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# Role of control constraints in quantum optimal control

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The problems of optimizing the value of an arbitrary observable of the two-level system at both a fixed time and the shortest possible time is theoretically explored. Complete identification and classification along with comprehensive analysis of globally optimal control policies and traps (i.e. policies which are locally but not globally optimal) is presented. The central question addressed is whether the control landscape remains trap-free if control constraints of the inequality type are imposed. The answer is astonishingly controversial: Although the traps are proven to always exist in this case, in practice they become trivially escapable once the control time is fixed and chosen long enough.

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## I. INTRODUCTION

Within the optimal control paradigm, efficient control of quantum dynamics is based on determination of the global maximum of the multidimensional “control landscape” with respect to the shapes of driving laser pulses or external magnetic fields. In the laboratory, the search usually involves sophisticated genetic algorithms [1]. This is a time-consuming procedure but it guarantees that the optimization will neither get “trapped” in the landscape’s sub-optimal local extrema nor faltered in the vicinity of a saddle point. The existence of “traps” is known both experimentally and theoretically [1–3]. At the same time, there are strong arguments that a large variety of control problems may be treated as trap-free from the practical perspective [4–9]. These arguments, however, assume the set of controls to be an open manifold. In practice, this is not the case: The magnitudes of applied fields are constrained by a number of competing strong-field processes (ionization, dissociation) and to a lesser extent by technical limitations. The overall effect of these constraints on the landscape topology is an open question. They are known, however, to dramatically influence the forms of the time-optimal controls (see e.g. [10–12]), which are highly relevant for quantum information applications.

In this paper we study in detail the constrained control landscape of the two-level Landau-Zener system representing the probably most fundamental model of a controlled qubit with a single control parameter, denoted below  $u$ . The corresponding master equation reads as

$$\rho(\tau) = U_{\tau,0}(u)\rho(0)U_{\tau,0}^\dagger(u), \quad (1)$$

with the unitary transformation  $U_{\tau'',\tau'}(u)$  defined as  $U_{\tau'',\tau'}(u) = \overrightarrow{\text{exp}}(-i \int_{\tau=\tau'}^{\tau''} (\hat{\sigma}_x + u(\tau)\hat{\sigma}_z) d\tau)$ . Here  $\rho$  is the system’s density matrix,  $\sigma_x$  and  $\sigma_z$  are Pauli matrices,  $\tau$  is a dimensionless time  $\tau = \alpha t$ , and the control parameter

is usually proportional to the interaction strength with an external controlled electric or magnetic field ( $u = \beta\mathcal{E}$  or  $u = \beta\mathcal{B}$ ). Depending on the physical meaning of the scaling factors  $\alpha$  and  $\beta$ , Eq. (1) can represent the wide variety of modern experiments, including magnetic and/or optical control of quantum dots [13], vacancy centers in crystals [14], spin states of atoms and molecules [12], Bose-Einstein condensates [15, 16] and superconducting circuits [17].

We consider the following optimal control problem:

$$J = \text{Tr}[\rho(T)\hat{O}] \rightarrow \max; \quad (2)$$

$$-u_{\max} \leq u \leq u_{\max}; \quad (3)$$

$$T < T_{\max}, \quad (4)$$

where maximization is with respect to the program (or control policy)  $\tilde{u}(\tau)$ , and possibly also the final time  $T$ . In the context of qubit design, for instance, the performance index (2) with  $\hat{O} = |1\rangle\langle 1|$  can represent the task of initial preparation of the qubit in a given initial pure state  $|1\rangle$ . Provided that the initial state of the system is  $|0\rangle$  ( $\langle 0|1\rangle = 0$ ), the optimal policy will effectively represent the realization of the SWAP quantum gate (up to undefined diagonal phase shifts). In this case, the bound (4) is motivated by the unrecoverable losses of operation fidelity due to uncontrollable decoherence at long times.

The key question of our study is the extent to which the restrictions (3), (4) complicate finding the policy  $\tilde{u}^{\text{opt}}(\tau)$  that maximizes the functional  $J[u(t)]$  (representing the system’s control landscape) using local search methods. The Landau-Zener system is special from this perspective since it is the only system for which the absence of traps in the unconstrained case (i.e. when  $u_{\max} = \infty$  in (3)) was formally proven [18–20]. Moreover, its complete controllability for any finite value of  $u_{\max}$  (provided that  $T_{\max}$  is chosen sufficiently long) was also justified [21–23]. Thus, this system provides opportunity to evaluate the effect of constraints (3) and (4) on the landscape complexity in the most pristine form. The existing data portend that this effect should be nontrivial. For example, the unconstrained time-optimal policies  $\tilde{u}(\tau)$  are shown to be  $\tilde{u}(\tau) = c'\delta(\tau) + c''\delta(\tau - T)$  where  $c'$  and  $c''$  are constants and  $\delta(\tau)$  is the Dirac delta function [25]. Such

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77 solutions are evidently inconsistent with any constraints 132  
78 of the form (3). 133

79 An additional feature of the Landau-Zener system is 134  
80 its simplicity, which allows us to analytically infer the 135  
81 topology of  $J[u]$ . At the same time, this system consti- 136  
82 tutes an elementary building block for describing the dy- 137  
83 namics of a variety of important quantum systems, from 138  
84 NMR controlled spin chains to laser-driven excitations 139  
85 in atoms, molecules and quantum dots. These features 140  
86 make the Landau-Zener system a lovely model whose an- 141  
87 alytical beauty could help to understand the fundamental 142  
88 controllability and regularity properties of generic quan- 143  
89 tum control.

90 It is worth noting that the restrictions (3) are critical 134  
91 in the foundation of modern theory of optimal control 135  
92 since the corresponding problems can not be solved in the 136  
93 framework of classical calculus of variations and require 137  
94 special methods, such as the Pontryagin's maximum prin- 138  
95 ciple (PMP) [10, 11]. For completeness of the presenta- 139  
96 tion, we provide in Sec. II and Appendix A a brief review 140  
97 of PMP and the known results of first-order analysis of 141  
98 the controlled Landau-Zener system in the PMP frame- 142  
99 work. In particular, we clarify why the unconstrained 143  
100 problem (2) is trap-free, and introduce the primary clas- 144  
101 sification of the stationary points (i.e. the locally and 145  
102 globally optimal solutions, traps and saddle points) by 146  
103 showing that, in the case of time-optimal control, all of 147  
104 them, and likewise traps and saddle points in the case of 148  
105 fixed time control, are represented by piecewise-constant 149  
106 controls  $\tilde{u}(\tau)$  that can take only 3 values: 0 and  $\pm u_{\max}$ .

107 The rest of the paper is organized as follows. In Sec. III 134  
108 we derive a comprehensive set of criteria that allow to 135  
109 outline the landscape profile and distinguish among its 136  
110 various types of stationary points. The obtained criteria 137  
111 substantially extend, generalize or specialize a number of 138  
112 known results [24–27] obtained for related problems using 139  
113 the index theory [28] or methods of optimal syntheses on 140  
114 2-D manifolds [29]. In this work we propose the technique 141  
115 of “sliding” variations, which allows to reduce the high- 142  
116 order analysis to methodologically simple and intuitively 143  
117 appealing geometrical arguments.

118 In sections IV and V we apply these criteria to identify 134  
119 and classify the traps and saddle points for the cases 135  
120 of time-optimal and time-fixed control, respectively. A 136  
121 brief summary of the obtained results and the general 137  
122 conclusions that follow from this analysis are given in 138  
123 the final section VI.

124 We recommend readers who are interested primarily 134  
125 in physical rather than formal mathematical content of 135  
126 the paper to skip directly to concluding section VI after 136  
127 reviewing Section II and Appendix A, and then, if neces- 137  
128 sary, refer to sections III–V for details. For convenience, 138  
129 the key results of the these sections are compactly form- 139  
130 ulated in the form of 16 propositions whose proofs are 140  
131 deferred to Appendices B–J.

## II. REGULAR AND SINGULAR OPTIMAL POLICIES

134 In this section, we review the first-order analysis of 135  
135 problem (1) with constraint (3) in the PMP framework. 136  
136 For completeness, we sketch in more detail the basics of 137  
137 the Pontryagin theory and outline the derivations of key 138  
138 statements and relations of this section in Appendix A. 139  
139 For further details, we refer interested readers to the ex- 140  
140 tensive literature on this topic, e.g. [11], pp.280-286, [24]. 141  
141 PMP provides the necessary criterion of local optimality 142  
142 of control  $u(\tau)$  in terms of the Hamilton-type Pontryagin 143  
143 function  $K(\rho(\tau), \hat{O}(\tau), u(\tau))$ ,

$$\tilde{u}(\tau) = \arg \max_{u(\tau)} K(\tilde{\rho}(\tau), \tilde{\hat{O}}(\tau), u(\tau)). \quad (5)$$

144 Here the matrix elements of the operator  $\tilde{\hat{O}}$  represent 134  
145 the set of so-called costate (or adjoint) variables (see Ap- 135  
146 pendix A). The processes satisfying the PMP are called 136  
147 stationary points, or extremals, and will be denoted by 137  
148  $\tilde{\cdot} : \{\tilde{u}(\tau), \tilde{\rho}(\tau), \tilde{\hat{O}}(\tau)\}$ .

149 The explicit form of the Pontryagin function of the 134  
150 control problem (1), (2) is

$$K(\rho(\tau), \hat{O}(\tau), u(\tau)) = -i \text{Tr} \left\{ [\rho(\tau), \hat{O}(\tau)] (\hat{\sigma}_x + u(\tau) \hat{\sigma}_z) \right\}, \quad (6)$$

151 the evolution equation for  $\hat{O}(\tau)$  coincides with (1),

$$\hat{O}(\tau'') = U_{\tau'', \tau'}(u) \hat{O}(\tau') U_{\tau'', \tau'}^\dagger(u), \quad (7)$$

152 and the boundary conditions read as

$$\hat{O}(T) = \hat{O}; \quad (8)$$

$$K(T) \begin{cases} = 0 & \text{if } T \text{ is unconstrained;} \\ \geq 0 & \text{in the case (4).} \end{cases} \quad (9)$$

153 Since the Pontryagin function (6) depends linearly on 134  
154  $u(\tau)$ , the PMP can be satisfied in two ways:

- 155 1) The switching function 134  
156  $\frac{\partial}{\partial u(\tau)} K = -i \text{Tr} \left\{ [\rho(\tau), \hat{O}(\tau)] \hat{\sigma}_z \right\} \neq 0$ , and 135  
157  $\tilde{u}(\tau) = u_{\max} \text{sign} \left( \frac{\partial}{\partial u(\tau)} K \right)$ . The corresponding section 136  
158 of the trajectory is called regular. In this case 137  
159 the optimal policy  $\tilde{u}(\tau)$  is actively constrained, so 138  
160 that relaxing the constraints (3) will improve the 139  
161 optimization result. For this reason, the optimal 140  
162 trajectory containing the regular sections can not 141  
163 be kinematically optimal. An optimal process 142  
164  $\{\tilde{\rho}(\tau), \tilde{\hat{O}}(\tau), \tilde{u}(\tau)\}$  for which  $\tilde{u}(\tau) = \pm u_{\max}$  everywhere 143  
165 except for a finite number of time moments is often 144  
166 referred to as bang-bang control.
- 167 2) It may happen that the switching function remains 134  
168 equal to zero over a finite interval of time. The corre- 135  
169 sponding segment of the trajectory is called singular,

and the associated optimal control can be determined only from higher-order optimality criteria, such as the generalized Legendre-Clebsch conditions or Goh condition [11, 30, 31].

