Gamma_{21} + \Gamma_{13}\Gamma_{31} & \Gamma_{13}\Gamma_{32} + \Gamma_{12}R_2 & \Gamma_{12}\Gamma_{23} + \Gamma_{13}R_3 \\ \Gamma_{31}\Gamma_{23} + \Gamma_{21}R_1 & \Gamma_{12}\Gamma_{21} + \Gamma_{23}\Gamma_{32} & \Gamma_{13}\Gamma_{21} + \Gamma_{23}R_3 \\ \Gamma_{21}\Gamma_{32} + \Gamma_{31}R_1 & \Gamma_{31}\Gamma_{12} + \Gamma_{32}R_2 & \Gamma_{13}\Gamma_{31} + \Gamma_{23}\Gamma_{32} \end{bmatrix}$$

$$\xrightarrow{\text{OBE}} - \begin{bmatrix} -(\omega_2^2 + \omega_3^2) & \omega_1\omega_2 + \omega_3R_2 & \omega_1\omega_3 - \omega_2R_3 \\ \omega_1\omega_2 - \omega_3R_1 & -(\omega_1^2 + \omega_3^2) & \omega_2\omega_3 + \omega_1R_3 \\ \omega_1\omega_3 + \omega_2R_1 & \omega_2\omega_3 - \omega_1R_2 & -(\omega_1^2 + \omega_2^2) \end{bmatrix}. \quad (57)$$

736 Referring to the system of three coupled oscillators in  
737 Fig. 4, the displacement  $r_i$  of mass  $m_i$  from equilibrium  
738 is equal to  $\mathcal{M}_i$ . The natural frequency of  $m_i$  is  $(\Lambda^2)_{ii}$ ,  
739 with associated damping coefficient  $R_i$  multiplying com-  
740 ponent  $\mathcal{M}_i$ . For unit masses, the force equation for  $m_i$   
741 gives  $(\Lambda^2)_{ii} = k_{ii} + \sum_{j \neq i} k_{ij}$  and a simple solution for  
742 the  $k_{ii}$ . Up to this point, a mechanical implementation  
743 of the oscillator system would be possible. However, the  
744 coupling constants  $k_{ij} = -(\Lambda^2)_{ij}$  are asymmetric, which  
745 is a distinguishing feature of two-level systems with dis-

746 sipation and can not be implemented with a system of  
747 springs or other mechanical contrivances.

748 The effect of asymmetric couplings seen more clearly  
749 by keeping  $\Gamma$  intact throughout the previous derivation,  
750 giving

$$\ddot{M}(t) - \Gamma^2 M = 0. \quad (58)$$

751 The elements of  $\Gamma^2$  are similar to those of  $\Lambda^2$ . They dif-  
752 fer by the addition of  $R_i^2$  to each diagonal element of

753  $-\Lambda^2$  and  $R_i\Gamma_{ij}$  to each element of  $-(\Lambda)_{ij}$ . This version  
754 of the oscillator model is in the form of ideal, friction-  
755 less couplings but is, nonetheless, damped. How might  
756 dissipation arise in a “frictionless” system?

757 The couplings  $k_{ij}$  are still asymmetric. For a given  
758 positive  $k_{ij}$ , a positive displacement of mass  $m_j$  results  
759 in a positive force on  $m_i$ . The resulting positive dis-  
760 placement of  $m_i$  provides a different force on  $m_j$  due to  
761  $k_{ji} \neq k_{ij}$ . Energy transferred from  $m_j$  to  $m_i$  is not recip-  
762 rocally transferred back from  $m_i$  to  $m_j$ , and the motion  
763 is quenched. Asymmetric couplings can act as a nega-  
764 tive feedback mechanism to curb system oscillations in  
765 the models represented in Eq. (56) and Eq. (58), similar  
766 to pushing a swing at a nonresonant frequency. Damped  
767 solutions are obtained in both models even if  $R_i \rightarrow 0$  in  
768 the diagonal elements of  $(\Lambda)^2$  or  $\Gamma^2$ .

769 Further insight is obtained by converting the simple  
770 damped oscillator to a system of coupled first-order dif-  
771 ferential equations, i.e., in the same format as the Bloch  
772 equation. Defining a two-element vector  $\mathbf{r}$  with compo-  
773 nents  $r_1 = x - g/\omega_0^2$  and  $r_2 = \dot{x}$  gives

$$\begin{aligned} \dot{\mathbf{r}}(t) &= - \begin{pmatrix} 0 & -1 \\ \omega_0^2 & 2b \end{pmatrix} \mathbf{r}(t) \\ &= -\tilde{\Lambda} \mathbf{r}(t) \end{aligned} \quad (59)$$

774 and solution  $\mathbf{r}(t) = e^{-\tilde{\Lambda}t}\mathbf{r}(0)$ . The propagator is easi-  
775 ly calculated directly or deduced using the solution in  
776 Eq. (6). Either way, the action of the propagator on any  
777 initial state  $\mathbf{r}(0)$  is a decaying spiral in the  $(r_1, r_2)$ -plane,  
778 as discussed previously. One might then wonder whether  
779 there is a similarly simple vector model of system dynam-  
780 ics for the Bloch equation.

## 781 B. Bloch equation dynamics: simple limiting cases

782 As a point of departure, consider first the OBE. For  
783 simple limiting cases, the dynamics are already well  
784 known and readily visualized. In the absence of relax-  
785 ation, i.e., all  $R_i = 0$ , any magnetization vector  $\mathcal{M}$  ro-  
786 tates about the total effective field  $\boldsymbol{\omega}_e$  at constant angular  
787 frequency  $\omega_e$ . The time evolution of a vector under the  
788 action of the propagator has a simple solution in a coor-  
789 dinate system rotated to align one of the axes with the  
790 effective field. The component of  $\mathcal{M}$  along  $\boldsymbol{\omega}_e$  is con-  
791 stant, and the components in the plane perpendicular  
792 to  $\boldsymbol{\omega}_e$  rotate at angular frequency  $\omega_e$  in the plane. By  
793 contrast, the solution for each component  $\mathcal{M}_i(t)$  in the  
794 standard  $(x_1, x_2, x_3)$ -coordinate system is more compli-  
795 cated, and it is not immediately apparent by inspection  
796 that the solution is a rotation.

797 If the relaxation is switched on with equal rates  $R_i =$   
798  $R$ , the diagonal relaxation matrix  $R\mathbb{1}$  commutes with the  
799 remaining rotation matrix. The simplification it affords  
800 has not been acknowledged in any of the previously cited  
801 solutions. The solution is a simple dynamic scaling  $e^{-Rt}$   
802 of the rotating vector  $\mathcal{M}$ , as obtained by Jaynes [31] via

803 a more circuitous route. In addition, for  $\omega_{12} = 0$  and  
804  $R_1 = R_2 \neq R_3$ , the relaxation matrix still commutes with  
805 the rotation about nonzero  $\omega_3$ . The evolution is then in  
806 terms of noninteracting longitudinal and transverse com-  
807 ponents. We have exponential decay  $e^{-R_3t}$  of component  
808  $\mathcal{M}_3$  and decay  $e^{-R_2t}$  of the transverse component  $\mathcal{M}_{12}$ ,  
809 which rotates at angular frequency  $\omega_3$  in the plane per-  
810 pendicular to  $\omega_3$ , as illustrated in Fig. 3a. In the case of  
811 pure relaxation, with all the field components  $\omega_i = 0$ , the  
812 solution is a non-oscillatory exponential decay  $e^{-R_3t}$  for  
813 each component  $\mathcal{M}_i$  along coordinate axis  $x_i$ .

## 814 C. Bloch equation dynamics: a more general 815 vector model

816 With the exception of the above simple cases, there has  
817 been no analogous picture of system dynamics when the  
818 rotation and relaxation do not commute. The combined,  
819 noncommutative action of arbitrary fields and dissipation  
820 rates appears to require something more complex. Yet,  
821 the simple visual model shown in Fig. 3a, which is com-  
822 prised of independent relaxation and rotation elements, is  
823 readily extended to the general case of arbitrary  $\Gamma$  when  
824 viewed in an appropriate coordinate system. This re-  
825 quires the action of the propagator  $e^{-\Gamma t}$  on an arbitrary  
826 vector.

827 The eigensystem for  $\Gamma$  is considered in sections that fol-  
828 low, but one can substitute notation for the partitioned  
829 matrix  $\Gamma_p$  in the expressions which are derived, since, as  
830 defined in Eq. (32), the matrices differ by a constant  $\bar{R}$   
831 times the identity matrix. The difference in the eigenval-  
832 ues is also  $\bar{R}$ , from Eqs. (24) and (25). Thus  $-\Gamma$  and  $-\Gamma_p$   
833 have the same eigenvectors  $\mathbf{s}_i \equiv \mathbf{z}_i$ . Simple analytical ex-  
834 pressions for the eigenvectors and other constituents of  
835 the model are derived in Appendix F. Each (unnormal-  
836 ized) eigenvector, which can assume different analytical  
837 forms depending on the scaling, comprises the columns of  
838  $\text{adj } A(s_i) = \text{adj } A_p(z_i)$ , as derived in Appendix B. This  
839 provides a useful method for calculating an eigenvector,  
840 especially in symbolic form as a function of matrix pa-  
841 rameters.

### 842 1. One real, two complex conjugate roots

843 The solution for each component  $\mathcal{M}_i$  is known to be a  
844 combination of oscillation and bi-exponential decay [6],  
845 as is also evident from the propagator derived in Eq. (15).  
846 The underlying simplicity of the system dynamics can  
847 be demonstrated starting with the eigensystem for  $\Gamma$  (or,  
848 alternatively,  $\Gamma_p$ , as noted above).

849 The real eigenvalue  $s_1$  of  $-\Gamma$  has a real eigenvector  $\mathbf{s}_1$   
850 which can be used as one axis of a physical coordinate  
851 system, but the complex roots  $s_+$  and  $s_- = s_+^*$  have  
852 associated complex eigenvectors  $\mathbf{s}_+$  and  $\mathbf{s}_- = \mathbf{s}_+^*$ .

853 Define the real vectors

$$\begin{aligned}\tilde{\mathbf{s}}_1 &= \mathbf{s}_1, & \tilde{\mathbf{s}}_2 &= \frac{1}{2}(\mathbf{s}_+ + \mathbf{s}_-), & \tilde{\mathbf{s}}_3 &= -\frac{i}{2}(\mathbf{s}_+ - \mathbf{s}_-) \\ & & &= \text{Re}[\mathbf{s}_+], & &= \text{Im}[\mathbf{s}_+].\end{aligned}\quad (60)$$

854 The eigenvectors above are most generally not orthogonal  
855 for arbitrary  $\Gamma$ , but they are linearly independent, given  
856 the distinct eigenvalues. The set  $\{\tilde{\mathbf{s}}_1, \tilde{\mathbf{s}}_2, \tilde{\mathbf{s}}_3\}$  is then also  
857 linearly independent and can be used as an alternative  
858 physical basis for describing the system evolution. The  
859 new coordinate system will most generally also be non-  
860 orthogonal (oblique). System states and operators are  
861 transformed between bases in the usual fashion by a ma-  
862 trix  $P$  comprised of the  $\{\tilde{\mathbf{s}}_i\}$  entered as column vectors.  
863 Vector  $\tilde{\mathcal{M}}$  and the propagator in the new basis are given  
864 by

$$\begin{aligned}\tilde{\mathcal{M}} &= P^{-1}\mathcal{M} \\ e^{-\tilde{\Gamma}t} &= P^{-1}e^{-\Gamma t}P \\ &= e^{-(P^{-1}\Gamma P)t},\end{aligned}\quad (61)$$

865 with  $P$  invertible since the  $\tilde{\mathbf{s}}_i$  are linearly independent.

866 The potentially tedious process of calculating  $e^{-\tilde{\Gamma}t}$   
867 from Eq. (61) can be bypassed, with  $e^{-\tilde{\Gamma}t}$  deduced from  
868 the action of  $\Gamma$  on its eigenvectors (see Appendix F). In  
869 terms of constants

$$\tilde{s}_1 = -(\bar{R} - z_1), \quad \tilde{s}_{23} = -(\bar{R} + z_1/2), \quad (62)$$

870 and  $\varpi$  of Eq. (22), the solution  $\tilde{\mathcal{M}}(t) = e^{-\tilde{\Gamma}t}\tilde{\mathcal{M}}(0)$  for  
871 the time dependence of state vector  $\tilde{\mathcal{M}}$  in the new basis  
872 is found to be

$$\begin{aligned}\tilde{\mathcal{M}}(t) &= \begin{pmatrix} e^{\tilde{s}_1 t} & 0 & 0 \\ 0 & e^{\tilde{s}_{23} t} & 0 \\ 0 & 0 & e^{\tilde{s}_{23} t} \end{pmatrix} \times \\ &\quad \begin{pmatrix} 1 & 0 & 0 \\ 0 & \cos \varpi t & \sin \varpi t \\ 0 & -\sin \varpi t & \cos \varpi t \end{pmatrix} \tilde{\mathcal{M}}(0)\end{aligned}\quad (63)$$

873 Viewed in the  $\{\tilde{\mathbf{s}}_i\}$  coordinate system,  $\mathcal{M}$  evolves ac-  
874 cording to independent, commuting rotation and relax-  
875 ation operators. The component of  $\mathcal{M}$  along  $\tilde{\mathbf{s}}_1$  (i.e.,  
876  $\tilde{\mathcal{M}}_1$ ) decays at the rate  $\tilde{s}_1 = \bar{R} - z_1$ , while components  
877 in the  $(\tilde{\mathbf{s}}_2, \tilde{\mathbf{s}}_3)$ -plane rotate in the plane and decay at the  
878 rate  $\tilde{s}_{23} = \bar{R} + z_1/2$ . Thus, even in the most general case  
879 of three unequal rates  $R_1, R_2, R_3$ , there emerges a single  
880 ‘‘planar’’ relaxation rate  $R_{2s}$  and a new ‘‘longitudinal’’  
881 relaxation rate  $R_{1s}$  defined as

$$R_{1s} = |\tilde{s}_1| = 1/T_{1s} \quad \text{and} \quad R_{2s} = |\tilde{s}_{23}| = 1/T_{2s}. \quad (64)$$

882 Defining  $\tilde{\mathcal{M}}(t)$  as the state  $\mathbf{M}(t) - \mathbf{M}_\infty$  expressed  
883 in the  $\{\tilde{\mathbf{s}}_i\}$  coordinates and working backwards from

884 Eq. (63) gives the Bloch equation in this basis as

$$\begin{aligned}\frac{d}{dt}\tilde{\mathcal{M}}(t) + \tilde{\Gamma}\tilde{\mathcal{M}}(t) &= 0 \\ \tilde{\Gamma} &= \begin{pmatrix} R_{1s} & 0 & 0 \\ 0 & R_{2s} & \varpi \\ 0 & -\varpi & R_{2s} \end{pmatrix}\end{aligned}\quad (65)$$

885 The diagonal matrix consisting of the relaxation rates  
886  $R_{is}$  commutes with the matrix of off-diagonal elements.  
887 This anti-symmetric matrix comprised of  $\pm\varpi$  generates  
888 a rotation about  $\tilde{\mathbf{s}}_1$ , and one immediately obtains the  
889 solution given in Eq. (63). This extends the result of  
890 Sec. VB for the simple OBE with  $\omega_{12} = 0$  and  $R_1 =$   
891  $R_2 \neq R_3$  to completely general Bloch equations.