Substituting (1) and (7) into (6), one can directly check that the Pontryagin function for problem (1) is constant along any extremal,

$$\forall \tau : K(\tau) = \tilde{K} \geq 0 \text{ on each extremal,} \quad (10)$$

where the strict inequality holds only if the constraint (4) is active, and

$$\forall \tau : K(\tau) \equiv 0 \text{ for any kinematically optimal solution.} \quad (11)$$

### A. Singular extremals of the problem (1)

Every kinematically optimal solution  $\tilde{u}(\tau)$  consist of a single singular subarc. Here we show that in the case of the Landau-Zener system the converse is also true: every singular extremal  $\tilde{u}(\tau)$  corresponding to an inactive constraint (4) delivers the global kinematic extremum (maximum or minimum) to the problem (2). Indeed, let  $\tau_1$  be an arbitrary internal point of the singular trajectory. The PMP states that

$$\frac{\partial}{\partial u(\tau)} K(\tau) = -i \operatorname{Tr} \left\{ [\rho(\tau_1), \hat{O}(\tau_1)] U_{\tau, \tau_1}^\dagger(\tilde{u}) \hat{\sigma}_z U_{\tau, \tau_1}(\tilde{u}) \right\} \equiv 0 \quad (12)$$

for any  $\tau$  such that  $|\tau - \tau_1| < \epsilon$  for a sufficiently small  $\epsilon$ . In particular,

$$-i \operatorname{Tr} \left\{ [\rho(\tau_1), \hat{O}(\tau_1)] \hat{\sigma}_z \right\} = 0. \quad (13a)$$

The two subsequent time derivatives of the equality (12) at  $\tau = \tau_1$  give

$$-i \operatorname{Tr} \left\{ [\rho(\tau_1), \hat{O}(\tau_1)] \hat{\sigma}_y \right\} = 0; \quad (13b)$$

$$-i \tilde{u}(\tau_1) \operatorname{Tr} \left\{ [\rho(\tau_1), \hat{O}(\tau_1)] \hat{\sigma}_x \right\} = 0. \quad (13c)$$

Equations (13) can be simultaneously satisfied only in two cases:

$$[\rho(\tau), \hat{O}(\tau)] = 0; \quad (14a)$$

$$[\rho(\tau), \hat{O}(\tau)] = i\kappa \hat{\sigma}_x \text{ and } u(\tau) = 0 \text{ } (\kappa = \text{const} \neq 0). \quad (14b)$$

The condition (14a) is nothing but the criterion of the global kinematic extremum (maximum or minimum) for our two-level system. In other words, we showed that all the extrema of the landscape  $J(u)$  for the unconstrained Landau-Zener system except for the case of  $u(t) \equiv 0$  are its global kinematic maxima and minima. This result was obtained in [18, 19].

The condition (14b) indicates that the only possible everywhere singular non-kinematic extremal of the problem (2) is  $\tilde{u}(\tau) \equiv 0$  ( $\tau \in [0, T]$ ). Eq. (6) implies that  $K(\tau) = \kappa$  in this case. Thus, in view of (9), this extremal can appear only when the constraint (4) is active.

### B. Regular and mixed extremals of the problem (1)

According to the PMP and conditions (14), the generic non-singular extremal is the piecewise-constant function with  $n$  switchings of either bang ( $u = \pm u_{\max}$ ) or bang-singular ( $u = \pm u_{\max}, 0$ ) type, where the singular arcs match (14b). For brevity, we will refer to extremals with (without) singular arcs as of type II (type I). We will use the subscript  $i$  (i.e.  $\tilde{\tau}_i, \tilde{\rho}_i$  etc.,  $0 < i < n+1$ ) for the parameters related to the  $i$ -th control discontinuity (corner point). The durations of the right (left) adjacent arcs and the associated values of  $u$  will be labeled  $\tilde{\Delta}\tau_i$  ( $\tilde{\Delta}\tau_{i-1}$ ) and  $\tilde{u}_i^+$  ( $\tilde{u}_i^-$ ). The subscripts  $i=0$  and  $i=n+1$  will be reserved for the parameters of the trajectory endpoints. We will also sometimes use the notations  ${}^s\text{I}$  and  ${}^s\text{II}$  with index  $s$  denoting the number of times the control changes sign.

Let us first address the properties of type I extremals. The necessary condition of the  $i$ -th corner point is given by eq. (13a). Combining it with (10) we get

$$-i[\tilde{\rho}(\tilde{\tau}_i), \tilde{O}(\tilde{\tau}_i)] = c_{i,1} \hat{\sigma}_x + c_{i,2} \hat{\sigma}_y, \quad c_{i,1}, c_{i,2} \in \mathbb{R}, \quad (15)$$

where  $c_{i,1} = 0 (>0)$  when the constraint (4) is inactive (active) and the case  $c_{i,1} \leq 0$  can result from optimization with a fixed  $T$ . Consider the adjacent  $(i+1)$ -th bang arc. The PMP criterion (5) for its interior reads as

$$\tilde{u}(\tau)|_{\tau > \tilde{\tau}_i} = \arg \max_u \operatorname{Tr} [U_{\tau, \tilde{\tau}_i}(c_{i,1} \hat{\sigma}_x + c_{i,2} \hat{\sigma}_y) U_{\tau, \tilde{\tau}_i}^{-1} \hat{\sigma}_z] u, \quad (16)$$

which gives  $\tilde{u}_i^+ = \frac{c_{i,2}}{|c_{i,2}|} u_{\max}$ . If the  $(i+1)$ -th arc ends with another corner point  $\tilde{\tau}_{i+1}$ , then it follows from (16) that

$$\operatorname{Tr} [U_{\tilde{\tau}_{i+1}, \tilde{\tau}_i}(c_{i,1} \hat{\sigma}_x + c_{i,2} \hat{\sigma}_y) U_{\tilde{\tau}_{i+1}, \tilde{\tau}_i}^{-1} \hat{\sigma}_z] = 0. \quad (17)$$

Condition (17) can be reduced to

$$c_{i,2} \sqrt{u_{\max}^2 + 1} = -c_{i,1} \tilde{u}_i^+ \tan(\tilde{\Delta}\tau_i \sqrt{u_{\max}^2 + 1}) \quad (18)$$

and resolved relative to  $\tilde{\Delta}\tau_{i+1}$ . Retaining the physically appropriate solutions consistent with eq. (16) we obtain:

$$\tilde{\Delta}\tau_{i+1} = \begin{cases} \tilde{\delta}\tau_i, & c_{i,1} < 0; \\ \pi \cos(\alpha) - \tilde{\delta}\tau_i, & c_{i,1} > 0, \end{cases} \quad (19)$$

where  $\alpha = \arctan(u_{\max})$  and

$$\tilde{\delta}\tau_i = \arctan \left( \left| \frac{c_{2,i}}{c_{1,i} u_{\max}} \right| \sec(\alpha) \right) \cos(\alpha). \quad (20)$$

Note that  $-i[\tilde{\rho}(\tilde{\tau}_{i+1}), \tilde{O}(\tilde{\tau}_{i+1})] = c_{1,i} \hat{\sigma}_x - c_{2,i} \hat{\sigma}_y$ , i.e.

$$c_{1,i+1} = c_{1,i}, \quad c_{2,i+1} = -c_{2,i}. \quad (21)$$

Since eqs. (19) and (20) do not depend on the sign of  $c_{i,2}$ , one obtains that the durations of all interior bang segments are equal:  $\forall i \geq 1, i < n : \tilde{\Delta}\tau_i = \tilde{\Delta}\tau$  (see Fig. 1a). Moreover, eq. (19) admits the estimate

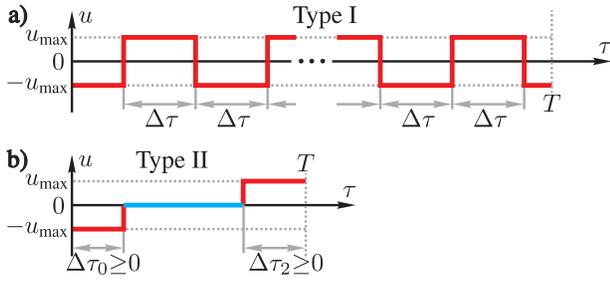


FIG. 1. Possible types of extremals  $\tilde{u}(t)$  associated with non-kinematic optimal solutions and traps along with the locally time-optimal kinematic optimal solutions.

239  $\frac{\pi}{2} \cos \alpha \leq \Delta\tau \leq \pi \cos \alpha$  for the case of time-optimal prob-  
240 lem with constraint (4).

241 Consider now the extremals of type II. Let  $\tau \in (\tilde{\tau}_{j-1}, \tilde{\tau}_j)$   
242 be the singular arc where the relations (14b) hold. If  
243  $\tilde{\tau}_j \neq T$  when the time instant  $\tau = \tilde{\tau}_j$  corresponds to the cor-  
244 ner point between regular and singular arc. Suppose that  
245 there exists another corner point at  $\tau = \tau_{j+1} > \tilde{\tau}_j$ . Then it  
246 follows from eqs. (21) (19) and (17) that  $\Delta\tilde{\tau}_j = \pi \cos \alpha$   
247 and  $U_{\tilde{\tau}_{j+1}, \tilde{\tau}_j} = -\hat{I}$ , so that  $\tilde{\rho}(\tilde{\tau}_{j+1}) = \tilde{\rho}(\tilde{\tau}_j)$ . Using similar  
248 arguments, it is straightforward to derive the analogous  
249 result for possible corner points prior to  $\tau_j$ . Thus, taking  
250 any 3-segment ‘‘ansatz’’ extremal similar to that shown in  
251 Fig. 1b, one can construct an infinite family  $\mathcal{F}^{[k]}(\tilde{u}(\tau))$  of  
252  $\text{II}^{[k]}$  extremals ( $k=k_1, k_2$ ) by randomly inserting  $k_1$  and  
253  $k_2$  bang segments of length  $\pi \cos \alpha$  with  $u = +u_{\max}$  and  
254  $u = -u_{\max}$  into corner points of  $\tilde{u}(\tau)$  or inside its singular  
255 arcs. It is clear that each family  $\mathcal{F}^{[k]}(\tilde{u}(\tau))$  constitutes  
256 the connected set of solutions, and all the members have  
257 equal performances  $J$ . Thus, the properties of any type  
258 II extremal can be reduced to the analysis of the equiv-  
259 alent three-segment  ${}^0\text{II}$  type or  ${}^1\text{II}$  type extremal, where  
260 all the positive and negative bang segments are merged  
261 into distinct continuous arcs separated by a singular arc.

262 The presented first-order analysis outlines the admis-  
263 sible profiles for optimal non-kinematic solutions (see  
264 Fig. 1). Moreover, by continuity argument (i.e. by con-  
265 sidering the series of solutions with fixed  $T \rightarrow T_{\text{opt}}$  from  
266 below), these profiles should embrace all possible types of  
267 the stationary points of the time-optimal problem (2),(4).  
268 It is worth stressing that the latter include the globally  
269 optimal and everywhere singular kinematic solutions for  
270 which both segments with  $u = \pm u_{\max}$  and  $u = 0$  are singu-  
271 lar. With this in mind, it is helpful to introduce the  
272 following terminological convention for the rest of the pa-  
273 per in order to avoid potential confusions: we will reserve  
274 the term ‘‘singular’’ exclusively for segments of extremals  
275 at which  $u = 0$  whereas segments with  $u = \pm u_{\max}$  will be  
276 always referred to as ‘‘bang’’ ones.

277 The reviewed results have several serious limitations.  
278 First, they do not allow to distinguish the globally time-  
279 optimal solution from a trap or a saddle point. Second,  
280 they do not provide *a priori* knowledge of the characteris-  
281 tic structural features of these stationary points (e.g. the

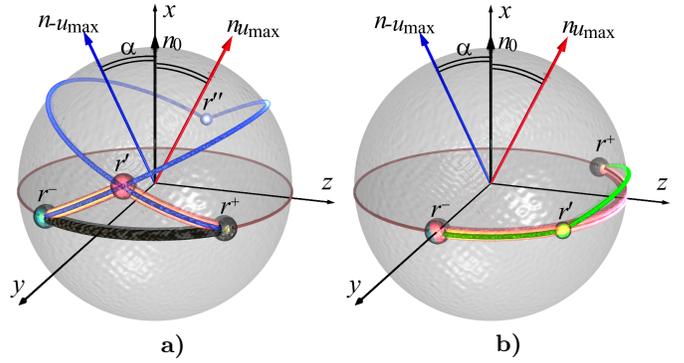


FIG. 2. (a) The case  $r_y^- r_y^+ > 0$ : The equatorial singular arc  
 $r^- \rightarrow r^+$  (thick black line) is more time-effective than the bang-  
bang extremal  $r^- \rightarrow r' \rightarrow r^+$  (thick orange line). The extremal  
 $r^- \rightarrow r'' \rightarrow r^+$  (thin blue curve) represents a local extremum  
(trap). (b) The case  $r_y^- r_y^+ < 0$ : The equatorial singular arc  
 $r^- \rightarrow r^+$  (thick orange line) is suboptimal relative to the bang-  
singular extremal  $r^- \rightarrow r' \rightarrow r^+$  (thin black line).

282 expected type, number of switchings etc.) which is nec-  
283 essary to determine the topology of the landscape  $J[u]$ .  
284 These tasks require higher-order analysis, which is the  
285 subject of the next section.

### 286 III. DETAILED CHARACTERIZATION OF THE 287 STATIONARY POINTS

288 In this section we will extensively use geometrical argu-  
289 ments in our reasoning. To make the presentation more  
290 visual, it is useful to expand the states and observables  
291 in the basis of Pauli matrices and identity matrix  $\hat{I}$ :  
292  $\rho = \frac{1}{2} \hat{I} + \sum_{i=x,y,z} r_i \hat{\sigma}_i$ ,  $\hat{O} = \frac{1}{2} \text{Tr}[\hat{O}] \hat{I} + \sum_{i=x,y,z} o_i \hat{\sigma}_i$ . The  
293 dynamics induced by eq. (1) corresponds to rotation of  
294 the 3-dimensional Bloch vector  $\vec{r} = \{r_x, r_y, r_z\}$  about the  
295 axis  $\vec{n}_u \propto \{1, 0, u\}$  (note that the angle between  $\vec{n}_{\pm u_{\max}}$   
296 and  $\vec{n}_0$  is equal to  $\alpha$ , see e.g. Fig. 2), and the optimiza-  
297 tion goal (2) is equivalent to the requirement to arrange  
298 the state vector  $\vec{r}$  in parallel to  $\vec{o}$ . In what follows we will  
299 often refer to the quantum states  $\rho$  as the endpoints  $r$  of  
300 vectors  $\vec{r}$ . Hereafter we will also assume that both  $r$  and  
301  $o$  are renormalized such that  $|r| = |o| = 1$ .

302 We start by taking a closer look at type II extremals  
303 and their singular arc(s) where  $\tilde{u}(\tau) = 0$ . According to cri-  
304 terion (14b), these arcs are always located at the equato-  
305 rial plane  $x = 0$ . The following proposition indicates that  
306 such arcs may represent the time-optimal solution at any  
307 values of  $u_{\max}$  (see Appendix B for proof):

308 **Proposition 1.** *The shortest type II singular trajectory*  
309 *connecting any two ‘‘equatorial’’ points  $\vec{r}^- = \{0, r_y^-, r_z^-\}$*   
310 *and  $\vec{r}^+ = \{0, r_y^+, r_z^+\}$  (see Fig. 2) will represent the (glob-*  
311 *ally) time-optimal solution if  $r_y^- r_y^+ > 0$ ,  $(r_z^+ - r_z^-) r_y^- > 0$*   
312 *and a saddle point otherwise.*

313 Since all  ${}^s\text{II}$  extremals can be reduced to the effective  
314 3-segment ansatz shown in Fig. 1b (see the end of the

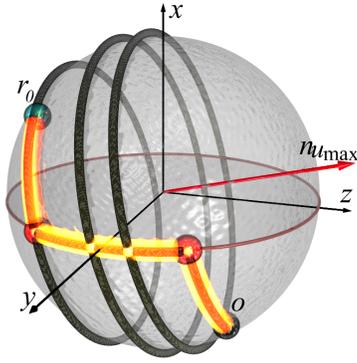


FIG. 3. The globally time-optimal  ${}^0\text{II}$  type trajectory  $\tilde{u}_{\text{anz}}(\tau)$  (thick bright yellow curve) and the locally time-optimal trapping solution (black curve) of the  $\mathcal{F}^{[3]}(\tilde{u}^{\text{anz}}(\tau))$  family connecting the points  $r_0 \propto \{1, 1, -1\}$  and  $o \propto \{-1, 1, 1\}$ .

previous section), Proposition 1 has the evident corollary:

**Proposition 2.** *All singular arcs of the locally optimal type II extremals are located in the same semi-space  $y > 0$  or  $y < 0$ , and their total duration can not exceed  $\pi/2$ .*

For further analysis we need the following generic necessary condition for time optimality:

**Proposition 3.** *If the type I extremal  $\{\tilde{u}(\tau), \tilde{r}(\tau)\}$  is locally time-optimal then each of its corner points  $\tilde{r}_i$  satisfies the inequality*

$$\tilde{u}_i^- \tilde{r}_{i,x} \tilde{r}_{i,y} \geq 0. \quad (22)$$

Qualitatively, Proposition 3 states that the projections of optimal trajectories on the  $xz$ -plane are always "V"-shaped at the corner points  $\tilde{r}_i$  with  $\tilde{r}_{i,x} > 0$  and "Λ"-shaped otherwise (here we assume that the  $x$ -axis is oriented vertically, like in Fig. 2).

This result allows us to substantially narrow down the range of type II candidate trajectories:

**Proposition 4.** *Any type  ${}^s\text{II}$  extremal with  $s > 0$  containing an interior bang arc is a saddle point for time-optimal control.*

In other words, all type  ${}^s\text{II}|_{s>0}$  locally time-optimal solutions reduce to the three-segment ansatz shown in Fig. 1b, where two regular arcs of duration  $\tilde{\Delta}\tau_0, \tilde{\Delta}\tau_2 < \pi \sec \alpha$  "wrap" the singular section where  $u=0$ . Accordingly, the number of control switchings is bounded by  $n_{\text{II}} \leq 2$ .

The properties of  ${}^0\text{II}$  type extremals are richer:

**Proposition 5.** *Suppose that the  ${}^0\text{II}$  type extremal  $\tilde{u}(\tau)$  is the member of family  $\mathcal{F}^{[k]}(\tilde{u}^{\text{anz}}(\tau))$ , and its ansatz  $\tilde{u}^{\text{anz}}(\tau)$  includes opening and closing bang segments of durations  $\tilde{\Delta}\tau_0 > 0$  and  $\tilde{\Delta}\tau_2 > 0$ . Then  $\tilde{u}(\tau)$  is locally optimal iff  $\tilde{u}^{\text{anz}}(\tau)$  is locally optimal.*

(for proof see Appendix E).

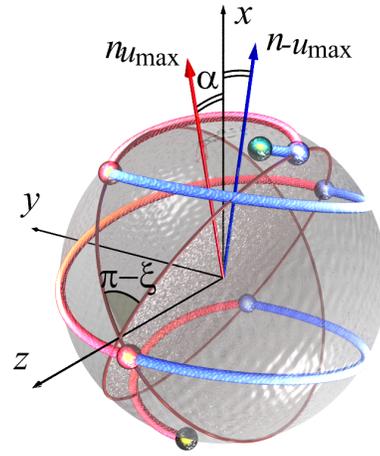


FIG. 4. Illustration of the statement of Proposition 6. The thick colored curve depicts the band-bang extremal. Its red and blue segments correspond to  $u = +u_{\text{max}}$  and  $u = -u_{\text{max}}$ . All interior corner points (red and blue balls) lie on two circles (associated with switchings  $u_{\text{max}} \rightarrow -u_{\text{max}}$  and  $-u_{\text{max}} \rightarrow u_{\text{max}}$ , respectively) whose planes  $\lambda_{\pm 1}$  intersect along the  $z$ -axis.

The analysis of type I extremals is somewhat more complicated. We begin by determining the loci of corner points  $\tilde{r}_i$  on the Bloch sphere. Denote as  $\theta = 2\tilde{\Delta}\tau \sec \alpha$  the rotation angles on the Bloch sphere associated with the inner bang sections of the type I extremals. Note that it follows from (19), (20) that  $\pi < \theta < 2\pi$  in the case of a time-optimal control problem.