892 We should emphasize that one has considerable lati-  
893 tude in the choice of  $\tilde{\mathbf{s}}_2$  and  $\tilde{\mathbf{s}}_3$ , since all components in  
894 the plane they define decay at the same rate. Rotating  
895 these coordinate axes in the plane by any angle results in  
896 an equally valid set of axes for representing the dynam-  
897 ics. The vectors  $\tilde{\mathbf{s}}_2$  and  $\tilde{\mathbf{s}}_3$  constructed from a particular  
898 column in the coefficient matrices of Eq. (F7) are related  
899 to axes constructed from one of the other columns by  
900 a rotation (excepting when one of the columns returns  
901 the irrelevant zero vector). By contrast,  $\tilde{\mathbf{s}}_1$  defines the  
902 unique axis for longitudinal decay, so the  $\tilde{\mathbf{s}}_1$  chosen from  
903 different columns must be related by a scale factor.

904 Note also that the rotation in the plane is *not* at a con-  
905 stant angular frequency  $\varpi$  unless  $\tilde{\mathbf{s}}_2$  and  $\tilde{\mathbf{s}}_3$  are orthog-  
906 onal. A component aligned with  $\tilde{\mathbf{s}}_2$  rotates to  $\tilde{\mathbf{s}}_3$  during  
907 a time defined by the condition  $\varpi t = \pi/2$ , then rotates  
908 from there to  $-\tilde{\mathbf{s}}_2$  in the same time. In an oblique coor-  
909 dinate system, the rotations are through different angles  
910 in the same time, so clearly the angular frequency of the  
911 rotation in physical space is not constant.

912 Although Eq. (63) is perhaps reminiscent of a normal  
913 mode analysis, recall that the normal mode coordinates  
914 are the eigenvectors of  $-\Gamma$ , two of which are complex and,  
915 hence, unphysical. The physical  $\{\tilde{\mathbf{s}}_i\}$  coordinate system  
916 is comprised of linear combinations of the eigenvectors,  
917 which have distinct eigenvalues. The  $\{\tilde{\mathbf{s}}_i\}$  as a set are  
918 therefore not the eigenvectors of  $-\Gamma$  (although  $\{\tilde{\mathbf{s}}_1\}$  is,  
919 by definition).

## 2. Three real roots

921 In this case, all the eigenvectors are real and the new  
922 basis is simply the eigenbasis  $\{\mathbf{s}_1, \mathbf{s}_2, \mathbf{s}_3\}$  obtained from  
923 the roots

$$s_i = -(\bar{R} - z_i) \quad (66)$$

924 defined in Eq. (24). The real roots  $z_i$  are obtained for  
925  $\varpi^2 < 0$  in Eq. (22). Substituting  $\varpi \rightarrow i\mu$  in Eq. (21)  
926 gives  $z_{2,3} = -1/2 z_1 \mp \mu$ .

927 The matrix  $\Gamma$  is obviously diagonal in its eigenbasis,

and, by extension, so is the propagator in this basis. Thus

$$\tilde{\mathcal{M}}(t) = \begin{pmatrix} e^{s_1 t} & 0 & 0 \\ 0 & e^{s_2 t} & 0 \\ 0 & 0 & e^{s_3 t} \end{pmatrix} \tilde{\mathcal{M}}(0) \quad (67)$$

Each component of  $\mathcal{M}$  along  $\tilde{\mathbf{s}}_i$  decays at the rate determined by  $s_i$ . In contradistinction to the rates that emerge from the oscillatory solutions, here, even in the typical case of equal transverse rates  $R_1 = R_2$  and longitudinal rate  $R_3$ , we find three distinct rates

$$R_{is} = |s_i| = 1/T_{is} \quad (68)$$

due to the coupling of the field with the relaxation processes.

Given  $e^{-\tilde{\Gamma}t}$  as obtained in Eq. (63) or (67), the propagator in the standard coordinate basis is  $e^{-\Gamma t} = P e^{-\tilde{\Gamma}t} P^{-1}$  from Eq. (61). One obtains a simple, factored solution for the propagator derived by different methods in Sec. III. The physical interpretation of the dynamics is correspondingly simple, with oscillation frequencies and decay rates hinging upon the primary real root  $z_1$ . The dependence of this root on the fields and relaxation rates has been shown previously in Fig. 2.

### 3. Degenerate roots

The vector model approach to obtaining the propagator is only applicable to the case of distinct eigenvalues. Degenerate eigenvalues do not give the linearly independent eigenvectors necessary to define a new coordinate system. However, the degeneracies are a relatively trivial component of the parameter space, at least for the OBE, as shown in Fig. 1. Moreover, the solution has to be continuous as the degeneracies are approached, with a smooth transition from oscillatory, decaying solutions to pure decay as one crosses the parameter-space boundary identifying the degenerate solutions.

### 4. Discussion and representative examples

The solutions of Sec. III are represented in the standard coordinate system, expressed in general form for arbitrary driving matrix  $\Gamma$ . Here, they are applied to specific physical examples applicable to the OBE, with  $R_1 = R_2$ . The trajectories of initial states under the action of the propagator are plotted to illustrate the underlying simplicity of the dynamics and corroborate the alternative coordinate system that defines the vector model. Parameters for the examples are chosen to demonstrate the damping and rotation that are characteristic of the dynamics for all but a small region of the parameter space. A purely damped solution and model dynamics given by Eq. (67) is rather featureless, by comparison. Unless stated otherwise, the first column of  $\text{adj } A_p$  is chosen to calculate the eigenvectors and coordinate basis  $\{\tilde{\mathbf{s}}_i\}$ .

*a. Free precession,  $\boldsymbol{\omega}_e = (0, 0, \omega_3)$*  When the only field in the rotating frame is the offset from resonance,  $\omega_3$ , the matrix  $\Gamma_p$  is the sum of a diagonal relaxation matrix and the matrix which generates a rotation about  $\omega_3$ . Since they commute, the propagator factors into the product of exponential decay and a rotation, leading to the standard interpretation of the dynamics discussed previously in Sec. V B. This example also provides a simple illustration of the more general vector model. The eigenvalues are easily obtained as  $z_1 = 2R_\delta$  and  $z_\pm = -R_\delta \pm i\omega_3$ . Then Eq. (F6) gives, upon identifying  $\varpi \equiv \omega_3$  and eliminating common factors in individual columns,

$$\begin{aligned} \tilde{\mathbf{s}}_1 &\leftarrow \begin{pmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 1 \end{pmatrix} & \tilde{\mathbf{s}}_2 &\leftarrow \begin{pmatrix} \omega_3 & -3R_\delta & 0 \\ 3R_\delta & \omega_3 & 0 \\ 0 & 0 & 0 \end{pmatrix} \\ \tilde{\mathbf{s}}_3 &\leftarrow \begin{pmatrix} 3R_\delta & \omega_3 & 0 \\ -\omega_3 & 3R_\delta & 0 \\ 0 & 0 & 0 \end{pmatrix}. \end{aligned} \quad (69)$$

As noted earlier, there is always only one unique nonzero result for  $\tilde{\mathbf{s}}_1$ , with any apparent differences between columns simply a matter of scale. The nonzero columns for  $\tilde{\mathbf{s}}_2$  are orthogonal, as are those of  $\tilde{\mathbf{s}}_3$ . The columns thus differ, as expected, by a rotation in the  $(\tilde{\mathbf{s}}_2, \tilde{\mathbf{s}}_3)$ -plane, in this case by  $90^\circ$ . Choosing the second column and a left-handed rotation by  $\phi = \tan^{-1}(3R_\delta/\omega_3)$  or the first column and a right-handed rotation by  $90 - \phi$  gives the more typical result  $\tilde{\mathbf{s}}_2 = (0, 1, 0)$  and  $\tilde{\mathbf{s}}_3 = (1, 0, 0)$  depicted in Fig. 3a. The model dynamics for an initial state  $\mathcal{M}_0$  is a spiral about  $\boldsymbol{\omega}_e$ , which is aligned along the  $z$ -axis, with rotation at constant angular frequency  $\omega_e$  in the  $(x, y)$ -plane, as required. The relaxation rate obtained from Eq. (51) or Eq. (62) for  $z_1 = 2R_\delta$ , with  $\lambda_z = 2$ , is  $R_{1s} = R_3$ , while the roots  $z_\pm$  with  $\lambda_z = -1$  give  $R_{2s} = R_2$ , as expected.

*b. On resonance,  $\boldsymbol{\omega}_e = (\omega_1, \omega_2, 0)$*  The effective field is now in the transverse plane instead of along the  $z$ -axis as in the preceding example. Yet there has been no visual intuition of the dynamics for this simple change in the orientation of  $\boldsymbol{\omega}_e$ . This is the simplest example for the new vector model. What does it predict?

The root  $z_1 = -R_\delta$ , and  $\varpi^2 = \omega_e^2 - (3/2R_\delta)^2$  from Eq. (G14). The associated eigenvector  $\tilde{\mathbf{s}}_1$  is obtained by inspection from Eq. (F5), with  $\tilde{\mathbf{s}}_2$  and  $\tilde{\mathbf{s}}_3$  obtained from Eqs. (F6) and (F7), giving

$$\tilde{\mathbf{s}}_1 = \begin{pmatrix} \omega_1 \\ \omega_2 \\ 0 \end{pmatrix} \quad \tilde{\mathbf{s}}_2 = \begin{pmatrix} -\omega_2 \\ \omega_1 \\ -\frac{3}{2}R_\delta \end{pmatrix} \quad \tilde{\mathbf{s}}_3 = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}. \quad (70)$$

Thus, on resonance, the propagator still generates a spiral about the effective field  $\boldsymbol{\omega}_e = \tilde{\mathbf{s}}_1$  with precession in the  $(\tilde{\mathbf{s}}_2, \tilde{\mathbf{s}}_3)$ -plane orthogonal to  $\tilde{\mathbf{s}}_1$ . However, as considered in section V C 1, the rotation frequency driven by  $\varpi$  is not constant, since  $\tilde{\mathbf{s}}_2$  is not perpendicular to  $\tilde{\mathbf{s}}_3$ . The deviation from orthogonality, determined by the third component of  $\tilde{\mathbf{s}}_2$ , is small for fields that are large

1020 compared to  $R_\delta$ . The respective decay rates  $R_{1s}$  and  $R_{2s}$  1078  
 1021 are  $R_2$  and  $1/2(R_2 + R_3)$ , using  $\lambda_z = -1$  and  $\lambda_z = 1/2$  as 1079  
 1022 determined from  $z_1$  and  $-z_1/2$ . Components along  $\tilde{\mathbf{s}}_1$ , 1080  
 1023 i.e., in the  $(x, y)$ -plane, decay at the usual spin-spin relax-  
 1024 ation rate, as would be expected. Components rotating  
 1025 in the plane orthogonal to  $\tilde{\mathbf{s}}_1$  experience equal influence, 1081  
 1026 on average, from their projection onto the longitudinal  
 1027  $z$ -axis defining  $\omega_3$  and their projection into the  $(x, y)$ - 1082  
 1028 plane, so one might predict from the model that they 1083  
 1029 decay at the average of the usual spin-spin and longitu- 1084  
 1030 dinal relaxation rates. These values for the decay rates 1085  
 1031 have been obtained previously as elements of the solu- 1086  
 1032 tion in the standard coordinate system [6] without the 1087  
 1033 physical interpretation presented here.

1034 The trajectory for an initial state  $\mathcal{M}_0$  due to the action 1089  
 1035 of propagator  $e^{-\Gamma t}$  with  $\boldsymbol{\omega}_e = (\omega_1, 0, 0)$  and nonzero re- 1090  
 1036 laxation is shown in Fig. 3b. Values of the parameters are 1091  
 1037 given in the caption. For nonzero  $\omega_2$ , the figure is sim- 1092  
 1038 ply rotated about the  $z$ -axis by angle  $\phi = \tan^{-1}(\omega_2/\omega_1)$ . 1093  
 1039 The state  $\mathcal{M}_0$  has been chosen with equal components 1094  
 1040 parallel and orthogonal to  $\boldsymbol{\omega}_e$  to most clearly illustrate 1095  
 1041 the dynamics predicted by the vector model. The slight 1096  
 1042 misalignment between  $\tilde{\mathbf{s}}_2$  and the  $y$ -axis, which makes  
 1043  $\tilde{\mathbf{s}}_2$  and  $\tilde{\mathbf{s}}_3$  nonorthogonal, is evident in the figure and be-  
 1044 comes more prominent as the magnitude of the field,  $\omega_{12}$ ,  
 1045 is reduced relative to  $R_\delta$ .