**Proposition 6.** *All the corner points  $\tilde{r}_i$  of any locally optimal type I solution  $\tilde{u}(\tau)$  of the problem (2), (3) are located on the circular intersections of the Bloch sphere with the two planes  $\lambda_{\pm 1}$  (see Fig. 4),*

$$\tilde{r}_i = \left\{ \text{sign}(\tilde{u}_i^+) \sin(\gamma_i) \sin\left(\frac{\xi}{2}\right), -\sin(\gamma_i) \cos\left(\frac{\xi}{2}\right), \cos(\gamma_i) \right\}. \quad (23)$$

Here  $\xi = -2 \arctan\left(\frac{u_{\text{max}}}{2} \tan\left(\frac{\theta}{2}\right) \cos(\alpha)\right)$  is the dihedral angle between the planes  $\lambda_{\pm 1}$ , and  $\gamma_{i+1} = \gamma_i + i\eta$ , where  $\eta = -2 \arctan\left(\frac{\sin(\frac{\theta}{2})}{\sqrt{u_{\text{max}}^2 + \cos^2(\frac{\theta}{2})}}\right)$ .

**Proposition 7.** *Denote  $q_i = q(\gamma_i) = \cot^2(\gamma_i) - \cot^2(\frac{\eta}{2})$  ( $i=1, \dots, n$ ). The set  $\{q_i\}$  associated with any locally time-optimal extremal  $\tilde{u}(t)$  contains at most one negative entry  $q'$ , and  $|q'| = \min(|\{q_i\}|)$ .*

The proofs of the above two propositions are given in Appendix F.

To use Proposition 7, it is convenient to introduce parameters  $\zeta_i$  through,  $\zeta_1 = \gamma_1 + \frac{\pi}{2}(1 - \text{sign}(u_1^+))$ ,  $\zeta_{i+1} = \zeta_1 + i(\pi + \eta)$ . It is evident that  $q(\gamma_i) = q(\zeta_i)$ . The relation between the sign of  $q_i$  and the index  $i$  of the corner point can be illustrated by associating each  $q_i$  with the point on the unit circle whose position is specified by  $\zeta_i$ , as shown

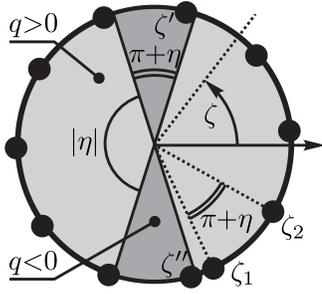


FIG. 5. Signs of the parameters  $q(\zeta)$  as function of  $\zeta$ . Black dots indicate the values  $\zeta = \zeta_i$  associated with  $i$ -th corner point.

in Fig. 5. One can see that the maximal number  $n_{\max}$  of sequential parameters  $q_i$  having at most one negative term can not exceed  $\frac{\pi + |\eta|}{\pi - |\eta|} + 1 \leq \frac{\pi}{\alpha}$ , i.e.,

**Proposition 8.** *Type I locally optimal extremals can have at most  $\frac{\pi}{\alpha}$  switchings.*

This helpful upper bound was first obtained by Agrachev and Gamkrelidze [27]. As shown in Appendix G, we can further refine this result via more detailed inspection of the criterion  $|q'| = \min(|\{q_i\}|)$  as follows:

**Proposition 9.**  $n_{I, \max} \leq 2$  if  $u_{\max} > \sqrt{1 + \sqrt{2}}$

(The latter roughly corresponds to  $\alpha > 1$ ).

The analysis in this section so far is equally valid for both global and local extrema of optimal control. It is clear that any globally time-optimal type II solution includes at most 2 corner points that separate the central singular section from the outside regular arcs (see Fig. 1b). The case of type I solutions is not as evident. The following propositions impose more stringent necessary criteria on the globally time-optimal extremals (see Appendices H and I for proofs).

**Proposition 10.** *Any corner point  $\tilde{r}_i$  such that  $q(\gamma_{i'}) < 0$  must be either the first or the last corner point of the globally time optimal solution, so that the total number of switchings  $n_{I, \max} \leq \frac{\pi}{2\alpha} + 1$ .*

**Proposition 11.** *The corner points  $\tilde{r}_i$  of any globally optimal solution of type I satisfy the inequality*

$$\min(0, \tilde{r}_{0,x}, \tilde{r}_{n+1,x}) < \tilde{r}_{i,x} < \max(0, \tilde{r}_{0,x}, \tilde{r}_{n+1,x}), \quad (24)$$

where  $\tilde{r}_{0,x}$  and  $\tilde{r}_{n+1,x}$  are the trajectory endpoints.

Proposition 11 can be used to establish the following, more accurate, upper bound on the number of switchings (see Appendix J for proof).

**Proposition 12.** *The number of corner points of the globally time-optimal type I solution  $\tilde{u}(\tau)$  is bounded by the following inequalities:*

$$n_{I \leq} \begin{cases} \max \left( \frac{\arccos(\frac{\tilde{r}_x^-}{\tilde{r}_x^+})}{|2 \arctan(\frac{u_{\max}}{\tilde{r}_x^+})|}, \frac{\pi}{|2 \arctan(\frac{u_{\max}}{\tilde{r}_x^-})|} \right) + 1 & \text{if } \tilde{r}_x^- \tilde{r}_x^+ < 0; \\ \min \left( \frac{\arccos(\frac{\tilde{r}_x^-}{\tilde{r}_x^+})}{|2 \arctan(\frac{u_{\max}}{\tilde{r}_x^+})|} + 3, \frac{\pi}{|4 \arctan(\frac{u_{\max}}{\tilde{r}_x^-})|} \right) + 1 & \text{if } \tilde{r}_x^- \tilde{r}_x^+ > 0, \end{cases} \quad (25a)$$

$$n_{I \leq} \begin{cases} \max \left( \frac{\arccos(\frac{\tilde{r}_x^-}{\tilde{r}_x^+})}{|2 \arctan(\frac{u_{\max}}{\tilde{r}_x^+})|}, \frac{\pi}{|2 \arctan(\frac{u_{\max}}{\tilde{r}_x^-})|} \right) + 1 & \text{if } \tilde{r}_x^- \tilde{r}_x^+ < 0; \\ \min \left( \frac{\arccos(\frac{\tilde{r}_x^-}{\tilde{r}_x^+})}{|2 \arctan(\frac{u_{\max}}{\tilde{r}_x^+})|} + 3, \frac{\pi}{|4 \arctan(\frac{u_{\max}}{\tilde{r}_x^-})|} \right) + 1 & \text{if } \tilde{r}_x^- \tilde{r}_x^+ > 0, \end{cases} \quad (25b)$$

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where  $\tilde{r}^+$  and  $\tilde{r}^-$  are new notations for the trajectory endpoints  $\tilde{r}_0$  and  $\tilde{r}_{n+1}$ , such that  $|\tilde{r}_x^+| \geq |\tilde{r}_x^-|$ .

Denote  $\phi_\xi = |\theta_{r_0, \xi} - \theta_{o, \xi}|$  ( $\xi = x, z$ ), where  $\theta_{r, \xi}$  is the angle between the axes  $\vec{e}_\xi$  and  $\vec{r}$ . One can geometrically show that the maximum possible change  $\Delta \theta_{r, \xi}^{\max}$  in  $\theta_{r, \xi}$  generated by rotation about any of the axes  $\vec{n}_{\pm u_{\max}}$  is  $\Delta \theta_{r, x}^{\max} = 2\alpha$  and  $\Delta \theta_{r, z}^{\max} = \pi - 2\alpha$  (see Fig. 6). This result allows us to establish the following lower bounds on the number of corner points:

**Proposition 13.** *The minimum number of corner points in locally time-optimal solutions reaching the global max-*

imum of  $J$  is bounded by the inequalities

$$n \geq \frac{|\arcsin(r_{0,x}) - \arcsin(o_x)|}{2 \arctan(u_{\max})} - 1; \quad (26a)$$

$$n_{I \geq} \frac{|\arcsin(r_{0,z}) - \arcsin(o_z)|}{2 \operatorname{arccot}(u_{\max})} - 1. \quad (26b)$$

It is worth stressing that the bound (26b) is valid only for type I solutions.

Combination of the upper bounds on  $n$  imposed by Propositions 4 and 10 with inequalities (26) leads to the following conclusion:

**Proposition 14.** *The globally time-optimal solution(s) of problem (2) is of type I if*

$$\phi_x = |\arcsin(r_{0,x}) - \arcsin(o_x)| > 4\alpha \quad (27a)$$

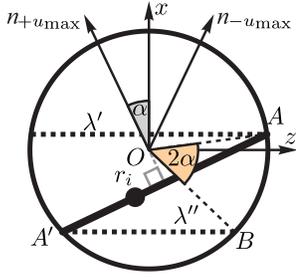


FIG. 6. Geometrical calculation of the value of  $\Delta\theta_{r,x}^{\max}$ . Rotation  $\mathcal{S}_{\tilde{n}_{-u_{\max}}}$  about vector  $\tilde{n}_{-u_{\max}}$  transfers any point  $r_i$  on the Bloch sphere into a new point on the  $AA'$  plane. The  $x$ -coordinate of this new point is bounded by the planes  $\lambda'$  and  $\lambda''$ . Thus, the associated change in  $\theta_{r,x}$  is less than  $\angle AOB=2\alpha$ .

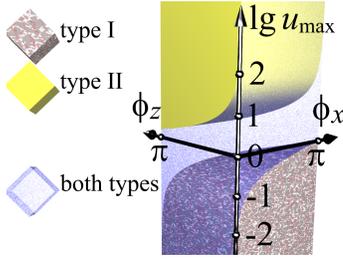


FIG. 7. Distribution of types of globally optimal solutions according to Proposition 14. Note that the admissible values of  $\phi_x$  and  $\phi_z$  are restricted by inequality  $\phi_x + \phi_z \leq \pi$ .

and of type II if

$$\phi_z = |\arcsin(r_{0,z}) - \arcsin(o_z)| > \left[ \frac{\pi}{2\alpha} + 2 \right] (\pi - 2\alpha). \quad (27b)$$

Note that this estimate can be further refined if combined with the upper bounds stated in Proposition 12. The statement of Proposition 14 is illustrated graphically in Fig. 7 which clearly shows that type I and type II solutions dominate in the opposite limits of tight and loose control restriction  $u_{\max} \rightarrow 0$  and  $u_{\max} \rightarrow \infty$ , respectively. Neither type, however, completely suppresses the other one at any finite positive value of  $u_{\max}$ . This coexistence sets the origin for the generic structure of suboptimal solutions (traps), whose analysis will be the subject of next two sections.