1046 *c. Off resonance, general  $\boldsymbol{\omega}_e$*  Most generally,  $\tilde{\mathbf{s}}_1$  is  
 1047 not aligned with  $\boldsymbol{\omega}_e$ . Dividing column  $j$  of the matrix in  
 1048 Eq. (F5) by (nonzero)  $\omega_j$  quantifies the degree to which  
 1049  $\tilde{\mathbf{s}}_1$  deviates from  $\boldsymbol{\omega}_e$  due to the coupling between the fields  
 1050 and the relaxation rates  $R_i$ . The result is an expression  
 1051 of the form  $\mathbf{s}_1 = \boldsymbol{\omega}_e + \delta\mathbf{v}$ , where vector  $\delta\mathbf{v}$  is comprised  
 1052 of the second term in each row of the  $j^{\text{th}}$  column divided  
 1053 by  $\omega_j$ .

1054 In addition,  $\tilde{\mathbf{s}}_1$  is typically not orthogonal to the  
 1055  $(\tilde{\mathbf{s}}_2, \tilde{\mathbf{s}}_3)$ -plane. One then has to further modify intuitions  
 1056 developed from orthogonal coordinate systems. For ex- 1097  
 1057 ample, in Fig. 3c,  $\mathcal{M}_0$  is aligned with the normal to the 1098  
 1058  $(\tilde{\mathbf{s}}_2, \tilde{\mathbf{s}}_3)$ -plane. It therefore has no orthogonal projection 1099  
 1059 in the plane and might naively be expected to have no 1100  
 1060 evolution in the plane. However,  $\tilde{\mathbf{s}}_1$  is distinctly different 1101  
 1061 than the normal, and  $\mathcal{M}_0$  is the vector sum of a compo- 1102  
 1062 nent along  $\tilde{\mathbf{s}}_1$  and a component parallel to the plane, 1103  
 1063 which are the quantities relevant for the vector model. As 1104  
 1064 shown in the figure, the parallel component rotates and 1105  
 1065 decays in the plane while the component along  $\tilde{\mathbf{s}}_1$  strictly 1106  
 1066 decays. Similarly,  $\mathcal{M}_0$  orthogonal to  $\tilde{\mathbf{s}}_1$  as in Fig. 3d 1107  
 1067 nonetheless has a component along  $\tilde{\mathbf{s}}_1$  in the oblique co- 1108  
 1068 ordinates. This component decays to generate the spiral 1109  
 1069 shown in the figure.

1070 Contrast this with the dynamics viewed in standard co- 1111  
 1071 ordinates, where the solution for each component  $\mathcal{M}_i(t)$  1112  
 1072 is an oscillation combined with relaxation at two separate 1113  
 1073 rates. As in simpler examples, it can be decoupled into 1114  
 1074 two independent dynamical systems, one of which rotates 1115  
 1075 in a plane and decays at one rate and another which de- 1116  
 1076 cays along a fixed axis, albeit in an oblique coordinate 1117  
 1077 system.

The deviation of  $\tilde{\mathbf{s}}_1$  from the normal to the plane is  
 1079 quantified in Appendix F for  $\boldsymbol{\omega}_{12}$  of either  $x$ - or  $y$ -phase  
 1080 and for  $\omega_1 = \omega_2 = \omega_3$ .

#### D. Alternative vector model

1082 The Bloch equation, considered here in matrix form,  
 1083 is typically represented in vector form. Its physics is the  
 1084 torque on a magnetic moment in a magnetic field subject  
 1085 to relaxation of the magnetization. The effects of this  
 1086 physics on the OBE solution can be made more explicit  
 1087 by returning to the original vector operations, motivated  
 1088 by the treatment in Jaynes [31] for the rotation of a vector  
 1089 about the field.

1090 Partition  $\Gamma_p$  into its diagonal elements  $R_{ip}$  and off-  
 1091 diagonal  $\omega_i$ , writing  $\Gamma_p = \mathcal{R}_p + \Omega$ . The diagonal matrix  
 1092  $\mathcal{R}_p$  scales each component  $\mathcal{M}_i$  of a vector  $\mathcal{M}$  by  $R_{ip}$ , and  
 1093  $\Omega$  implements the cross product  $(-\boldsymbol{\omega}_e \times \cdot)$ . According to  
 1094 Eq. (30), the propagator acting on  $\mathcal{M}$  generates three  
 1095 separate vectors  $\mathbf{v}_n = \Gamma_p^n \mathcal{M}$ , ( $n = 0, 1, 2$ ), which can be  
 1096 represented starting with  $\mathbf{v}_0 = \mathcal{M}$  as

$$\begin{aligned} \Gamma_p \mathcal{M} &= (\mathcal{R}_p + \Omega) \mathbf{v}_0 \\ &= (\mathcal{R}_p \mathcal{M}) - (\boldsymbol{\omega}_e \times \mathcal{M}) \\ &= \mathbf{v}_1 \end{aligned}$$

$$\begin{aligned} \Gamma_p^2 \mathcal{M} &= (\mathcal{R}_p + \Omega) \mathbf{v}_1 \\ &= (\mathcal{R}_p^2 \mathcal{M}) - \mathcal{R}_p (\boldsymbol{\omega}_e \times \mathcal{M}) - \boldsymbol{\omega}_e \times (\mathcal{R}_p \mathcal{M}) + \\ &\quad \boldsymbol{\omega}_e \times (\boldsymbol{\omega}_e \times \mathcal{M}) \\ &= (\mathcal{R}_p^2 \mathcal{M}) - \mathcal{R}_p (\boldsymbol{\omega}_e \times \mathcal{M}) - \boldsymbol{\omega}_e \times (\mathcal{R}_p \mathcal{M}) + \\ &\quad \boldsymbol{\omega}_e (\boldsymbol{\omega}_e \cdot \mathcal{M}) - \omega_e^2 \mathcal{M} \\ &= \mathbf{v}_2 \end{aligned} \tag{71}$$

1097 Each succeeding  $\mathbf{v}_n$  is a nonuniform scaling of the pre-  
 1098 vious  $\mathbf{v}_{n-1}$  added to a vector  $(\mathbf{v}_{n-1} \times \boldsymbol{\omega}_e)$  that is or-  
 1099 thogonal to  $\mathbf{v}_{n-1}$ . The time dependence of  $\mathbf{v}_n$  is given  
 1100 by the associated term  $a_n(t)e^{-\tilde{R}t}$  found in Eqs. (37–39).  
 1101 The  $a_n(t)$  are factored as the product of a matrix  $W(z_1)$   
 1102 and vector  $\mathbf{u}(t)$ . Each  $a_n(t)$  is merely a different linear  
 1103 combination of the same three simple functions  $u_i(t)$  that  
 1104 comprise the components of  $\mathbf{u}$ , weighted according to the  
 1105 corresponding elements from row  $n$  of the matrix  $W$ . A  
 1106 given  $\mathbf{v}_n(t)$  thus maintains a fixed orientation, changing  
 1107 length with a time dependence consisting of the different  
 1108 weightings of the  $u_i(t)$  for different  $\mathbf{v}_n$ . The trajectory  
 1109  $\mathcal{M}(t) = \sum_n \mathbf{v}_n(t)$  can thus be represented in terms of  
 1110 the decaying oscillations of three vectors fixed in place.

1111 Alternatively, expand  $(\mathbb{1}, \Gamma_p, \Gamma_p^2) W(z_1) \mathbf{u}(t)$  and group  
 1112 terms of the same time dependence  $u_i(t)$ . The propaga-  
 1113 tor applied to  $\mathcal{M}$  gives three different linear combinations  
 1114 of the  $\mathbf{v}_n$ , with a time dependence  $u_i(t)$  for the  $i^{\text{th}}$  com-  
 1115 bination. The resulting interpretation of  $\mathcal{M}(t)$  is similar  
 1116 to the previous paragraph, but the functional form of the  
 1117 decaying oscillations is simpler using this different set of  
 1118 vectors.

## VI. CONCLUSION

1119  
 1120 A more comprehensive solution of the Bloch equation  
 1121 has been presented together with intuitive visual models  
 1122 of its dynamics. The solution is valid for arbitrary system  
 1123 parameters, yet is simpler than previous solutions. It  
 1124 can be expressed as the product of three separate terms:  
 1125 one which depends directly on the physical parameters  
 1126 of the problem through the driving matrix  $\Gamma$ , a term  
 1127 that depends on its eigenvalues, and a term that gives  
 1128 the time dependence, which in turn is solely a function  
 1129 of the eigenvalues. Moreover, the time evolution of the  
 1130 system as a function of the physical parameters has been  
 1131 made more explicit and apparent.

1132 System dynamics depend critically on the eigenvalues,  
 1133 with (i) oscillatory, underdamped evolution for one real  
 1134 and two complex-conjugate values, (ii) non-oscillatory,  
 1135 overdamped evolution for three real values, and (iii)  
 1136 non-oscillatory, critically damped evolution for doubly  
 1137 or triply degenerate (real) values. The damping rates  
 1138 and the frequency driving the oscillatory behavior have  
 1139 been reduced to simple functions of a primary, real eigen-  
 1140 value that is obtained as a straightforward function of  
 1141 the system parameters. For the conventional Bloch equa-  
 1142 tion, simple quantitative relations have been derived that  
 1143 delineate the three categories of dynamical behavior in  
 1144 terms of the physical parameters. A linear relation has  
 1145 also been derived in this case relating critical system  
 1146 parameters to the primary eigenvalue, which provides

1147 a straightforward graphical realization of the damping  
 1148 rates and frequency for a given physical configuration.

1149 An intuitive dynamical model developed here trans-  
 1150 forms the general Bloch equation to a frame in which  
 1151 damping commutes with a rotation, providing a prop-  
 1152 agator for the time evolution of the system that is the  
 1153 product of a rotation times a decay, in either order. The  
 1154 decay rates in this frame result from interaction/coupling  
 1155 of the fields with the spin-lattice and spin-spin relaxation  
 1156 processes. The model was motivated by well-known vi-  
 1157 sual models for simple conventional cases such as equal  
 1158 relaxation rates or free precession (no fields transverse  
 1159 to the longitudinal,  $z$ -axis). The system state in such  
 1160 cases rotates about the effective field, with concurrent ex-  
 1161 ponential decay of the longitudinal and transverse com-  
 1162 ponents. The extended model retains the same essen-  
 1163 tial features: rotation, exponential decay of the invariant  
 1164 component in the rotation (analogous to the longitudinal  
 1165 axis), and a separate decay of the rotating components  
 1166 in an analogous transverse plane. The model also in-  
 1167 cludes solely damped solutions (i.e., no rotation). An  
 1168 alternative vector model has also been provided, as well  
 1169 as a representation of the Bloch equation as a system of  
 1170 coupled, damped harmonic oscillators. The net result of  
 1171 the solutions and models is a framework for more direct  
 1172 physical insight into the dynamics of the Bloch equation.

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## Appendix A: Proof of Eq. (27)

1176 Consider a general  $3 \times 3$  matrix  $\Upsilon$  with characteristic  
1177 polynomial  $p(s) = \det(s\mathbb{1} - \Upsilon) = \sum_{j=0}^3 c_j s^j$  and poly-  
1178 nomials  $p_j(s)$  derived from it as defined in Eq. (31). The  
1179 claim is that

$$\text{adj}(s\mathbb{1} - \Upsilon) = \sum_{j=0}^2 p_j(s)\Upsilon^j. \quad (\text{A1})$$

1181 Note first that  $\sum_{j=0}^2 p_j(s)\Upsilon^j = \sum_{j=0}^2 p_j(\Upsilon)s^j$ , as is eas-  
1182 ily verified by expanding the terms. Then Eq. (12) for  
1183 the inverse matrix  $(s\mathbb{1} - \Upsilon)^{-1} = \text{adj}(s\mathbb{1} - \Upsilon)/p(s)$  gives

$$\begin{aligned} p(s)\mathbb{1} &= (s\mathbb{1} - \Upsilon)\text{adj}(s\mathbb{1} - \Upsilon) \\ &= s \sum_{j=0}^2 p_j(s)\Upsilon^j - \Upsilon \sum_{j=0}^2 p_j(\Upsilon)s^j. \end{aligned} \quad (\text{A2})$$

1184 For the  $j = 0$  term, make the substitution  $s p_0(s)\mathbb{1} =$   
1185  $[p(s) - c_0]\mathbb{1}$  using Eq. (31). Similarly,  $\Upsilon p_0(\Upsilon) = p(\Upsilon) -$   
1186  $c_0\mathbb{1}$ . But  $p(\Upsilon) = 0$  from the Cayley-Hamilton theorem,  
1187 and we are left with  $p(s)$  on both sides of the equation  
1188 plus the remaining sum, which is easily shown to equal  
1189 zero upon evaluating  $p_1(x) = c_2 + x^2$  and  $p_2(x) = 1$  for  
1190  $x = s$  and  $x = \Upsilon$ .

## 1191 Appendix B: An Alternative Method for Calculating 1192 an Eigenvector

1193 Equation (A2) suggests the modest result, at the least  
1194 not widely recognized, that an eigenvector  $\mathbf{v}$  correspond-  
1195 ing to a distinct eigenvalue  $v$  of operator  $\Upsilon$  can be ob-  
1196 tained as

$$\mathbf{v} \in \text{adj}(v\mathbb{1} - \Upsilon), \quad (\text{B1})$$

1197 seen as follows. The characteristic polynomial  $p(s)$  equals  
1198 zero for eigenvalue  $s = v$ . Then

$$\begin{aligned} p(s) &= (s\mathbb{1} - \Upsilon)\text{adj}(s\mathbb{1} - \Upsilon) \\ 0 &= (v\mathbb{1} - \Upsilon)\text{adj}(v\mathbb{1} - \Upsilon) \\ \therefore \Upsilon \text{adj}(v\mathbb{1} - \Upsilon) &= v \text{adj}(v\mathbb{1} - \Upsilon) \end{aligned} \quad (\text{B2})$$

1200 Only a single column of the adjugate matrix is required,  
1201 so the method is fairly efficient. However, the trivial zero  
1202 eigenvector solution can be one of the columns, requiring  
1203 further completion of the adjugate to obtain the desired  
1204 eigenvector.

1205 For the case of degenerate eigenvalues, the method  
1206 is incomplete. When the nullity (dimension of the null  
1207 space) of  $(v\mathbb{1} - \Upsilon)$  equals the order of the degeneracy,  $k$   
1208 (i.e, the rank equals the dimension of the operator,  $n$ , mi-  
1209 nus  $k$ ), there are  $k$  distinct eigenvectors, but the method  
1210 fails, returning only the zero eigenvector. If there is not a  
1211 complete set of eigenvectors (the degenerate eigenvalue is  
1212 defective in that the nullity is less than  $k$ ), and the rank  
1213 is greater than  $(n - k)$ , the method appears to return the  
1214 eigenvectors that exist, but one rarely needs these, since  
1215 the matrix  $\Upsilon$  is not diagonalizable in this case.

## Appendix C: Cubic Polynomials with Real Coefficients

1217 The standard solutions for the three roots of Eq. (19),  
1218 cast here in terms of

$$\Lambda_{\pm} = [-\tilde{c}_0/2 \pm \sqrt{(\tilde{c}_0/2)^2 + (\tilde{c}_1/3)^3}]^{1/3}, \quad (\text{C1})$$

1219 are

$$\begin{aligned} z &= \left\{ \Lambda_+ + \Lambda_-, -\frac{\Lambda_+ + \Lambda_-}{2} \pm \sqrt{-3} \frac{\Lambda_+ - \Lambda_-}{2} \right\}, \\ &= \{z_1, z_{\pm}\}. \end{aligned} \quad (\text{C2})$$

1220 These solutions can be consolidated in a convenient form  
1221 that does not appear to have been employed heretofore.

1222 Substituting  $(\Lambda_+ - \Lambda_-) = [(\Lambda_+ + \Lambda_-)^2 - 4\Lambda_+\Lambda_-]^{1/2}$  and  
1223 noting  $\Lambda_+\Lambda_- = -\tilde{c}_1/3$  gives

$$\begin{aligned} z_1 &= \Lambda_+ + \Lambda_- \\ z_{\pm} &= -\frac{1}{2}z_1 \pm i\sqrt{3} \sqrt{\left(\frac{z_1}{2}\right)^2 + \frac{\tilde{c}_1}{3}} \\ &= -\frac{1}{2}z_1 \pm i\varpi \end{aligned} \quad (\text{C3})$$

1224 in terms of a discriminant

$$\varpi^2 = 3[(z_1/2)^2 + \tilde{c}_1/3]. \quad (\text{C4})$$

1225 Any polynomial with real coefficients has at least one  
1226 real root. Therefore  $\varpi^2 > 0$  gives one real and two com-  
1227 plex conjugate roots, with three real roots resulting from  
1228  $\varpi^2 \leq 0$ .

1229 One can then employ simple forms for  $z_1$  [37, 38]. The  
1230 number of conditional dependencies relating  $z_1$  in the  
1231 cited references to the signs and relative magnitudes of  
1232  $\tilde{c}_1$  and  $\tilde{c}_0$  are simplified here in terms of

$$\begin{aligned} \alpha &= |\tilde{c}_1/3| \\ \beta &= |\tilde{c}_0/2| \\ \gamma &= \frac{\beta}{\alpha^{3/2}}. \end{aligned} \quad (\text{C5})$$

1233 Then the roots can be calculated according to their do-

1234 main of applicability as

$$\tilde{c}_1 > 0$$

$$\begin{aligned} \varphi &\equiv \frac{1}{3} \sinh^{-1} \gamma \\ x_1 &\equiv \operatorname{sgn}(\tilde{c}_0) \sinh \varphi \\ z_1 &= -2\sqrt{\alpha} x_1 \\ \varpi &= \sqrt{3\alpha(x_1^2 + 1)} = \sqrt{3\alpha} \cosh \varphi \\ z_{\pm} &= \sqrt{\alpha} x_1 \pm i \varpi \end{aligned} \quad (\text{C6a})$$

$$\tilde{c}_1 < 0$$

$$\begin{aligned} \gamma &\geq 1 \\ \varphi &\equiv \frac{1}{3} \cosh^{-1} \gamma \\ x_1 &\equiv \operatorname{sgn}(\tilde{c}_0) \cosh \varphi \\ z_1 &= -2\sqrt{\alpha} x_1 \\ \varpi &= \sqrt{3\alpha(x_1^2 - 1)} = \sqrt{3\alpha} \sinh \varphi \\ z_{\pm} &= \sqrt{\alpha} x_1 \pm i \varpi \\ &\rightarrow \sqrt{\alpha} x_1 \quad \gamma = 1 \end{aligned} \quad (\text{C6b})$$

$$\begin{aligned} \gamma &\leq 1 \\ \varphi &\equiv \frac{1}{3} \cos^{-1} \gamma \\ x_1 &\equiv \operatorname{sgn}(\tilde{c}_0) \cos \varphi \\ z_1 &= -2\sqrt{\alpha} x_1 \\ \varpi &= i\sqrt{3\alpha(1 - x_1^2)} = i\sqrt{3\alpha} \sin \varphi \\ &= i\mu \\ z_{\pm} &= \sqrt{\alpha} x_1 \pm \mu \quad \text{or, alternatively} \end{aligned} \quad (\text{C6c})$$

$$\begin{aligned} \varphi &\equiv \frac{1}{3} \sin^{-1} \gamma \\ x_1 &\equiv \operatorname{sgn}(\tilde{c}_0) \sin \varphi \\ z_1 &= +2\sqrt{\alpha} x_1 \\ \varpi &= i\sqrt{3\alpha(1 - x_1^2)} = i\sqrt{3\alpha} \cos \varphi \\ &= i\mu \\ z_{\pm} &= -\sqrt{\alpha} x_1 \pm \mu \end{aligned} \quad (\text{C6d})$$

$$\tilde{c}_1 = 0$$

$$\begin{aligned} z_1 &= -\operatorname{sgn}(\tilde{c}_0) \sqrt[3]{|b|} \\ z_{\pm} &= -\frac{1}{2} z_1 (1 \pm i\sqrt{3}) \end{aligned} \quad (\text{C6e})$$

1235 For  $(\tilde{c}_1 > 0)$  or  $(\tilde{c}_1 < 0$  and  $\gamma > 1)$ , there is one real  
1236 root and complex conjugate roots  $z_{\pm}$ . For  $\tilde{c}_1 < 0$ ,  $\gamma < 1$ ,  
1237 there are three real roots. When  $\gamma = 1$ , both Eq. (C6b)  
1238 and Eq. (C6c) give  $\varphi = 0 = \varpi$  and two degenerate roots  
1239  $z_+ = z_-$ . Equation (C6d) reorders the roots relative to  
1240 Eq. (C6c), so that the nondegenerate root for the case  
1241  $\gamma = 1$  is one of the  $z_{\pm}$ . Results for  $\tilde{c}_1 = 0$  are straight-  
1242 forwardly obtained from Eq. (C2) and Eq. (21), or using  
1243 the expressions in (C6a) and (C6b), with  $\sinh^{-1} \gamma \rightarrow$   
1244  $\cosh^{-1} \gamma \rightarrow \ln(2\gamma)$  in the limit  $\gamma \rightarrow \infty$ . Terms then re-  
1245 sult that are multiplied by  $\sqrt{\alpha}$ , canceling the singularity  
1246 at  $\tilde{c}_1 = 0$ . For the case  $\tilde{c}_1 = 0 = \tilde{c}_0$ , there are three equal  
1247 roots  $z_i = 0$ .

1248

## Appendix D: Calculation of $e^{-\Gamma_P t}$

1249

### 1. First-order pole

1250 Consider the case of one real root  $z_1$  and two com-  
1251 plex conjugate roots  $z_{2,3} = -1/2 z_1 \pm i \varpi$ , as given by  
1252 Eq. (21), with  $\varpi^2 = 3(z_1/2)^2 + \tilde{c}_1 > 0$ . Two of the terms  
1253 in Eq. (35) for the Cayley-Hamilton coefficients  $a_j(t)$  are  
1254 therefore also complex conjugates of each other, of the  
1255 form  $w + w^* = 2 \operatorname{Re}(w)$  for the sum of  $w$  and its complex  
1256 conjugate. Then

$$a_j(t) = \frac{q_j(z_1)}{q'(z_1)} e^{z_1 t} + 2 \operatorname{Re} \left[ \frac{q_j(z_2)}{q'(z_2)} e^{z_2 t} \right], \quad (\text{D1})$$

1257 with  $q'(z_i) = \prod_{j \neq i} (z_i - z_j)$ , as discussed in section III D.  
1258 Evaluating the  $q'(z_i)$  and using Eq. (22) for  $\varpi^2$  gives

$$\begin{aligned} q'(z_1) &= (z_1 - z_2)(z_1 - z_3) \\ &= (3/2 z_1)^2 + \varpi^2 \\ &= 3z_1^2 + \tilde{c}_1, \\ q'(z_2) &= (z_2 - z_1)(z_2 - z_3) \\ &= -q'(z_1)(z_2 - z_3)/(z_1 - z_3) \\ &= -(3z_1^2 + \tilde{c}_1) 2i\varpi / (3/2 z_1 + i\varpi). \end{aligned} \quad (\text{D2})$$

1259 The  $q_j(z)$  are defined in Eq. (31), giving

$$q_0(z) = \tilde{c}_1 + z^2 \quad q_1(z) = z \quad q_2(z) = 1 \quad (\text{D3})$$

1260 for a cubic polynomial in the standard canonical form of  
1261 Eq. (19). Evaluating Eq. (D1) gives

$$\begin{aligned} a_0 &\sim e^{z_1 t} (z_1^2 + \tilde{c}_1) + e^{-z_1 t/2} \left[ 2z_1^2 \cos \varpi t - \tilde{c}_1 z_1 \frac{\sin \varpi t}{\varpi} \right] \\ a_1 &\sim z_1 e^{z_1 t} + e^{-z_1 t/2} \left[ -z_1 \cos \varpi t + \left( \frac{3}{2} z_1^2 + \tilde{c}_1 \right) \frac{\sin \varpi t}{\varpi} \right] \\ a_2 &\sim e^{z_1 t} - e^{-z_1 t/2} \left[ \cos \varpi t + \frac{3}{2} z_1 \frac{\sin \varpi t}{\varpi} \right], \end{aligned} \quad (\text{D4})$$

1262 with a common factor  $(3z_1^2 + \tilde{c}_1)^{-1}$  multiplying each  $a_i(t)$ .  
1263 Arranging coefficients of each time-dependent term in  
1264 a matrix gives the result in Eq. (37). All three roots are  
1265 real when  $\varpi^2 < 0$ , which is the case for  $\tilde{c}_1 < 0$  and  $\gamma < 1$ .  
1266 Then  $\varpi \rightarrow i\mu$  in Eq. (37), with  $\mu^2 = |3(z_1^2/2) + \tilde{c}_1|$  and  
1267  $\tilde{c}_1 = -|\tilde{c}_1|$ .

### 2. Second-order pole

1268 The case  $\varpi = 0$  resulting from  $\tilde{c}_1 = -3(z_1/2)^2$  in  
1269 Eq. (22) gives doubly-degenerate real roots  $z_2 = z_3 =$   
1270  $-z_1/2$  and  $q(z) \rightarrow (z - z_1)(z - z_2)^2$ . The residue at  
1271  $z = z_2$  in Eq. (29) for the Cayley-Hamilton coefficients  
1272  $a_j(t)$  requires the derivative of  $e^{z t} q_j(z)/(z - z_1)$  with re-  
1273 spect to  $z$ , evaluated at  $z = z_2$ . Calculating the residue  
1274

1275 according to Eq. (16) and substituting  $z_2 = -z_1/2$  gives

$$\begin{aligned} a_0(t) &= e^{-z_1 t/2} \left( \frac{8}{9} + \frac{1}{3} z_1 t \right) \\ a_1(t) &= e^{-z_1 t/2} \left( -\frac{4}{9} z_1^{-1} + \frac{1}{3} t \right) \\ a_2(t) &= -e^{-z_1 t/2} \left( \frac{4}{9} z_1^{-2} + \frac{2}{3} t z_1^{-1} \right) \end{aligned} \quad (\text{D5})$$

1276 The contribution from the first-order pole at  $z_1$  is ob-  
1277 tained as before from the simple-pole term of Eq. (37),  
1278 i.e., the first column of  $W_1(z_1)$  and the first element of  
1279  $u_1(t)$  remain the same.

### 1280 3. Third-order pole

1281 When  $\tilde{c}_0 = 0 = \tilde{c}_1$ , the characteristic polynomial  
1282  $q(z) \rightarrow z^3$ , with a triply degenerate, real root  $z_1 = 0$ .  
1283 The residue at  $z = 0$  in Eq. (29) for the Cayley-Hamilton  
1284 coefficients  $a_j(t)$  is one-half the second derivative of  
1285  $q_j(z) e^{zt}$  with respect to  $z$ , evaluated at  $z = 0$ , giving

$$\begin{aligned} a_j(t) &= \left[ \frac{1}{2} q_j''(z) + t q_j'(z) + \frac{1}{2} t^2 q(z) \right] e^{zt} \Big|_{z=0} \\ a_0(t) &= 1 \quad a_1(t) = t \quad a_2(t) = \frac{1}{2} t^2. \end{aligned} \quad (\text{D6})$$

### 1286 Appendix E: Existence of Degenerate Roots

1287 The characteristic polynomial for the case  $R_1 = R_2$  has  
1288 degenerate roots for  $D(\tilde{c}_0, \tilde{c}_1) = 0$  [see Eq. (46)], which  
1289 requires  $\tilde{c}_1 < 0$ . The special case  $\tilde{c}_0 = 0 = \tilde{c}_1$  discussed  
1290 in section IV A gives  $\omega_3^2 = 1$  and  $\omega_{12}^2 = 8$ , normalized to  
1291  $R_\delta^2/3$ . More generally, scale  $\omega_3^2$  and  $\omega_{12}^2$  in terms of the  
1292 same normalization as

$$\omega_3^2 = \lambda_3 R_\delta^2/3, \quad (\text{E1})$$

1293 where  $\lambda_3 \geq 0$ , and

$$\omega_{12}^2 = (\eta - \lambda_3 + 9/4) R_\delta^2/3. \quad (\text{E2})$$

1294 Then  $D(\tilde{c}_0, \tilde{c}_1) = 0$  gives

$$\eta^3 + a_\eta \eta + b_\eta = 0, \quad (\text{E3})$$

1295 with

$$\begin{aligned} \frac{a_\eta}{3} &= -\left(\frac{3}{2}\right)^4 (8\lambda_3 + 1) \\ \frac{b_\eta}{2} &= \left(\frac{3}{2}\right)^6 (8\lambda_3^2 + 20\lambda_3 - 1). \end{aligned} \quad (\text{E4})$$

1296 The roots  $\eta_1(\lambda_3)$  and  $\eta_\pm(\lambda_3)$  of Eq. (E3) can then be  
1297 obtained using Eqs. (C6) with the appropriate substitu-  
1298 tion of variables. Only those solutions such that  $\omega_{12}^2 \geq 0$   
1299 (i.e., is real) are of interest. The results, outlined in de-  
1300 tail below, are that (i) there are no degenerate roots if  
1301  $\omega_3^2 > R_\delta^2/3$ ; and (ii) for each  $\omega_3$  satisfying  $0 \leq \omega_3^2 \leq R_\delta^2/3$ ,  
1302 there are two values of  $\omega_{12}^2$  that give degenerate roots.