#### IV. TRAPS IN TIME-OPTIMAL CONTROL

The globally time-optimal solution (hereafter denoted as  $\tilde{u}^{\text{opt}}$ ) of the problem (2) can be supplemented by a number of trapping suboptimal solutions  $\tilde{u}$  (characterized by  $\tilde{J} < \tilde{J}^{\text{opt}}$  and/or  $\tilde{T} > \tilde{T}^{\text{opt}}$ ) that are, however, optimal with respect to any infinitesimal variation of  $\tilde{u}(\tau)$  and  $T$ . In particular, Proposition (2) implies that each locally optimal solution of type 0II gives rise to the infinite family of traps of the form shown in Fig. 3. In what

follows, we will call such traps “perfect loops”. Proposition 1 indicates that perfect loops may exist at any value of  $u_{\max}$ . Nevertheless, their presence does not stipulate sufficient additional complications in finding the globally optimal solution by gradient search methods. Indeed, these “simple” traps can be identified at no cost by the presence of the continuous bang arc of the duration  $\Delta\tau_i \geq \pi \sec(\alpha)$ . Moreover, one can easily escape any such trap by inverting the sign of the control  $u(\tau)$  at any continuous subsegment of this arc of duration  $\pi \sec(\alpha)$  or by removing the respective time interval from the control policy.

For this reason, the primary objective of this section is to investigate the other, “less simple” types of traps which can be represented by type I and  $^s\text{II}|_{s>0}$  suboptimal extremals. Propositions 8, 10, 12, and 13 show that the number of switchings  $n$  in such extremals is always bounded (at least by  $\pi/\alpha$ ). Thus, the maximal number of such traps is also finite and decreases with increasing  $u_{\max}$ . It will be convenient to loosely classify the traps into the “deadlock”, “loop” and “topological” ones as follows. The first two kinds of traps are represented by type I extremals. The deadlock traps are defined by inequalities  $\tilde{J} < \tilde{J}^{\text{opt}}$   $\tilde{T} < \tilde{T}^{\text{opt}}$ . They usually also satisfy the inequalities  $n < n^{\text{opt}}$ . Their existence is mainly related to the fact that the distance to the destination point  $o$  for most extremals non-monotonically changes with time. The trajectory of the loop trap has the intersection with itself other than the perfect loop. These solutions require longer times  $\tilde{T} > \tilde{T}^{\text{opt}}$  and typically also larger numbers of switchings  $n > n^{\text{opt}}$  in order to reach the kinematic extremum  $\tilde{J} = \tilde{J}^{\text{opt}}$ . Finally, the topological traps are associated with extremals of the type distinct from the type of the globally optimal solution. Of course, real traps can combine the features of all these three kinds.

Examples of the deadlock and loop traps are shown in Fig 8. In this case the globally time optimal solution with  $n^{\text{opt}}=4$  is accompanied by two deadlock traps and two degenerate loop traps corresponding to  $n=5$  (only one is shown; the remaining solution can be obtained via subsequent reflections of the black trajectory relative to the  $yz$  and  $xy$ -planes). At the same time, no traps exist for  $n=1, 3$  and  $n>5$ .

The bang-bang extremal represented by blue curve  $r^- \rightarrow r'' \rightarrow r^+$  in Fig. 2a provides another example of the loop trap that is also the topological trap relative to type II optimal trajectory  $r^- \rightarrow r^+$  (the specific parameters used in this example are:  $u_{\max} = \frac{1}{2}$ ,  $r^- = r_0 \propto \{0, 1, -\frac{1}{2}\}$ ,  $r^+ = o \propto \{0, 1, 1\}$ ). In general, once the endpoints  $r^-$  and  $r^+$  satisfy the conditions of Proposition 1, the time-optimal solution remains the same type II trajectory even in the limit  $u_{\max} \rightarrow 0$ , where the time optimal trajectories are mostly of type I (see Proposition 14 and Fig. 7). Moreover the traps of the shown form will exist for any value of  $u_{\max} < \sqrt{4 - (r_z^- + r_z^+)^2 / |r_z^- - r_z^+|}$ .

Another generic example of the traps of all three types can be straightforwardly constructed in the case  $u_{\max} \gg 1$  (see Fig. 9) by selecting  $o \propto \{1, 0, u_{\max}\}$  and choosing the

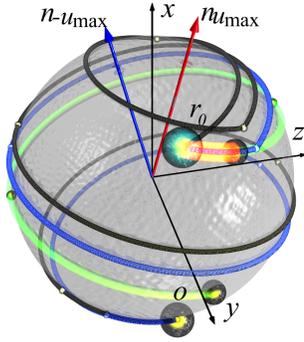


FIG. 8. Globally optimal solution (blue line), deadlock traps (light-red and green lines) and loop trap (black line) for the time-optimal control problem (2),(3),(4) with  $u_{\max}=\frac{1}{4}$ ,  $r(0)=\{\frac{1}{\sqrt{2}}, \frac{1}{\sqrt{2}}, 0\}$ , (big emerald dot) and  $o=\{\frac{1}{\sqrt{2}}, -\frac{1}{\sqrt{2}}, 0\}$  (big black-yellow dot). Small dots indicate the positions of corner points. The parameters of extremals are listed in the table:

extremal	sign( $\tilde{u}_1^-$ )	$n$	$\tilde{\Delta}\tau_1$	$\tilde{\Delta}\tau$	$\tilde{\Delta}\tau_{n+1}$
red	+	0	0.23	-	-
green	-	2	0.88	1.52	0.88
blue	+	4	0.33	1.78	0.33
black	-	5	1.15	1.72	0.57

507 initial state in vicinity of  $z=1$ :  $r_0 \propto \{c_1, c_2, u_{\max}\}$ , where  
 508  $0 < c_1 < 1$  and  $c_2$  is any sufficiently small number. Al-  
 509 though the vast majority of time-optimal solutions are  
 510 of type II in the limit  $u_{\max} \rightarrow \infty$  (see Proposition 14), for  
 511 this special choice the optimal solution is of type I for  
 512 any finite value of  $u_{\max}$  whereas the complementary type  
 513 II extremal represents the topological trap. In the case  
 514  $c_2 < 0$ , there also exist a deadlock trap structurally similar  
 515 to the ones shown in Fig. 8.

516 These observations lead to the following key proposi-  
 517 tion:

518 **Proposition 15.** *For any value of  $u_{\max}$  there exist ini-*  
 519 *tial states  $\rho_0$  and observables  $\hat{O}$ , such that the time opti-*  
 520 *mal control problem (2),(3) has locally time-optimal so-*  
 521 *lutions  $\tilde{u}(\tau)$  representing non-simple traps.*

## 522 V. TRAPS IN FIXED-TIME OPTIMAL 523 CONTROL

524 Consider the problem (2), (3) where the control time  
 525  $T$  is fixed. Specifically, we will be interested in the case

$$T = \text{const} \gg \frac{\pi^2}{\alpha} \quad (28)$$

526 when the kinematically optimal solutions exist for any  
 527 given  $\rho_0$  and  $\hat{O}$ . We again will exclude the class of perfect  
 528 loop traps from the analysis for the same reasons as in  
 529 the previous section. Intuitively one can expect that the  
 530 probability of trapping in the local extrema (other than  
 531 perfect loops) should be small at large  $T$ . However, it is

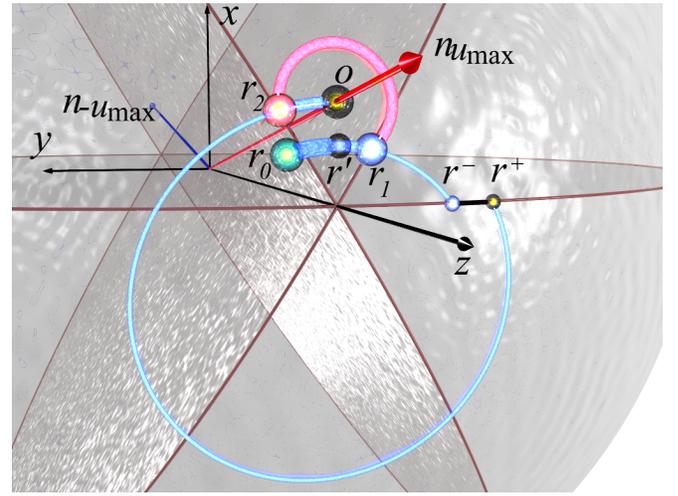


FIG. 9. The optimal solution (medium-thick trajectory  $r_0 \rightarrow r_1 \rightarrow r_2 \rightarrow o$ ), topological trap (thin trajectory  $r_0 \rightarrow r^- \rightarrow r^+ \rightarrow o$ ) and deadlock trap (thick trajectory  $r_0 \rightarrow r'$ ) for the time-optimal control problem (2),(3),(4) with  $u_{\max}=8$ ,  $r(0) \propto \{\frac{1}{2}, \frac{1}{2}, u_{\max}\}$ ,  $o \propto \{1, 0, u_{\max}\}$ . The segments colored blue/black/red correspond to  $u(\tau) = -u_{\max}/0/+u_{\max}$  and are associated with rotations about the axes  $\vec{n}_{-u_{\max}} \setminus \vec{e}_x \setminus \vec{n}_{-u_{\max}}$ . The durations  $\Delta\tau_i$  of the consequent bang arcs are summarized in the table:

extremal	type	$n$	$\tilde{\Delta}\tau_1$	$\tilde{\Delta}\tau_2$	$\tilde{\Delta}\tau_3$
deadlock trap	I	0	0.020	-	-
optimal solution	I	2	0.0327	0.262	0.017
topological trap	II	2	0.075	0.031	0.324

532 not clear if there exists such value of  $T$  that the functional  
 533 (2) will become completely free of such traps.

534 To answer this question, note that in line with the anal-  
 535 ysis given in Sec. II any trap should be represented by  
 536 either type I or type II extremal. However, the maximal  
 537 number of switchings is not limited by inequalities simi-  
 538 lar to Proposition 8. At the same time, Proposition 6  
 539 remains applicable (see Remark 1 in Appendix F). Recall  
 540 that its proof is based on introduction of the “sliding”  
 541 variations  $\delta\gamma_i$  which shift the angular positions of the  
 542 “images” of corner points on the diagram of Fig. 5 (see  
 543 Appendix F). The explicit expression for the “sliding”  
 544 variation around the  $i$ -th corner point up to the third  
 545 order in the associated control time change  $\delta\tau_i$  is given  
 546 by eq. (F4). By definition, if the trajectory  $\tilde{u}(\tau)$  is type I  
 547 trap, then no admissible control variation  $\delta u$  can improve  
 548 the performance index (2). Consider the subset  $\Omega$  of such  
 549 variations composed of infinitesimal sliding variations  $\delta\gamma_i$   
 550 that preserve the total control time  $T$ . Then, the neces-  
 551 sary condition of trap  $\tilde{u}(\tau)$  is absence of the non-uniform  
 552 sliding variation  $\delta u(\tau) \in \Omega$  that leaves the trajectory end-  
 553 point  $r_{n+1}$  intact. Indeed, the trajectory associated with  
 554 varied control  $\tilde{u} + \delta u$  would deliver the same value of the  
 555 performance index but at the same time is not the lo-  
 556 cally optimal solution (since it is no longer the type I  
 557 extremal) which implies that  $\tilde{u}$  is not locally optimal.