1303 Note for use in what follows that

$$\begin{aligned} &\cdot a_\eta < 0 \text{ for all } \lambda_3 \geq 0 \\ &\cdot \therefore \text{no Eq. (C6a) solutions for } \eta \\ &\cdot \sqrt{\alpha_\eta} = \sqrt{|a_\eta/3|} = \frac{9}{4} \sqrt{8\lambda_3 + 1} \\ &\cdot b_\eta = 0 \text{ for } \lambda_3 = \frac{3}{4} (\sqrt{3} - \frac{5}{3}) \equiv \lambda_b \approx 0.05 \\ &\cdot D(a_\eta, b_\eta) = \frac{3^{12}}{2^6} \lambda_3 (\lambda_3 - 1)^3 \\ &\cdot \gamma_\eta(\lambda_3) = \frac{|8\lambda_3^2 + 20\lambda_3 - 1|}{(8\lambda_3 + 1)^{3/2}} \quad [\text{see Eq. (C5)}] \\ &\gamma_\eta(0) = 1, \quad \gamma_\eta(\lambda_b) = 0, \quad \gamma_\eta(1) = 1 \end{aligned}$$

1311 1) If  $\lambda_3 > 1$ , then

$$\begin{aligned} &\cdot D(a_\eta, b_\eta) > 0, \text{ equivalent to } \gamma_\eta > 1 \\ &\cdot \text{there is one real solution } \eta_1 \text{ from Eq. (C6b)} \\ &\cdot \text{Define } \varphi_\eta = \frac{1}{3} \cosh^{-1} \gamma_\eta \\ &\cdot b_\eta > 0 \\ &\cdot \eta_1 = -2\sqrt{\alpha_\eta} \cosh \varphi_\eta \\ &\quad \cosh \varphi_\eta \geq 1 \text{ for all } \varphi_\eta, \\ &\quad 2\sqrt{\alpha_\eta} > \frac{9}{2} (3) \\ &\therefore \eta_1 < -\frac{27}{2} \\ &\implies \omega_{12}^2 \sim (\eta_1 + \frac{9}{4} - \lambda_3) < -\frac{45}{4} - \lambda_3 < 0 \\ &\bullet \text{No real } \omega_{12} \text{ such that Eq. (19) has degenerate roots for} \\ &\omega_3^2 = \lambda_3 R_\delta^2/3 > R_\delta^2/3 \end{aligned}$$

1324 2) If  $\lambda_3 \leq 1$ , then

$$\begin{aligned} &\cdot \omega_{12}^2 \sim (\eta + \frac{9}{4} - \lambda_3) \geq 0 \text{ for } \eta \geq 0 \\ &\cdot D(a_\eta, b_\eta) \leq 0, \text{ equivalent to } \gamma_\eta \leq 1 \\ &\cdot \text{there are three real solutions } \eta_1, \eta_\pm \text{ from Eq. (C6d)} \\ &\cdot \text{Define } \vartheta = \frac{1}{3} \sin^{-1}(\gamma_\eta) \\ \text{(a) If } \lambda_b \leq \lambda_3 \leq 1, \text{ then} \\ &\quad 0 \leq \gamma_\eta \leq 1, \\ &\quad 0 \leq \vartheta \leq \pi/6, \\ &\quad b_\eta \geq 0 \\ &\cdot \eta_1 = 2\sqrt{\alpha_\eta} \sin \vartheta \\ &\quad \therefore \eta_1 \geq 0 \\ &\quad \implies \omega_{12}^2 > 0 \\ &\cdot \eta_\pm = -\sqrt{\alpha_\eta} \sin \vartheta \pm \sqrt{3} (\alpha_\eta - \alpha_\eta \sin^2 \vartheta)^{1/2} \\ &\quad = \pm 2\sqrt{\alpha_\eta} \sin(\pi/3 \mp \vartheta) \\ &\quad \therefore \eta_\pm \geq 0 \\ &\quad \implies \omega_{12}^2 > 0 \\ \text{(b) If } 0 \leq \lambda_3 \leq \lambda_b, \text{ then} \\ &\quad 1 \geq \gamma_\eta \geq 0, \\ &\quad \pi/6 \geq \vartheta \geq 0, \\ &\quad b_\eta \leq 0 \\ &\cdot \eta_1 = -2\sqrt{\alpha_\eta} \sin \vartheta \\ &\quad \therefore -\frac{9}{4} \leq \eta_1 \leq 0 \\ &\quad \implies \omega_{12}^2 \sim \eta_1 + \frac{9}{4} - \lambda_3 \geq 0, \\ &\quad \text{since } \eta_1 \in [-\frac{9}{4}, 0] \text{ as } \lambda_3 \in [0, \lambda_b] \\ &\cdot \eta_\pm = \sqrt{\alpha_\eta} \sin \vartheta \pm \sqrt{3} (\alpha_\eta - \alpha_\eta \sin^2 \vartheta)^{1/2} \\ &\quad = 2\sqrt{\alpha_\eta} \sin(\vartheta \pm \pi/3) \end{aligned}$$

$$\begin{aligned} \therefore \eta_+ &\geq 0 \\ \implies \omega_{12}^2 &> 0 \end{aligned}$$

• 2 real  $\omega_{12}^2$  such that Eq. (19) has degenerate roots for  $0 \leq \omega_3^2 \leq R_\delta^2/3$

The solutions for  $\omega_{12}^2$  become equal at  $\omega_3^2 = R_\delta^2/3$ , as shown in Fig. 1, corresponding to the case  $\tilde{c}_1 = 0 = \tilde{c}_0$ . There is then a three-fold degenerate root  $z = 0$  of Eq. (19). Recall that a solution to  $D(\tilde{c}_0, \tilde{c}_1) = 0$  for real  $\tilde{c}_0, \tilde{c}_1$  requires  $\tilde{c}_1 = \omega_{12}^2 + \omega_3^2 - 3R_\delta^2 \leq 0$ , which is readily verified for the solutions obtained above. Scaling  $\tilde{c}_1$  according to Eq. (E1) and Eq. (E2), dividing by  $R_\delta^2/3$  and using the maximum value  $\eta_{\max} = \sqrt{\alpha_\eta} = 27/4$  at  $\lambda_3 = 1$  gives

$$\begin{aligned} \tilde{c}_1 &\sim (\eta - \lambda_3 + \frac{9}{4}) + \lambda_3 - 9 \\ &\leq \frac{27}{4} + \frac{9}{4} - 9 = 0. \end{aligned} \quad (\text{E5})$$

### Appendix F: Vector Model

There is a simple physical interpretation for the action of the propagator  $e^{-\Gamma t}$  when, as is most common, the matrix  $\Gamma$  has three distinct eigenvalues. Supplementary details of the model introduced in section VC are presented here. Consider the case of one real eigenvalue and two complex conjugate eigenvalues. Results for the other possibility, that of three real eigenvalues, are obtained directly from Eq. (F5) in what follows.

The eigenvalues of  $-\Gamma$  are the roots  $s_1 = z_1 - \bar{R}$  and  $s_{2,3} \equiv s_\pm = -z_1/2 \pm i\varpi - \bar{R}$ , obtained from Eq. (24), with real  $z_1$  given in Eqs. (C6). The associated eigenvectors are  $\mathbf{s}_1$  and the complex conjugate pair  $\mathbf{s}_\pm$ . The relation between  $\mathbf{s}_\pm$  and the real vectors  $\tilde{\mathbf{s}}_2$  and  $\tilde{\mathbf{s}}_3$  defined in Eq. (60) is

$$\begin{aligned} \tilde{\mathbf{s}}_2 &= \frac{1}{2}(\mathbf{s}_+ + \mathbf{s}_-) & \tilde{\mathbf{s}}_3 &= -\frac{i}{2}(\mathbf{s}_+ - \mathbf{s}_-) \\ \mathbf{s}_+ &= \tilde{\mathbf{s}}_2 + i\tilde{\mathbf{s}}_3 & \mathbf{s}_- &= \tilde{\mathbf{s}}_2 - i\tilde{\mathbf{s}}_3. \end{aligned} \quad (\text{F1})$$

Defining  $\tilde{\mathbf{s}}_1 \equiv \mathbf{s}_1$  gives a set  $\tilde{\mathbf{s}}_i$  of three linearly independent vectors that can be used as an alternative basis for representing arbitrary system states. We then have

$$\begin{aligned} -\Gamma \tilde{\mathbf{s}}_2 &= \frac{1}{2}(\mathbf{s}_+ \mathbf{s}_+ + \mathbf{s}_- \mathbf{s}_-) = \frac{1}{2}(\mathbf{s}_+ \mathbf{s}_+ + \mathbf{s}_+^* \mathbf{s}_+^*) \\ e^{-\Gamma t} \tilde{\mathbf{s}}_2 &= \frac{1}{2}(e^{s_+ t} \mathbf{s}_+ + e^{s_+^* t} \mathbf{s}_+^*) = \text{Re}[e^{s_+ t} \mathbf{s}_+] \\ &= e^{-(\bar{R}+z_1/2)t} \text{Re}[e^{i\varpi t}(\tilde{\mathbf{s}}_2 + i\tilde{\mathbf{s}}_3)] \\ &= e^{-(\bar{R}+z_1/2)t} (\cos \varpi t \tilde{\mathbf{s}}_2 - \sin \varpi t \tilde{\mathbf{s}}_3). \end{aligned} \quad (\text{F2})$$

Similarly,

$$\begin{aligned} e^{-\Gamma t} \tilde{\mathbf{s}}_3 &= -\frac{i}{2}(e^{s_+ t} \mathbf{s}_+ - e^{s_+^* t} \mathbf{s}_+^*) = \text{Im}[e^{s_+ t} \mathbf{s}_+] \\ &= e^{-(\bar{R}+z_1/2)t} \text{Im}[e^{i\varpi t}(\tilde{\mathbf{s}}_2 + i\tilde{\mathbf{s}}_3)] \\ &= e^{-(\bar{R}+z_1/2)t} (\sin \varpi t \tilde{\mathbf{s}}_2 + \cos \varpi t \tilde{\mathbf{s}}_3). \end{aligned} \quad (\text{F3})$$

These relations, together with  $e^{-\Gamma t} \tilde{\mathbf{s}}_1 = e^{s_1 t} \tilde{\mathbf{s}}_1$ , yield the propagator  $e^{-\Gamma t}$  for the evolution of states  $\tilde{\mathcal{M}} = \sum_i \mathcal{M}_i \tilde{\mathbf{s}}_i$  expressed in the  $\{\tilde{\mathbf{s}}_i\}$  basis, as given in Eq. (63).

As noted in Eq. (61), matrix  $P$  generated from the  $\{\tilde{\mathbf{s}}_i\}$  entered as column vectors transforms from the  $\{\tilde{\mathbf{s}}_i\}$  basis to the standard basis, with  $P^{-1} = \text{adj } P / \det P$  giving the desired  $\tilde{\mathcal{M}}$  starting with  $\mathcal{M}$  in the standard basis. One easily shows that  $\det P = \tilde{\mathbf{s}}_1 \cdot (\tilde{\mathbf{s}}_2 \times \tilde{\mathbf{s}}_3)$ , and row  $i$ , column  $l$  of  $\text{adj } P$  is  $(\tilde{\mathbf{s}}_j \times \tilde{\mathbf{s}}_k)_l$  for cyclic permutation of  $i = 1, j = 2$ , and  $k = 3$  to obtain

$$P^{-1} = \frac{1}{\tilde{\mathbf{s}}_1 \cdot (\tilde{\mathbf{s}}_2 \times \tilde{\mathbf{s}}_3)} \begin{bmatrix} \cdots & (\tilde{\mathbf{s}}_2 \times \tilde{\mathbf{s}}_3) & \cdots \\ \cdots & (\tilde{\mathbf{s}}_3 \times \tilde{\mathbf{s}}_1) & \cdots \\ \cdots & (\tilde{\mathbf{s}}_1 \times \tilde{\mathbf{s}}_2) & \cdots \end{bmatrix} \quad (\text{F4})$$

The eigenvectors needed to construct the real basis are most readily obtained as any column of  $\text{adj } A(s_i) = \text{adj}(s_i \mathbf{1} + \Gamma)$  for each eigenvalue  $s_i$  (see Appendix B). Performing the straightforward calculation gives the following result for the eigenvectors, with the left arrow signifying that the columns of the matrix map to  $\mathbf{s}_i$ :

$$\begin{aligned} \mathbf{s}_i \leftarrow \text{adj } A(s_i) &= \begin{bmatrix} -\Gamma_{23}\Gamma_{32} + (s_i + R_2)(s_i + R_3) & \Gamma_{13}\Gamma_{32} - \Gamma_{12}(s_i + R_3) & \Gamma_{12}\Gamma_{23} - \Gamma_{13}(s_i + R_2) \\ \Gamma_{31}\Gamma_{23} - \Gamma_{21}(s_i + R_3) & -\Gamma_{13}\Gamma_{31} + (s_i + R_1)(s_i + R_3) & \Gamma_{13}\Gamma_{21} - \Gamma_{23}(s_i + R_1) \\ \Gamma_{21}\Gamma_{32} - \Gamma_{31}(s_i + R_2) & \Gamma_{31}\Gamma_{12} - \Gamma_{32}(s_i + R_1) & -\Gamma_{12}\Gamma_{21} + (s_i + R_1)(s_i + R_2) \end{bmatrix} \\ \xrightarrow{\text{OBE}} &\begin{bmatrix} \omega_1^2 + (s_i + R_2)(s_i + R_3) & \omega_1\omega_2 - \omega_3(s_i + R_3) & \omega_1\omega_3 + \omega_2(s_i + R_2) \\ \omega_1\omega_2 + \omega_3(s_i + R_3) & \omega_2^2 + (s_i + R_1)(s_i + R_3) & \omega_2\omega_3 - \omega_1(s_i + R_1) \\ \omega_1\omega_3 - \omega_2(s_i + R_2) & \omega_2\omega_3 + \omega_1(s_i + R_1) & \omega_3^2 + (s_i + R_1)(s_i + R_2) \end{bmatrix}. \end{aligned} \quad (\text{F5})$$

The three different forms of a given  $\mathbf{s}_i$  are therefore related by a scale factor, despite perhaps appearing otherwise. The scaling can be verified by calculating the eigenvectors in the usual fashion as solutions to  $(s_i \mathbf{1} + \Gamma)\mathbf{s}_i = 0$ . This system of equations is overdetermined, by construction, so any one of the three equations is a linear combination of the other two and is redundant. We are free to assign any (nonzero) value to one of the components, leaving two equations and two unknowns. There are three different but equivalent forms for the eigenvector solution depending on which two equations are chosen. Setting the third component equal to one gives

1412 an expression for the other two components involving a 1454  
1413 common denominator. Scaling each eigenvector by the  
1414 denominator of its other two components gives the result  
1415 in Eq. (F5).

1416 For the OBE in the absence of relaxation ( $R_i = 0$ ),  
1417  $\Gamma$  generates a rotation about  $\omega_e$ , as is well known. The  
1418 real eigenvalue of  $-\Gamma$  is  $s_1 = 0$  with eigenvector  $\mathbf{s}_1 =$   
1419  $(\omega_1, \omega_2, \omega_3)$ , obtained by dividing column  $j$  of  $\text{adj} A(s_1)$   
1420 by (nonzero)  $\omega_j$ . This is the expected rotation axis for  
1421 the resulting time evolution. If  $\omega_e = 0$ , then  $\Gamma$  is already  
1422 diagonal, and the coordinates reduce to the standard co-  
1423 ordinate system as required.

1424 We also have  $\text{adj} A(s_i) = \text{adj} A_p(z_i)$ , since  $s_i = z_i - \bar{R}$   
1425 and  $R_i - \bar{R} = R_{ip}$ . The real basis vectors  $\tilde{\mathbf{s}}_{2,3} \equiv \tilde{\mathbf{z}}_{2,3}$   
1426 are equal to the respective real, imaginary parts of  $\mathbf{z}_+ =$   
1427  $\text{adj} A_p(z_+)$  according to Eq. (60), with  $z_+ = -z_1/2 +$   
1428  $i\varpi$ . Then, using Eq. (26) for  $\text{adj} A_p(z_i)$  in polynomial  
1429 form and eliminating common scale factors, the real basis  
1430 vectors defining the oblique coordinate system can be  
1431 written concisely as

$$\begin{aligned}\tilde{\mathbf{s}}_1 &= \tilde{\mathbf{z}}_1 \leftarrow A_{0p} + A_{1p} z_1 + \mathbb{1} z_1^2 \\ \tilde{\mathbf{s}}_2 &= \tilde{\mathbf{z}}_2 \leftarrow A_{0p} - A_{1p} \frac{z_1}{2} + \mathbb{1} \left[ \left( \frac{z_1}{2} \right)^2 - \varpi^2 \right] \\ \tilde{\mathbf{s}}_3 &= \tilde{\mathbf{z}}_3 \leftarrow A_{1p} - \mathbb{1} z_1\end{aligned}\quad (\text{F6})$$

1432 The result for  $\tilde{\mathbf{z}}_1$  can be obtained directly from Eq. (F5)  
1433 with the substitutions  $s_i \rightarrow z_i$  and  $R_i \rightarrow R_{ip}$  for the  
1434 corresponding parameters associated with  $\Gamma_p$ . One can  
1435 readily deduce the coefficient matrices  $A_{0p}$  and  $A_{1p}$  by  
1436 comparing Eq. (F5) with the polynomial form in Eq. (26),  
1437 also given above in the expression for  $\tilde{\mathbf{s}}_1$ . Recall that  
1438  $\sum_i R_{ip} = 0$  by construction in the original matrix parti-  
1439 tioning, so we can simplify terms such as  $R_{2p} + R_{3p} \rightarrow$   
1440  $-R_{1p}$  and its cyclic permutations. The coefficients can  
1441 also be obtained as simple functions of  $\Gamma_p$  using Eq. (27).  
1442 For the OBE parameters, each coefficient matrix is

$$\begin{aligned}A_{0p} &= \begin{bmatrix} \omega_1^2 + R_{2p}R_{3p} & \omega_1\omega_2 - \omega_3R_{3p} & \omega_1\omega_3 + \omega_2R_{2p} \\ \omega_1\omega_2 + \omega_3R_{3p} & \omega_2^2 + R_{1p}R_{3p} & \omega_2\omega_3 - \omega_1R_{1p} \\ \omega_1\omega_3 - \omega_2R_{2p} & \omega_2\omega_3 + \omega_1R_{1p} & \omega_3^2 + R_{1p}R_{2p} \end{bmatrix} \text{ and} \\ A_{1p} &= -\Gamma_p = \begin{bmatrix} -R_{1p} & -\omega_3 & \omega_2 \\ \omega_3 & -R_{2p} & -\omega_1 \\ -\omega_2 & \omega_1 & -R_{3p} \end{bmatrix},\end{aligned}\quad (\text{F7})$$

1443 with  $R_{1p} = R_{2p} = R_\delta$  and  $R_{3p} = -2R_\delta$  from Eq. (44).

### 1. Measures of obliquity

1445 Bloch equation dynamics are simple in the oblique co-  
1446 ordinates of the model, consisting of independent rota-  
1447 tion and relaxation elements. This section provides ex-  
1448 amples that quantify the degree to which the plane of  
1449 rotation is oblique to the axis  $\tilde{\mathbf{z}}_1$  representing simple ex-  
1450ponential decay. In what follows, the first column of  
1451  $\text{adj} A_p$  is arbitrarily chosen to calculate the coordinate  
1452 basis  $\{\tilde{\mathbf{z}}_i\}$ , for  $R_1 = R_2$ . Similar results are obtained  
1453 using any of the other columns.

a. *Off resonance,  $\omega_e = (0, \omega_2, \omega_3)$*

1455 Off resonance, in contrast to the on-resonance example  
1456 of section VC4 b,  $\tilde{\mathbf{z}}_1$  is neither aligned with  $\omega_e$ , nor is  
1457 it orthogonal to the  $(\tilde{\mathbf{z}}_2, \tilde{\mathbf{z}}_3)$ -plane. Calculating the  $\tilde{\mathbf{z}}_i$  as  
1458 above provides the normal to this plane,  $\tilde{\mathbf{n}}_{23} = \tilde{\mathbf{z}}_2 \times \tilde{\mathbf{z}}_3$ .  
1459 Then

$$\tilde{\mathbf{z}}_1 = \begin{pmatrix} (z_1 + R_\delta)(z_1 - 2R_\delta) \\ \omega_3(z_1 - 2R_\delta) \\ -\omega_2(z_1 + R_\delta) \end{pmatrix}\quad (\text{F8})$$

$$\tilde{\mathbf{n}}_{23} = \begin{pmatrix} 3\omega_2\omega_3R_\delta \\ -\omega_2(\tilde{c}_1 - z_1R_\delta + z_1^2 + R_\delta^2) \\ -\omega_3(\tilde{c}_1 + 2z_1R_\delta + z_1^2 + 4R_\delta^2) \end{pmatrix}\quad (\text{F9})$$

1461 using  $\varpi^2 = 3/4z_1^2 + \tilde{c}_1$  from Eq. (22) in the expression  
1462 for  $\tilde{\mathbf{s}}_2$ . Although the normal bears little resemblance to  
1463  $\tilde{\mathbf{z}}_1$ , let us scale  $\tilde{\mathbf{z}}_1$  by  $f_s = -(\tilde{\mathbf{n}}_{23})_1/(\tilde{\mathbf{z}}_1)_1$ , so that the  
1464 first component  $(\tilde{\mathbf{z}}_1)_1 \rightarrow -(\tilde{\mathbf{n}}_{23})_1$ . For the other two  
1465 components, straightforward algebra gives the relation  
1466  $f_s\tilde{\mathbf{z}}_1 - \tilde{\mathbf{n}}_{23} \propto q(z_1)$ , the characteristic polynomial for  $-\Gamma_p$ ,  
1467 which is zero when evaluated at its root  $z_1$ . Thus, within  
1468 a scale factor or, equivalently, when both both vectors  
1469 are normalized, we have

$$\tilde{\mathbf{n}}_{23} = \begin{pmatrix} -(\tilde{\mathbf{z}}_1)_1 \\ (\tilde{\mathbf{z}}_1)_2 \\ (\tilde{\mathbf{z}}_1)_3 \end{pmatrix}.\quad (\text{F10})$$

b. *Off resonance,  $\omega_e = (\omega_1, 0, \omega_3)$*

1471 Similarly, for  $\omega_2 = 0$ ,

$$\tilde{\mathbf{z}}_1 = \begin{pmatrix} \omega_1^2 + (z_1 + R_\delta)(z_1 - 2R_\delta) \\ \omega_3(z_1 - 2R_\delta) \\ \omega_1\omega_3 \end{pmatrix}\quad (\text{F11})$$

$$\tilde{\mathbf{n}}_{23} = - \begin{pmatrix} \omega_1\omega_3 \\ \omega_1(z_1 + R_\delta) \\ \frac{1}{4}(z_1 + 4R_\delta)^2 + \varpi^2 - \omega_1^2 \end{pmatrix},\quad (\text{F12})$$

1473 Scaling  $\tilde{\mathbf{z}}_1$  by  $f_s = -(\tilde{\mathbf{n}}_{23})_2/(\tilde{\mathbf{z}}_1)_2$  gives  $f_s\tilde{\mathbf{z}}_1 - \tilde{\mathbf{n}}_{23} \propto$   
1474  $q(z_1)$  for components one and three, so that

$$\tilde{\mathbf{n}}_{23} = \begin{pmatrix} (\tilde{\mathbf{z}}_1)_1 \\ -(\tilde{\mathbf{z}}_1)_2 \\ (\tilde{\mathbf{z}}_1)_3 \end{pmatrix}\quad (\text{F13})$$

1475 within a scale factor.

c.  *$\omega_1 = \omega_2 = \omega_3 \equiv \omega$*

1477 In this case,

$$\tilde{\mathbf{z}}_1 = \begin{pmatrix} \omega^2 + (z_1 + R_\delta)(z_1 - 2R_\delta) \\ \omega(\omega + z_1 - 2R_\delta) \\ -\omega(\omega + z_1 + R_\delta) \end{pmatrix}\quad (\text{F14})$$

1478 and

$$\tilde{\mathbf{n}}_{23} = - \left( \begin{array}{c} \omega(2\omega - 3R_\delta) \\ \frac{1}{4}(z_1 - 2R_\delta)^2 + \omega(z_1 + R_\delta) + \varpi^2 - \omega^2 \\ \frac{1}{4}(z_1 + 4R_\delta)^2 - \omega(z_1 + R_\delta) + \varpi^2 - \omega^2 \end{array} \right). \quad (\text{F15})$$

1479 Scaling  $\tilde{\mathbf{z}}_1$  by  $f_s = (\tilde{\mathbf{n}}_{23})_1/(\tilde{\mathbf{z}}_1)_2$  gives both  $f_s(\tilde{\mathbf{z}}_1)_1 -$   
1480  $(\tilde{\mathbf{n}}_{23})_2$  and  $f_s(\tilde{\mathbf{z}}_1)_3 - (\tilde{\mathbf{n}}_{12})_3$  proportional to  $q(z_1)$ , so that  
1481 the vectors can be scaled to satisfy

$$\tilde{\mathbf{n}}_{23} = \left( \begin{array}{c} (\tilde{\mathbf{z}}_1)_2 \\ (\tilde{\mathbf{z}}_1)_1 \\ (\tilde{\mathbf{z}}_1)_3 \end{array} \right). \quad (\text{F16})$$

## 1482 Appendix G: Solution Verification

1483 The solutions are evaluated here for  $R_1 = R_2$  using a  
1484 representative set of limiting cases that are readily solved  
1485 by other methods to check the solutions.

### 1486 1. Three distinct roots

1487 Three examples are presented representing the sepa-  
1488 rate cases  $\tilde{c}_0 = 0$  and  $\tilde{c}_1 = 0$ .

1489 (i)  $\tilde{c}_0 = 0, \tilde{c}_1 \neq 0$

1490 According to the defining relations for  $\tilde{c}_0$  and  $\tilde{c}_1$  in  
1491 Eq. (45), the condition  $\tilde{c}_0 = 0$  implies  $\omega_{12}^2 = 2R_\delta^2(1 + \frac{1}{3}\lambda_3)$ ,  
1492 using Eq. (3) for  $\omega_e^2$  and Eq. (47) for  $\omega_3$ . Then

$$\tilde{c}_1 = \begin{cases} R_\delta^2(\lambda_3 - 1) & R_\delta \neq 0 \\ \omega_e^2 & R_\delta = 0 \end{cases} \quad (\text{G1})$$

1493 The roots of Eq. (19) are easily obtained, giving

$$z_1 = 0 \quad \varpi = \sqrt{\tilde{c}_1}. \quad (\text{G2})$$

1494 There are two cases, depending on the sign of  $\tilde{c}_1$ .

1495 (1)  $\tilde{c}_1 > 0$

1496 Equation 37 gives

$$e^{-\Gamma_p t} = \mathbf{1} - \frac{\Gamma_p}{\varpi} \sin \varpi t + \left( \frac{\Gamma_p}{\varpi} \right)^2 (1 - \cos \varpi t). \quad (\text{G3})$$

1497 There is no exponential decay contribution due to this  
1498 term, with the overall factor  $e^{-Rt}$  in the final expression  
1499 for  $e^{-\Gamma t}$  providing a single system decay rate  $\tilde{R}$ .