558 Using (F4) the stated necessary condition can be

rewritten as the requirement of definite signature of the quadratic form (F6), where the parameters  $q_i$  were introduced in Proposition (7). The necessary condition of the sign definiteness is that all (probably except one) parameters  $q_i$  are either non-positive or non-negative. Using Fig. 5 one can see that in the case of long  $T$  only the second option can be realized with  $\eta \simeq 0$ ,  $\eta \simeq -\frac{\pi}{2}$  and  $\eta \simeq -\frac{\pi}{3}$  (the case  $\eta \simeq -\pi$  must be eliminated because it implies  $u_{\max}=0$ ). One can show that the last two variants lead to saddle points rather than to the local extrema. The remaining case  $\eta \simeq 0$  leaves the two options  $\theta \simeq 0$  and  $\theta \simeq 2\pi$ . The last option corresponds to positive constant  $c_{i,1}$  in (15), which indicates the possibility of increasing  $J$  via monotonic “stretching” the time:  $T \rightarrow T + \delta T(T)$ ,  $u(\tau) \rightarrow u(\tau - \delta T(\tau))$ , where  $\delta T(\tau)$  is an infinitesimal positive monotonically increasing function. At the same time, the associated parameters  $q_i$  are all negative, so there exists the combination of variations  $\delta\tau$  of arcs durations  $\Delta\tau$  which will result in achieving the same value of the performance index at shorter time. Thus, we can conclude that it is also possible to increase  $J$  at fixed time  $T$  via proper combination of these two variations, so the variant  $\theta \simeq 2\pi$  should be dismissed as a saddle point. Only the remaining choice  $\theta \simeq 0$  is consistent with an arbitrary number of  $q_i$  of the same sign. However, in this case the length of each bang arc also reduces to zero. As result, the maximal duration of such optimal trajectories is limited by the inequality  $T \lesssim \pi$ .

This analysis leads us to remarkable conclusion:

**Proposition 16.** *The fixed-time optimal control problem (2) is free of non-simple traps for sufficiently long control times  $T$ .*

The spirit of this conclusion is in line with the results of numerical simulations performed in [19]. With this, it is worth recalling that the general time-fixed problem may have a variety of perfect loop traps for any value of  $u_{\max}$  and, thus, is not trap-free in the strict sense. These traps were missed in the simulations in [19] due to the specifics of numerical optimization procedure.

## VI. SUMMARY AND CONCLUSION

All stationary points of the time optimal control problem and all saddles and local extrema of the fixed-time optimal control problem are represented by the piecewise-constant controls of types I and II sketched in Fig. 1 (the associated characteristic trajectories  $\rho(\tau)$  on the Bloch sphere are shown in Figs. 4 and 3, correspondingly). We systematically explored the anatomy of stationary points of each type. Specifically, we identified the locations and relative arrangements of corner points on the Bloch sphere (propositions 2, 3, 6, 7, 10, 11) and estimated their total number (propositions 8, 9, 10, 12, 13). These characteristics, together with propositions 1, 4, 5 and 14, allow to determine whether the given extremal is a saddle point or a locally optimal solution, and also to

predict the shape of globally optimal solution. The presented results (except Proposition 8) substantially generalize and refine the estimates obtained in previous studies [25, 26]. Moreover, this study, to our knowledge, is the first example of a systematic analytic exploration of the overall topology of the quantum landscape  $J[u]$  in the presence of constraints on the control  $u$  and for the arbitrary initial quantum state  $\rho_0$  and observable  $\hat{O}$ . In particular, we distinguished 4 categories of traps tentatively called deadlock, topological, loop and perfect loop traps. The landscape can contain an infinite number of perfect loops whereas the number of traps of other types is always finite. Among them, the number of deadlock traps and loops decreases with increasing value of the constraint  $u_{\max}$  in eq. (4). Nevertheless, we have shown by an explicit example that the traps of all categories can simultaneously complicate the landscape  $J[u]$  of the time-optimal control problem regardless of the value of  $u_{\max}$ . So, this is the case where the intuitive attempt to “extrapolate” the conclusions based on analysis of the case of unconstrained controls totally fails.

The fixed-time control problem is more intriguing. On one hand we formally showed that it is impossible to completely eliminate all the traps in this case by increasing the value of  $u_{\max}$ . This result is in line with generic experience concerning the optimal control in technical applications. However, if the control time is long enough (specifically, if  $T \gg \pi^2 / \arctan u_{\max}$ ) the only traps which can survive are perfect loops. Remarkably, these traps can be easily avoided at virtually no computational cost.

Combined together, our results constitute a thorough guide for optimal control synthesis to manipulate the individual qubit in a variety of experiments with cold atoms, Bose-Einstein condensates, superconducting qubits etc. However, they also deliver more general message since the stable control over single-qubit operations is the necessary controllability prerequisite for a variety of quantum control problems including the universal quantum information processing. We can conclude that traps constitute a general obstacle for practical optimization, and their presence can not be ignored. Nevertheless, we have demonstrated that there can exist simple “patches” to standard gradient search algorithms such that the quantum landscape will appear as trap-free from practical perspective. The latter conclusion is consistent with the common viewpoint in the quantum optimal control literature. That said, validity of the same conclusion in the general case remains an open question.

The key methodological feature of the presented derivations is introduction of the sliding variations, which makes it possible to extensively rely on highly visual and intuitive geometrical arguments. For this reason, we believe that the mathematical aspect of the paper constitutes instructive introduction into high-order analysis of optimal processes.

668 **Appendix A: Review of the Pontryagin maximum**  
669 **principle**

670 In this appendix we briefly overview the concepts of the  
671 Pontryagin theory and outline the derivations of the key  
672 statements and relations of Sec. II. Consider the following  
673 canonical optimal control problem [10, 11]:

$$\frac{\partial}{\partial t} x_i = f_i(\mathbf{x}, \mathbf{u}, t) \quad (i=1, \dots, n); \quad (\text{A1a})$$

$$g_j(\mathbf{x}(t_0), \mathbf{x}(T), t_0, T) = 0 \quad (j=1, \dots, q < 2n+2); \quad (\text{A1b})$$

$$\mathbf{u} \in \mathcal{U}; \quad (\text{A1c})$$

$$J \rightarrow \max. \quad (\text{A1d})$$

674 Here  $\mathbf{x} = \{x_1, \dots, x_n\}$  and  $\mathbf{u} = \{u_1, \dots, u_m\}$  are the vectors  
675 of phase variables and the available controls, correspond-  
676 ingly. The functions  $g_j$  introduce the boundary con-  
677 straints on the admissible values of  $\mathbf{x}$  whereas eq. (A1c)  
678 describes the control constraints, which are the general-  
679 ization of eq. (3). The most general (Bolza) form of the  
680 performance index  $J$  in (A1d) is

$$J = g_0(\mathbf{x}(t_0), \mathbf{x}(T), t_0, T) + \int_{t_0}^T f_0(\mathbf{x}, \mathbf{u}, t) dt. \quad (\text{A1e})$$

681 The task is to find the control policy  $\tilde{u}(t)$  and, maybe,  
682 the final time  $T$  together with the initial and terminal  
683 phase variables  $\mathbf{x}(t_0)$  and  $\mathbf{x}(T)$  which maximize  $J$ .

684 Let us introduce the following auxiliary functions:

$$K = \sum_{i=0}^N \Psi_i f_i \quad \text{— Pontryagin function}; \quad (\text{A2})$$

$$G = \sum_{j=0}^q \nu_j g_j \quad \text{— determinant}, \quad (\text{A3})$$

685 where  $\nu_0, \Psi_0 = \text{const} \geq 0$  and the  $\Psi(t)$  stands for the set  
686 of so-called *costate* (or *adjoint*) variables. By definition,

$$\frac{\partial}{\partial t} x_i = \frac{\partial K}{\partial \Psi_i} \quad (\text{cf. (A1a)}); \quad (\text{A4a})$$

$$\frac{\partial}{\partial t} \Psi_i = - \frac{\partial K}{\partial x_i}. \quad (\text{A4b})$$

687 Mathematically, the functions  $\Psi_i(t)$  and variables  $\nu_j$  are  
688 the Lagrange multipliers in the extremal problem (A1d)  
689 that account for the dynamic and boundary constraints  
690 (A1a) and (A1b), respectively. The process (trajec-  
691 tory)  $\{\Psi(t), \mathbf{u}(t), \mathbf{x}(t)\}$  is called *admissible* if it matches  
692 eqs. (A4) and the boundary conditions (A1b).

693 The *Pontryagin maximum principle* (PMP) states that  
694 if  $\{\tilde{\mathbf{x}}(t), \tilde{\Psi}(t), \tilde{\mathbf{u}}(t)\}$  is an (locally) optimal solution of  
695 problem (A1) then  $\tilde{\Psi}_0 \geq 0, \tilde{\Psi}(t) \neq 0$  and

$$\tilde{\mathbf{u}}(t) = \arg \max_{\mathbf{u}(t) \in \mathcal{U}} K(\tilde{\mathbf{x}}(t), \tilde{\Psi}(t), \mathbf{u}(t), t). \quad (\text{A5})$$

696 Besides that, the following *transversality conditions* hold:

$$\tilde{\Psi}_i(t_0) = - \frac{\partial G}{\partial x_i(t_0)}; \quad \tilde{\Psi}_i(T) = \frac{\partial G}{\partial x_i(T)}; \quad (\text{A6})$$

$$\tilde{K} \Big|_{t=t_0} = \frac{\partial G}{\partial t_0}; \quad \tilde{K} \Big|_{t=T} = - \frac{\partial G}{\partial T}. \quad (\text{A7})$$

697 Processes satisfying (A5)-(A7) are called *extremals*.  
698 Any solution of the problem (A1) is extremal. The re-  
699 verse is not true since PMP provides only the first-order  
700 necessary optimality condition. To identify the solutions,  
701 the Legendre-Clebsch condition and its generalizations  
702 [32], or other higher-order extensions of PMP should be  
703 used [31].