1500 *Example (1)*

1501 Choose  $R_\delta = 0$  to obtain

1502  $\tilde{c}_0 = 0, \tilde{c}_1 = \omega_e^2, \varpi = \omega_e$ .

1503 Then Eq. (G3) represents a rotation about the field  $\omega_e$ .

1504 The propagator  $U_R$  for a rotation about  $\omega_e$  is read-  
1505 ily obtained by transforming to a coordinate system  
1506 with new  $z$ -axis aligned with  $\omega_e$ , rotating by angle

1507  $-\omega_e t$  about this axis, then transforming back to the  
1508 original coordinates. Specifying the orientation of  $\omega_e$   
1509 in terms of polar angle  $\theta$  and azimuthal angle  $\phi$  rela-  
1510 tive to the  $z$ - and  $x$ -axes, respectively, one has  $U_R =$   
1511  $U_z(-\phi)U_y(-\theta)U_z(-\omega_e t)U_y(\theta)U_z(\phi)$  in terms of the ele-  
1512 mentary operators  $U_y$  and  $U_z$  for rotations about the  $y$ -  
1513 and  $z$ - axes, respectively. Then  $U_R$  provides a verification  
1514 of the Eq. (G3) result upon substituting  $\cos \phi = \omega_1/\omega_{12}$ ,  
1515  $\sin \phi = \omega_2/\omega_{12}$ ,  $\cos \theta = \omega_3/\omega_e$ ,  $\sin \theta = \omega_{12}/\omega_e$ .

1516 (2)  $\tilde{c}_1 < 0$

1517 for  $\lambda_3 < 1$  gives  $\varpi \rightarrow i\mu = i\sqrt{|\tilde{c}_1|}$  and

$$e^{-\Gamma_p t} = \mathbf{1} - \frac{\Gamma_p}{\mu} \sinh \mu t + \left( \frac{\Gamma_p}{\mu} \right)^2 (\cosh \mu t - 1) \quad (\text{G4})$$

1518 *Example (2)*

1519 Choose  $\omega_1^2 = 2R_\delta^2, \omega_2 = 0, \lambda_3 = 0$  to obtain  
1520  $\tilde{c}_0 = 0, \tilde{c}_1 = -R_\delta^2, \mu = R_\delta$

1521 Then Eq. (G4) gives

$$e^{-\Gamma_p t} = \begin{pmatrix} e^{-R_\delta t} & 0 & 0 \\ 0 & 2 - e^{R_\delta t} & \sqrt{2}(1 - e^{R_\delta t}) \\ 0 & -\sqrt{2}(1 - e^{R_\delta t}) & 2e^{R_\delta t} - 1 \end{pmatrix}. \quad (\text{G5})$$

1522 For an independent calculation, the matrix  $-\Gamma_p$  can be  
1523 diagonalized, with eigenvalues given by the  $z_i$  and associ-  
1524 ated real-valued eigenvectors. The simple exponential of  
1525 the diagonalized matrix is then transformed back to the  
1526 original basis in the standard fashion using the matrix  
1527 of eigenvectors and its inverse to obtain  $e^{-\Gamma_p t}$  as given  
1528 above.

1529 (ii)  $\tilde{c}_1 = 0, \tilde{c}_0 \neq 0$

1530 The condition  $\tilde{c}_1 = 0$  implies  $\omega_e^2 = 3R_\delta^2$ , leading to

$$\tilde{c}_0 = R_\delta^3(1 - \lambda_3) \quad (\text{G6})$$

1531 and root  $z_1 = -\text{sgn}(\tilde{c}_0)|\tilde{c}_0|^{1/3}$  from Eq. (C6e). For  
1532  $\text{sgn}(\tilde{c}_0) = \pm 1$  and the definition  $\tilde{\lambda}_3 = |1 - \lambda_3|^{1/3}$ , we  
1533 have

$$z_1 = \mp \tilde{\lambda}_3 R_\delta \quad \varpi = \frac{\sqrt{3}}{2} \tilde{\lambda}_3 R_\delta \quad (\text{G7})$$

1534 Although the form of Eq. (37) does not simplify in this  
1535 case as appreciably as for  $\tilde{c}_0 = 0$ , both the root  $z_1$ , which  
1536 determines the decay rate, and the oscillatory frequency  
1537  $\varpi$  are simple multiples of  $R_\delta$ .

1538 *Example (3)*

1539 Choose  $\omega_e^2 \rightarrow \omega_1^2 = 3R_\delta^2, \omega_2 = 0 = \omega_3$ .

1540 Then most off-diagonal elements of  $\Gamma_p$  are equal to zero,  
1541 and  $\tilde{\lambda}_3 = 1$  for the Eq. (G7) input parameters to Eq. (37).  
1542 Defining  $\kappa = (\sqrt{3}/2)R_\delta$  and combining the sums of

trigonometric functions that appear on the diagonal gives the succinct form

$$e^{-\Gamma_p t} = e^{\frac{1}{2}R_\delta t} \begin{pmatrix} e^{-\frac{3}{2}R_\delta t} & 0 & 0 \\ 0 & -2\sin(\kappa t - \frac{\pi}{6}) & -2\sin(\kappa t) \\ 0 & 2\sin(\kappa t) & 2\sin(\kappa t + \frac{\pi}{6}) \end{pmatrix} \quad (\text{G8})$$

Again, the matrix  $-\Gamma_p$  is diagonalizable, providing a simple result for the matrix exponential in the eigenbasis and a straightforward means for calculating  $e^{-\Gamma_p t}$  as obtained above. The associated eigenvectors are complex-valued in this case, making the algebra slightly more tedious. Alternatively, one can readily verify that  $d/dt e^{-\Gamma_p t} = -\Gamma_p e^{-\Gamma_p t}$ .

## 2. Two equal roots

Degenerate roots require  $\gamma = 1$ . For a given  $\omega_3^2 = \lambda_3 R_\delta^2/3$ , with  $0 \leq \lambda_3 \leq 1$ , there are two values  $\omega_{12}^2$  that satisfy  $\gamma = 1$ , derived in Appendix E and discussed in Sec. IV A. Consider  $\lambda_3 = 0$ , on resonance, in which case Eqs. (47) and (48) give

$$\begin{aligned} (\vartheta_1, \vartheta_2) &= (-\pi/6, \pi/2) \\ (\eta_1, \eta_2) &= (-9/4, 9/2) \\ (\omega_{12,1}^2, \omega_{12,2}^2) &= (0, 9/4R_\delta^2). \end{aligned} \quad (\text{G9})$$

(i)  $\omega_{12} = 0$

Then there is only relaxation, with  $\Gamma_p$  reduced to the diagonal elements  $\{R_\delta, R_\delta, -2R_\delta\}$ . We have  $\tilde{c}_1 = -3R_\delta^2$ ,  $\tilde{c}_0 = -2R_\delta^3 < 0$ , and

$$z_1 = 2R_\delta \quad \varpi = 0 \quad (\text{G10})$$

from Eq. (C6b). Equation (38) gives the expected result

$$e^{-\Gamma_p t} = \begin{pmatrix} e^{-R_\delta t} & 0 & 0 \\ 0 & e^{-R_\delta t} & 0 \\ 0 & 0 & e^{2R_\delta t} \end{pmatrix}. \quad (\text{G11})$$

(ii)  $\omega_{12}^2 = \frac{9}{4}R_\delta^2 \rightarrow \omega_1^2$

$$z_1 = -R_\delta, \quad \varpi = 0, \quad (\text{G12})$$

resulting in

$$e^{-\Gamma_p t} = e^{\frac{1}{2}R_\delta t} \begin{pmatrix} e^{-\frac{3}{2}R_\delta t} & 0 & 0 \\ 0 & 1 - \omega_1 t & -\omega_1 t \\ 0 & \omega_1 t & 1 + \omega_1 t \end{pmatrix}. \quad (\text{G13})$$

Verifying that  $d/dt e^{-\Gamma_p t} = -\Gamma_p e^{-\Gamma_p t}$  is fairly straightforward and represents the simplest test of the solution, since  $\Gamma_p$  is not diagonalizable.

## 3. Three equal roots

There is a three-fold degenerate root  $z_i = 0$  in the case  $\tilde{c}_0 = 0 = \tilde{c}_1$ , since  $q(z) \rightarrow z^3$ . This requires  $\omega_e^2 = 3R_\delta^2$  from Eq. (45), which then forces  $\omega_3^2 = R_\delta^2/3$  in the expression for  $\tilde{c}_0$ . As noted previously, the Cayley-Hamilton theorem is simple to apply directly in this case, since  $q(\Gamma_p) = \Gamma_p^3 = 0$ . The series expansion of  $e^{-\Gamma_p t}$  is therefore truncated, giving the Eq. (39) result.

## 4. On resonance

When  $\omega_3 = 0$ ,  $\tilde{c}_0$  can be written in the form  $R_\delta(\tilde{c}_1 + R_\delta^2)$  from Eq. (45), with  $\tilde{c}_1 \rightarrow \omega_{12}^2 - 3R_\delta^2$ . The characteristic polynomial then becomes  $z^3 + R_\delta^3 + \tilde{c}_1(z + R_\delta)$ , so that, by inspection,

$$z_1 = -R_\delta \quad \varpi = \sqrt{\omega_{12}^2 - (\frac{3}{2}R_\delta)^2} \quad (\text{G14})$$

The solution for  $e^{-\Gamma_p t}$  using Eq. (37) with the above parameters yields the solution for  $e^{-\Gamma t}$  obtained originally by Torrey [6] for  $\varpi \neq 0$ . As discussed above, if  $\omega_{12} = 3R_\delta/2$  so that  $\varpi = 0$ , there is a two-fold degeneracy in the roots, giving the solution in Eq. (G13) for  $e^{-\Gamma_p t}$ .

For  $\omega_{12} < 3R_\delta/2$ , the sinusoidal terms become the corresponding hyperbolic functions, as noted earlier, with  $\cos \varpi t \rightarrow \cosh \mu t$  and  $\sin \varpi t/\varpi \rightarrow \sinh \mu t/\mu$ , where now  $\mu = \sqrt{(\frac{3}{2}R_\delta)^2 - \omega_{12}^2}$ .

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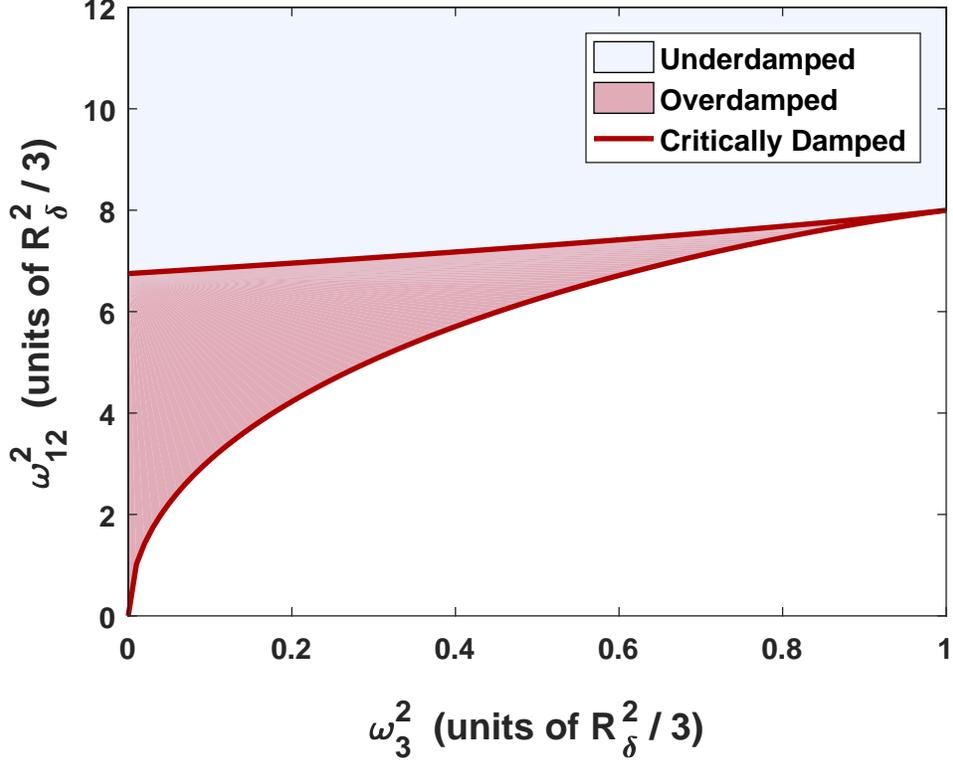


FIG. 1. Parameter values of  $\omega_{12}^2$  that give degenerate roots of the characteristic polynomial ( $\gamma = 1$ ) and critically damped solutions to the Bloch equation are plotted as a function of  $\omega_3^2$ , shown as red (solid) lines calculated using Eq. (48). The parameters are scaled to  $R_\delta^2/3$  as in Eq. (47). In the interior of the region delineated by these curves (light red), there are three distinct real roots ( $\tilde{c}_1 < 0$ ,  $\gamma < 1$ ) resulting in overdamped solutions. Outside this region (light blue), one real and two complex conjugate roots produce oscillatory, underdamped solutions, with  $\tilde{c}_1 > 0$  above the overdamped region and  $\tilde{c}_1 > 0$ ,  $\gamma > 1$  below the overdamped region.