704 In the general case, the optimal controls  $\tilde{u}_k(t)$  are the  
705 piecewise-smooth curves composed of *regular* and *singular*  
706 (or *degenerate*) subarcs and having any number of  
707 discontinuities of the first kind (*corner points*). The val-  
708 ues of  $\tilde{u}_k(t)$  on regular subarcs can be directly obtained  
709 from (A5) whereas the singular subarcs where  $\frac{\partial \tilde{K}}{\partial u_k} = 0$  re-  
710 quire an extra investigation. The following *Weierstrass-*  
711 *Erdmann conditions* must hold at each corner point:

$$\Psi|_{t=0} = \Psi|_{t+0}; \quad K|_{t=0} = K|_{t+0}. \quad (\text{A8})$$

712 Let us now outline the application of PMP to the quan-  
713 tum optimal control problem (1)-(4). In this case, the  
714 state vector  $\mathbf{x}(t)$  is composed of matrix elements of the  
715 density matrix  $\rho(t)$  and the control  $\mathbf{u}(t)$  reduces to a  
716 scalar function  $u(t)$ . The performance index (2) is a  
717 special case of (A1d), where  $f_0 = 0$  (a so-called Mayer  
718 problem). Using the definition (A2), one straightfor-  
719 wardly obtains the expression (6) for a Pontryagin func-  
720 tion, where the matrix elements of  $\hat{O}(t)$  serve as the com-  
721 ponents of a costate vector  $\Psi(t)$ . Application of (A4b)  
722 to (6) gives the evolution law (7). The endpoint relation  
723 (8) stems from the second of the transversality conditions  
724 (A6) with  $G = g_0(\rho(T)) = \text{Tr}[\rho(T)\hat{O}]$ , whereas the second  
725 pair of transversality conditions (A7) leads to the prop-  
726 erty (11). Finally, note that the Pontryagin function (6)  
727 does not explicitly depend on time  $t$ . Hence, eqs. (A4)  
728 imply the relation (10) since  $\frac{d}{dt} \tilde{K} = \frac{\partial \tilde{K}}{\partial \rho} \frac{d\rho}{dt} + \frac{\partial \tilde{K}}{\partial \hat{O}} \frac{d\hat{O}}{dt} = 0$ .

729 **Appendix B: Proof of Proposition 1**

730 Here we consider the case  $r_y^- > 0, r_y^+ > 0$ . The case  
731  $r_y^- < 0, r_y^+ < 0$  can be treated similarly. Simple geomet-  
732 rical analysis leads to the following expression for the  
733 travel time difference  $\delta T$  between bang-bang (orange)

734 and “equatorial” (black) trajectories shown in Fig. 2a:

$$\begin{aligned} \delta T_a = & \cos(\alpha) \left( \arcsin \left( \frac{\frac{\delta_z}{2} \sec(\alpha) - \cos(\alpha) r_z^+}{\sqrt{1 - \sin^2(\alpha) r_z^{\pm 2}}} \right) + \right. \\ & \arcsin \left( \frac{\cos(\alpha) r_z^+}{\sqrt{1 - \sin^2(\alpha) r_z^{\pm 2}}} \right) - \arcsin \left( \frac{\cos(\alpha) r_z^-}{\sqrt{1 - \sin^2(\alpha) r_z^{\pm 2}}} \right) + \\ & \left. \arcsin \left( \frac{\frac{\delta_z}{2} \sec(\alpha) + \cos(\alpha) r_z^-}{\sqrt{1 - \sin^2(\alpha) r_z^{\pm 2}}} \right) \right) - \arcsin(r_z^+) + \arcsin(r_z^-), \end{aligned} \quad (B1)$$

735 where  $\delta_z = r_z^+ - r_z^-$ . Let us fix one of the endpoints  $r^\pm$  and  
736 vary the position of another one. Note that  $\delta T_a|_{\delta_z=0} = 0$   
737 for any admissible value of  $r_z^\pm$ . Furthermore,

$$\pm \frac{d\delta T_a}{dr_z^\pm} = \frac{(1 - r_z^{\pm 2}) \left( \sqrt{1 - \frac{r_z^\pm \delta_z}{1 - r_z^{\pm 2}}} - \sqrt{1 - \frac{r_z^\pm \delta_z + \frac{\delta_z^2}{4} \sec^2 \alpha}{1 - r_z^{\pm 2}}} \right)}{\left( \csc^2 \alpha - r_z^{\pm 2} \right) \sqrt{1 - r_z^\pm \delta_z - r_z^{\pm 2} - \frac{\delta_z^2}{4} \sec^2 \alpha}} > 0. \quad (B2)$$

738 This allows to conclude that  $\delta T_a > 0$  for any  $\delta_z > 0$  which  
739 finishes the proof of Proposition for the case  $r_y^- r_y^+ > 0$ .

740 Consider now the case  $r_y^- r_y^+ < 0$ . For clarity, we will  
741 assume that  $r_y^- > 0$ ,  $r_z^- < r_z^+$  (see Fig. 2b). The remain-  
742 ing cases can be analyzed similarly. The time difference  
743  $\delta T_b$  between “equatorial” (black) and the green trajecto-  
744 ries and its derivative with respect to the position of the  
745 endpoint  $r_z^+$  read as

$$\delta T_b = \arccos(r_z^+) - \cos(\alpha) \arccos \left( \frac{r_z^+ \cos(\alpha)}{\sqrt{1 - r_z^{\pm 2} \sin^2(\alpha)}} \right); \quad (B3)$$

$$\frac{\partial}{\partial r_z^+} \delta T_b = - \frac{2\sqrt{1 - r_z^{\pm 2} \sin^2(\alpha)}}{r_z^{\pm 2} \cos(2\alpha) - r_z^{\pm 2} + 2}. \quad (B4)$$

746 These expressions show that  $\delta T_b|_{r_z^\pm=1} = 0$  and that  
747  $\frac{\partial}{\partial r_z^\pm} \delta T_b > 0$  for any admissible value of  $r_z^\pm$ . Thus,  $\delta T_b > 0$   
748 which proves Proposition for the case  $r_y^- r_y^+ < 0$ .

### 749 Appendix C: Proof of Proposition 3

750 The proof is based on explicit construction of the  
751 second-order McShane’s (needle) variation of the control  
752  $\tilde{u}(\tau)$  which decreases  $\tilde{T}$  if the inequality (22) is violated.  
753 Choose arbitrary infinitesimal parameter  $\delta\tau^- \rightarrow 0$  and de-  
754 note  $r_i^- = \tilde{r}(\tilde{\tau}_i - \delta\tau^-)$ . Under assumptions of Proposition  
755 it is always possible (except for the trivial case  $\tilde{r}_{i,y} = 0$ ) to  
756 choose another small parameter  $\delta\tau^+$  such that the state

757 vector  $r_i^+ = \tilde{r}(\tilde{\tau}_i + \delta\tau^+)$  obeys the equality:  $r_{i,x}^- = r_{i,x}^+$ . It is  
758 evident that the Bloch vector  $r_{i,x}^-$  can also reach  $r_{i,x}^+$  in  
759 the course of free evolution with  $u=0$  after certain time  
760  $\delta\tau^0$ . If we require that  $\delta\tau_i^+, \delta\tau_i^0|_{\delta\tau_i^- \rightarrow 0} = 0$  then both  $\tau_i^+$   
761 and  $\tau_i^0$  are uniquely defined by  $\delta\tau_i^-$ ,

$$\begin{aligned} \delta\tau_i^+ &= \frac{\delta\tau_i^-(\tilde{r}_{i,y} + 2\delta\tau_i^- \tilde{r}_{i,z})}{\tilde{r}_{i,y}} + o(\delta\tau_i^{-2}); \\ \delta\tau_i^0 &= \frac{2\delta\tau_i^-(\delta\tau_i^-(\tilde{u}_i^- \tilde{r}_{i,x} + \tilde{r}_{i,z}) + \tilde{r}_{i,y})}{\tilde{r}_{i,y}}, \end{aligned} \quad (C1)$$

762 and thus,  $\delta\tau_i^0 - \delta\tau^+ - \delta\tau^- = 2\tilde{u}_i^- (\delta\tau_i^-)^2 \tilde{r}_{i,x} / \tilde{r}_{i,y}$ . The lat-  
763 ter quantity should be nonnegative for the locally time-  
764 optimal solution which leads to eq. (22).

### 765 Appendix D: Proof of Proposition 4

766 Consider any type  $^s\Pi$  extremal with  $s > 0$  containing  
767 at least one interior bang segment  $\tau \in [\tilde{\tau}_i, \tilde{\tau}_{i+1}]$  of length  
768  $\tilde{\Delta}\tau_i = m\pi \cos(\alpha)$  ( $m \in \mathbb{N}, 0 < \tilde{\tau}_i, \tilde{\tau}_{i+1} < T$ ). Since  $\tilde{r}_i = \tilde{r}_{i+1}$   
769 both the value of the performance index  $J$  and dura-  
770 tion  $T$  will not change if this segment will be “trans-  
771 lated” in arbitrary new point  $\tilde{r}(\tau'_i(\kappa))$  of extremal  
772 via the following continuous variation  $\tilde{u}(\tau) \rightarrow u(\kappa, \tau)$   
773 ( $-\tau_i < \kappa < T - m\pi \cos \alpha$ ):

$$u(\kappa, \tau) = \begin{cases} \tilde{u}(\tau), & \tau < \tilde{\tau}_i + \frac{\kappa - |\kappa|}{2} \vee \tau > \tilde{\tau}_{i+1} + \frac{\kappa + |\kappa|}{2}; \\ \tilde{u}_i^+, & \tilde{\tau}_i + \kappa < \tau < \tilde{\tau}_{i+1} + \kappa; \\ u(\tau - \tilde{\Delta}\tau_i) & \text{otherwise,} \end{cases} \quad (D1)$$

774 where  $\tau'_i(\kappa) = \tilde{\tau}_i + \kappa + \frac{1}{2}(1 + \frac{\kappa}{|\kappa|})\tilde{\Delta}\tau_i$ .

775 Suppose that  $\tilde{u}(\tau)$  is locally time-optimal solu-  
776 tion. Then the entire family of control policies  
777  $\{u(\kappa, \tau), r(\kappa, \tau)\}$  should be locally time-optimal too.  
778 Since  $s > 0$  it is always possible to select the value  $\kappa = \kappa_0$   
779 such that  $\tilde{r}(\tau'_i(\kappa_0))$  is interior point of the bang arc with  
780  $\tilde{u}(\tau'_i(\kappa_0)) = -\tilde{u}_i^+$  and  $\tilde{r}_x(\tau'_i(\kappa_0)) \neq 0$ . However, the result-  
781 ing trajectory  $r(\kappa_0, \tau)$  is both  $\Lambda$ - and  $V$ -shaped in the  
782 neighborhood of point  $r(\tilde{\tau}_i + \kappa_0) = r(\tilde{\tau}_{i+1} + \kappa_0)$ . Accord-  
783 ing to Proposition (3) such trajectory can not be time-  
784 optimal. The obtained contradiction finishes the proof.