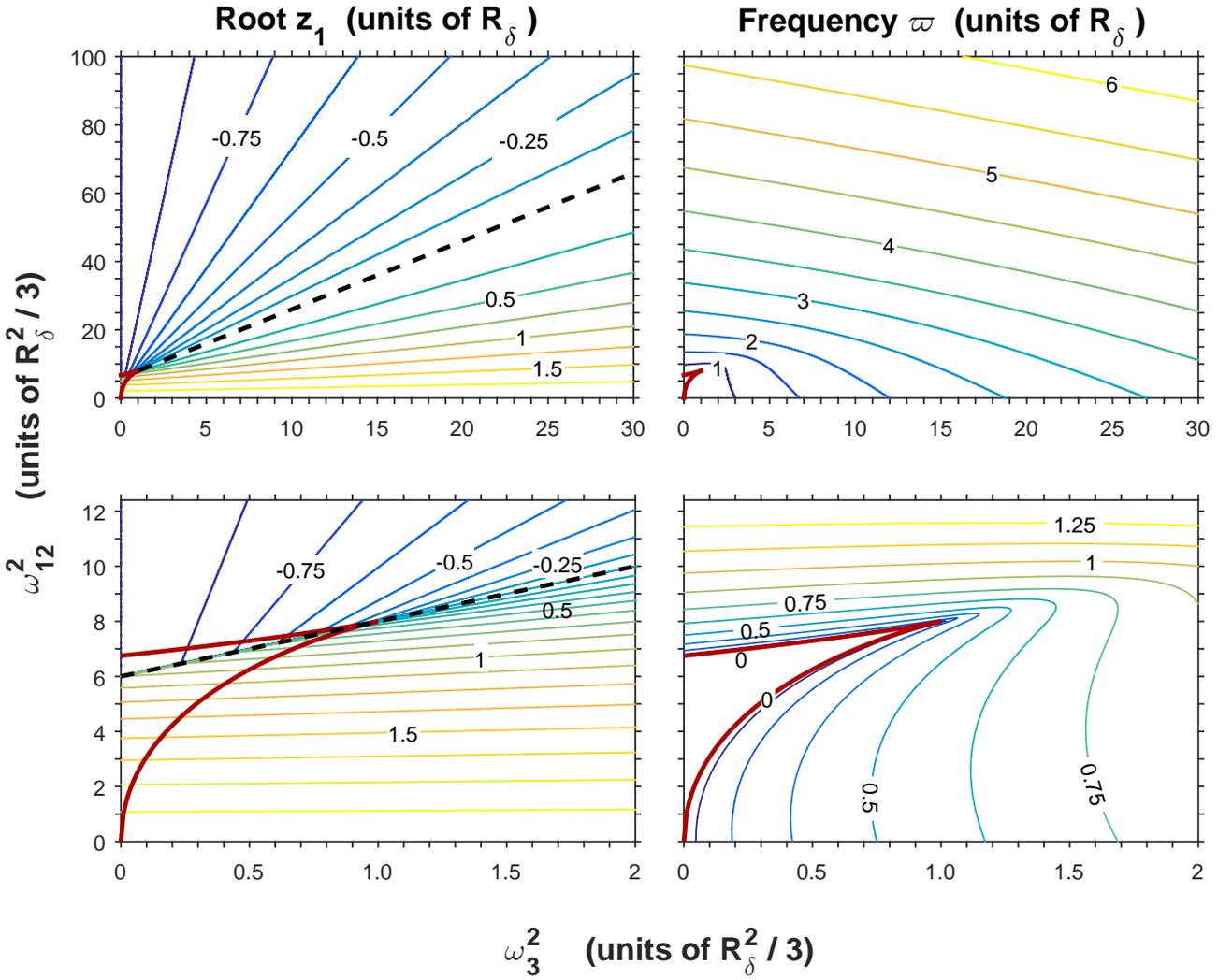


FIG. 2. Contours of the characteristic polynomial's guaranteed real root  $z_1$ , calculated according to Eqs. (C6) and normalized to  $R_\delta$ , are plotted as a function of  $\omega_{12}^2$  and  $\omega_3^2$  normalized as in Fig. 1. The root satisfies  $-1 \leq z_1 \leq 2$ , as expected from Eq. (51), with lines of constant  $z_1$  as derived in Eqs. (53–55). The  $z_1 = 0$  contour is shown as a dashed line. Contours of the frequency  $\varpi$  from Eq. (22) that appears in the oscillatory, underdamped solutions of the Bloch equation are also plotted in the rightmost panels. Within the overdamped region defined in Fig. 1 and expanded in the lower panels, there is no oscillation or frequency  $\varpi$ , and only one of the three real roots is plotted.

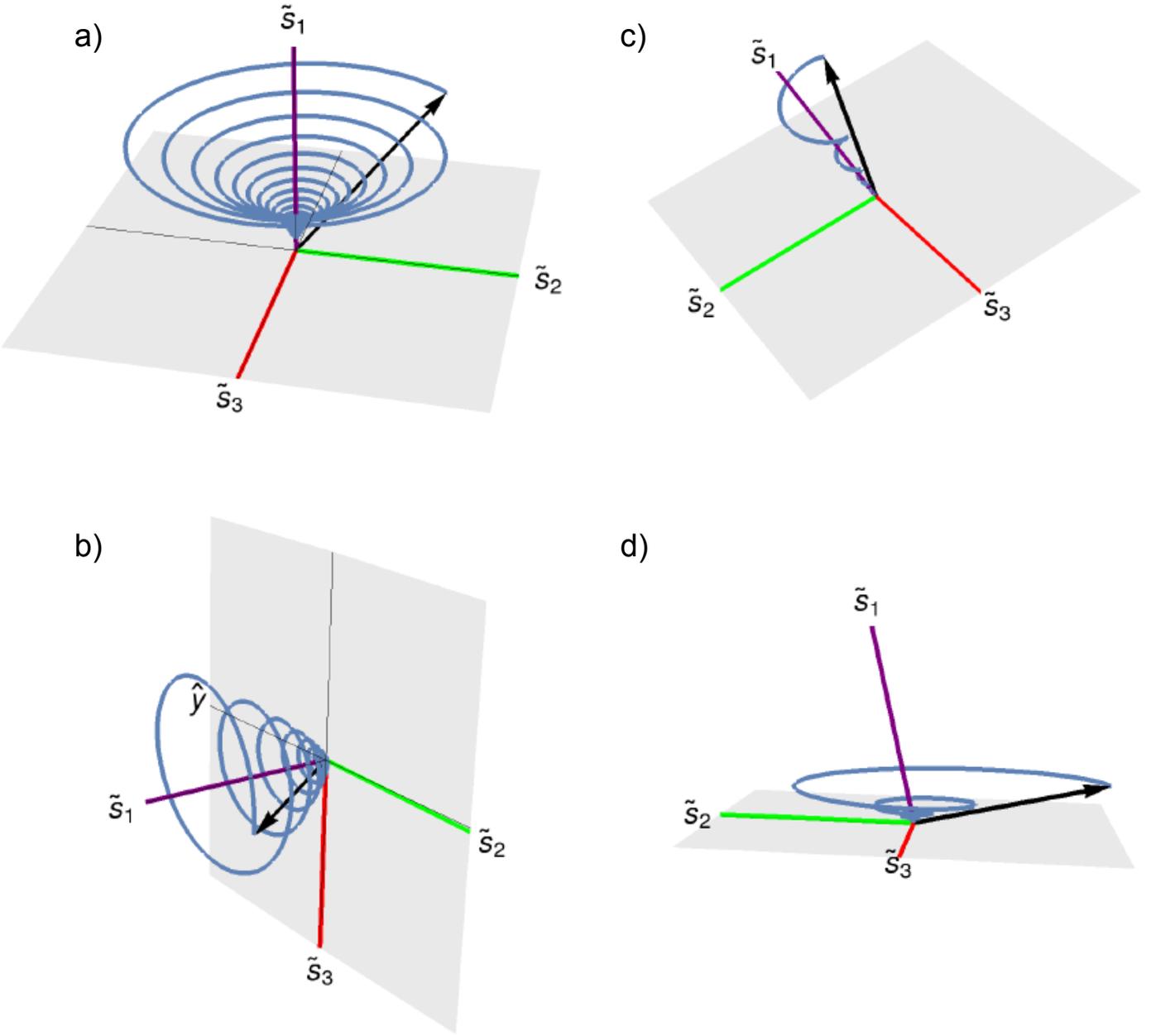


FIG. 3. Trajectories for initial vector  $\mathcal{M}_0$  acted upon by propagator  $e^{-\Gamma t}$  are displayed in the  $\{\tilde{s}_1, \tilde{s}_2, \tilde{s}_3\}$ -coordinates developed as the natural system for describing propagator dynamics. The component of  $\mathcal{M}_0$  along  $\tilde{s}_1$  decays at the rate  $\bar{R} - z_1$ , while components in the  $(\tilde{s}_2, \tilde{s}_3)$ -plane rotate in the plane and decay at the rate  $\bar{R} + z_1/2$ . The different panels represent different  $\mathcal{M}_0$ , fields  $\omega_e$ , transverse relaxation rate  $R_2$ , and longitudinal relaxation rate  $R_3$ , with details of the predicted system evolution described in more detail in the text. Physical parameters are in units inverse seconds. **(a)** Initial state  $\mathcal{M}_0 = (-1, 1, 1)$ . Physical parameters  $\omega_e = (0, 0, 10^4)$ ,  $R_2 = 400$ ,  $R_3 = 200$  give coordinates  $\tilde{s}_1 = \hat{z}$ ,  $\tilde{s}_2 = \hat{y}$ ,  $\tilde{s}_3 = \hat{x}$  and the well-known rotation about  $\omega_e = \omega_3$  followed by longitudinal and transverse relaxation. **(b)** Initial state  $\mathcal{M}_0 = (1, -1, 0)$ . Parameters  $\omega_e = (5000, 0, 0)$ ,  $R_2 = 400$ ,  $R_3 = 200$  lead to coordinates  $\tilde{s}_1 = \hat{x}$ ,  $\tilde{s}_2 = (0, -1, .02)$ ,  $\tilde{s}_3 = \hat{z}$ . Rotation is also about  $\omega_e$  for  $\omega_3 = 0$  (on resonance), but now  $\tilde{s}_2$  is not perpendicular to  $\tilde{s}_3$ , so the rotation in the plane transverse to  $\tilde{s}_1$  is not at constant angular frequency. **(c)** Parameters  $\omega_e = (0, 300, 300)$ ,  $R_2 = 100$ ,  $R_3 = 1$  lead to non-orthogonal oblique coordinates  $\tilde{s}_1 = (0.12, 0.69, 0, 71)$ ,  $\tilde{s}_2 = (0.99, 0.04, 0.12)$ ,  $\tilde{s}_3 = (0., 0.72, -0.70)$ . Initial  $\mathcal{M}_0 = (-0.12, 0.69, 0, 71)$  is normal to the  $(\tilde{s}_2, \tilde{s}_3)$ -plane, but has components in the plane and along  $\tilde{s}_1$  in the oblique coordinate system, so spirals about  $\tilde{s}_1$  as shown. **(d)** Initial  $\mathcal{M} = (-0.99, 0.17, 0)$  is orthogonal to  $\tilde{s}_1$ . Parameters  $\omega_e = (0, 3000, 3000)$ ,  $R_2 = 1000$ ,  $R_3 = 1$  lead to nearly identical coordinates as in (c).  $\mathcal{M}_0$  projects onto  $\tilde{s}_1$  in oblique coordinates and therefore decays along this direction, resulting in the spiral as shown.

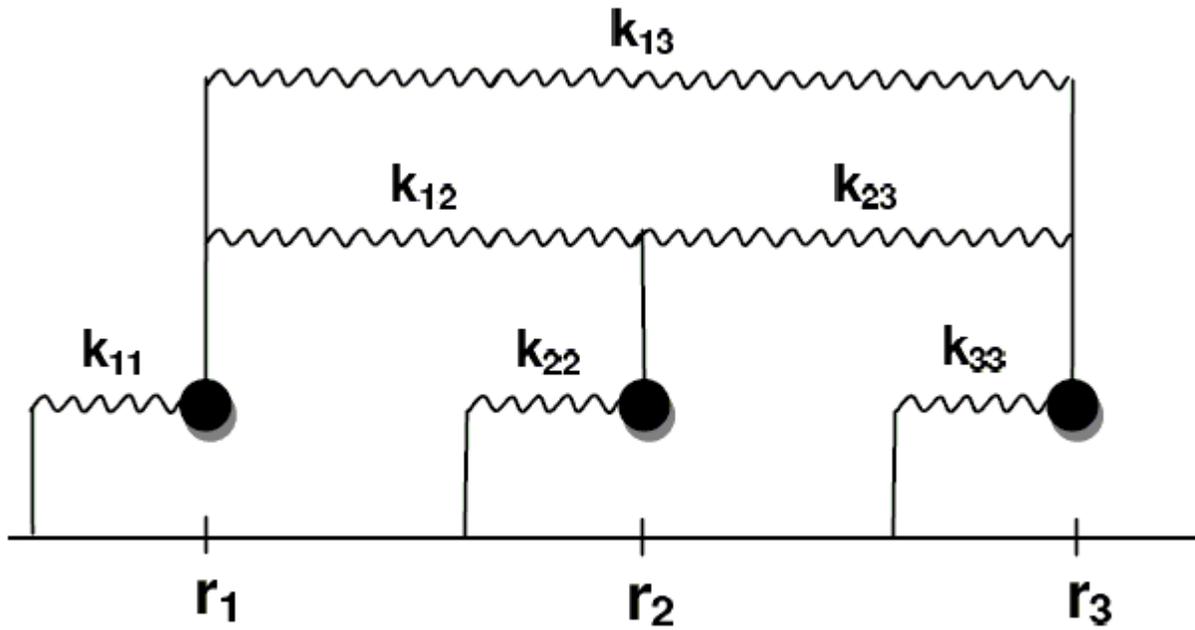


FIG. 4. The Bloch equation is shown in the text to model the displacements, from equilibrium positions  $r_i = 0$ , of a system of three unit masses coupled by springs of stiffness  $k_{ij}$ . One model identifies “velocity”-dependent damping terms. An alternative model is expressed as an ideal frictionless system that is, nonetheless, damped. Asymmetric couplings  $k_{ij} \neq k_{ji}$  provide a dissipative mechanism in both models. The mechanical springs depicted in the figure are therefore only an analogy.