### 785 Appendix E: Proof of Proposition 5

786 Let  $u'(\tau)$  be the control strategy obtained via arbitrary  
787 McShane variation  $\delta u(\tau)$  of the control  $\tilde{u}(\tau)$ . Let us show  
788 that  $u'(\tau)$  is less time efficient than some member  $u''(\tau)$   
789 of the control family  $\mathcal{F}^{[k]}(u''^{\text{anz}}(\tau))$  with the same  $k$  but  
790 perhaps the different ansatz  $\tilde{u}''^{\text{anz}}$ . For this we will need  
791 the following lemma which is complementary to Propo-  
792 sitions 1 and 3:

794 **Lemma 1.** *Suppose that  $r'(\tau')$  is junction point of two*  
795 *bang arcs of the trajectory  $u(\tau)$  such that  $r'_x = 0$ . Consider*

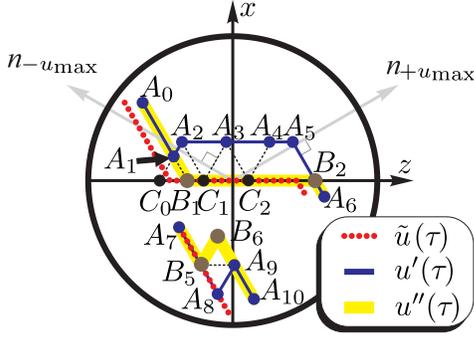


FIG. 10. Projections of the characteristic pieces of the original, varied and reduced trajectories  $\tilde{r}(\tau)$ ,  $r'(\tau)$  and  $r''(\tau)$  on the  $xz$  plane (it is assumed that  $y$ -components of all shown parts of trajectories are greater than zero). The color associations are indicated in the inset.

any two points  $r^-(\tau^-)$  and  $r^+(\tau^+)$  ( $\tau^- < \tau' < \tau^+$ ) on adjacent arcs such that  $r_x^- = r_x^+$  and the complete segment  $r'_y r_y(\tau) > 0$  for any  $\tau \in (\tau^-, \tau^+)$ . Denote as  $\widehat{\Delta\tau}$  the minimal duration of free evolution ( $u=0$ ) required to reach  $r^+$  starting from  $r^-$ . Then,  $\widehat{\Delta\tau} > \tau^+ - \tau^-$ .

Since  $\tilde{u}_{\text{anz}}(\tau)$  is locally optimal by assumption it is sufficient to consider the variations of the  $\delta u(\tau)$  which do not involve the vicinities of the trajectory endpoints. Moreover, it is sufficient to analyze the variations  $\delta u(\tau)$  which are nonzero only in vicinities points where  $\tilde{r}(\tau)=0$ . To show this consider the McShane variation in the arbitrary interior point  $A_8$  of the bang arc (see Fig. 10). Consider the piece  $A_7 A_8 A_9 A_{10}$  of the varied trajectory  $r'(\tau)$ . According to Proposition 3 (see eq. (C)) the path  $B_5 B_6 A_9$  is more time-efficient than  $B_5 A_8 A_9$  if the varied segment  $A_8 A_9$  is sufficiently small. Thus, the trajectory  $A_7 B_5 B_6 A_{10}$  is more time-efficient than original segment  $A_7 A_8 A_9 A_{10}$ . By repeated application of the same reasoning to the modified pieces of trajectory one can replace the control  $u'(\tau)$  with the more effective strategy which differs from  $\tilde{u}(\tau)$  only in vicinities of the points  $r'$  with  $r'_x \rightarrow 0$ . Since it is sufficient to consider only this modified control policy we will rename it as  $u'(\tau)$  and will refer as the initial variation in the subsequent analysis.

The characteristic piece  $A_0 A_2 A_5 A_6$  of the resultant trajectory is shown in Fig. 10. Following the proof of Proposition 1 (see eq. (B2)) the path  $C_0 A_2 C_1$  is less time-efficient than  $C_0 A_1 B_1 C_1$ . This implies that the path  $A_1 B_1 C_1$  is more time-efficient than  $A_1 A_2 C_1$ . According to Lemma 1, the path  $A_2 C_1 A_3$  is more time-efficient than the path  $A_2 A_3$  associated with the free evolution. As a result, the trajectory segment  $A_1 A_2 A_3$  of the  $r'(\tau)$  is less time efficient than the combination of the segment  $A_1 B_1 C_1$  of the trajectory  $r''(\tau)$  with the segment  $C_1 A_3$ . By continuing the similar analysis one finally comes to conclusion that the part of trajectory  $r'(\tau)$  between the points  $A_0$  and  $A_5$  is less time efficient than the corresponding segment of  $u''(\tau)$ . Applying the same reasoning to the entire trajectory  $r'(\tau)$  we will reduce the original

variation to the  ${}^0II$  type control  $u''(\tau)$  and trajectory  $r''(\tau)$ . Note that we must assume that all the singular segments where  $u''(\tau)=0$  are located on the same side with respect to  $xz$  plane (otherwise the control time can be further reduced by eliminating some singular segments following the proof of Proposition 2, see eq. (C)). This mean, that all the interior bang sections of the control  $u''(\tau)$  are of length  $m\pi/\cos(\alpha)$  ( $m \in \mathbb{N}$ ). Thus, the trajectory  $u''(\tau)=0$  must belong to the family  $\mathcal{F}^{[k]}(u''^{\text{anz}}(\tau))$  with the same index  $k$  as  $\mathcal{F}^{[k]}(u''^{\text{anz}}(\tau))$  and the anzatz  $u''^{\text{anz}}(\tau)$  related to  $\tilde{u}^{\text{anz}}(\tau)$  via infinitesimal variation. Since  $\tilde{u}^{\text{anz}}(\tau)$  is time-optimal the performances and control times associated with policies  $u''^{\text{anz}}$  and  $\tilde{u}^{\text{anz}}$  are related as  $\tilde{J}^{\text{anz}} \geq J''^{\text{anz}}$  and  $\tilde{T}^{\text{anz}} \leq T''^{\text{anz}}$ . Consequently,  $\tilde{J} \geq J''$  and  $\tilde{T} \leq T''$ , so that the control policies  $u''(\tau)$  and  $u'(\tau)$  can not be more effective than  $\tilde{u}(\tau)$ . The latter conclusion completes the proof of Proposition 5.

*Proof of the Lemma 1.* For concreteness, consider the case  $r'_y > 0$ ,  $r_x^- > 0$ . Denote  $\widehat{\delta\tau} = r^+(\tau^+) - r^+(\tau^-) - \widehat{\Delta\tau}$ . Using simple geometrical considerations one can find that

$$\widehat{\delta\tau}(r_x^-, r'_z) = \frac{1}{2} \sum_{s=\pm 1} \left( \arcsin \left( \frac{sr'_z - r_x^- \cot(\alpha)}{\sqrt{1-r_x^{-2}}} \right) + \frac{\arcsin \left( \frac{r_x^- \csc(\alpha) - sr'_z \cos(\alpha)}{\sqrt{1-r_z'^2 \sin^2(\alpha)}} \right)}{\sqrt{\tan^2(\alpha)+1}} \right). \quad (\text{E1})$$

By differentiating (E1) we find that  $\frac{\partial}{\partial r_x^-} \widehat{\delta\tau}(r_x^-, r'_z=0) = -\frac{x^2 \sin(2\alpha) \sqrt{1-x^2 \csc^2(\alpha)}}{(x^2-1)(\cos(2\alpha)+2x^2-1)} < 0$  for any admissible  $r_x^- > 0$ . Similarly, one can show that  $\widehat{\delta\tau}(r_x^-=0, r'_z) = 0$  and  $r'_z \frac{\partial}{\partial r'_z} \widehat{\delta\tau}(r_x^-, r'_z) < 0$  for any admissible  $r'_z \neq 0$ . Taken together, these relations lead to conclusion that  $\widehat{\delta\tau}(r_x^-, r'_z) < 0$  for any admissible  $r_x^- > 0$  which completes the proof for the case  $r'_y > 0$ ,  $r_x^- > 0$ . Other cases can be analyzed in the same way.  $\square$

## Appendix F: Proof of Proposition 6 and 7

One can directly check that the transformation  $\mathcal{S}_{\pm} = \exp(\widehat{\Delta\tau} \mathcal{L}(\pm u_{\text{max}}))$  is equivalent to the composition of rotation  $\mathcal{S}_{\vec{e}_z}(\mp \xi)$  around axis  $\vec{e}_z$  by angle  $\mp \xi$  with rotation  $\mathcal{S}_{\vec{n}_{\pm u_{\text{max}}}}(\eta)$  around the normal vector  $\vec{n}_{\pm u_{\text{max}}}$  to the plane  $\lambda_{\pm u_{\text{max}}}$  by  $\eta$ ,

$$\mathcal{S}_{\pm} = \mathcal{S}_{\vec{n}_{\pm 1}}(\eta) \mathcal{S}_{\vec{e}_z}(\mp \xi) \quad (-\pi < \eta < 0; \quad 0 < \xi < \pi), \quad (\text{F1})$$

where the domain restrictions on the values of  $\eta$  and  $\xi$  result from (19). Thus, the state transformation induced by any two subsequent bang arcs is equivalent to rotation around  $\vec{n}_{\pm u_{\text{max}}}$  by angle  $2\eta$ . This proofs that the all odd (even) corner points are located in the same plane orthogonal to  $\vec{n}_{u_1^-}$  ( $\vec{n}_{u_1^+}$ ) and parallel to  $\vec{e}_z$ . More specifically, they are located on the circles  $r\vec{n}_{\pm u_{\text{max}}} = c_0$  which are mirror images of each other in  $xz$  plane.

In order to complete proof of Proposition 6 it remains to show that  $\vec{e}_z \in \lambda_{\pm u_{\max}}$  (i.e. that  $c_0=0$ ). Since it is already shown that  $\vec{e}_z \parallel \lambda_{\pm u_{\max}}$  it is enough to prove that there exist an least one common point with axis  $\vec{e}_z$ . Consider the infinitesimal variations  $\delta\tau_i^-$  and  $\delta\tau_i^+$  of the durations  $\tilde{\Delta}\tau_i$  and  $\tilde{\Delta}\tau_{i+1}$  of the bang arcs adjacent to arbitrary corner point  $\tilde{r}_i = \tilde{r}(\tilde{\tau}_i)$ , such that the transformation  $\mathcal{S} = \exp(\delta\tau_i^- \mathcal{L}(\tilde{u}_i^-)) \exp(\delta\tau_i^+ \mathcal{L}(\tilde{u}_i^+))$  moves the point  $\tilde{r}_i$  into  $r'_i \in \lambda_{\tilde{u}_i^-}$ . In other words, we require that  $\tilde{r}_i$  and  $r'_i$  should relate by infinitesimal rotation  $\mathcal{S}_{\vec{n}_{\tilde{u}_i^-}}(\delta\gamma_i)$ . For convenience, we will call such variations as "sliding" ones. The form of decomposition (F1) indicates that the sliding variation at  $r_i$  shifts the locations of all subsequent corner points  $\tilde{r}_{j>i} \rightarrow r'_j$  by similar rotations  $\mathcal{S}_{\vec{n}_{\tilde{u}_j^-}}(\delta\gamma_i)$  around the associated axes  $\vec{n}_{\tilde{u}_j^-}$ . Consider the arbitrary composition of the sliding variations, such that the trajectory start and end points remain fixed, i.e.  $\sum_i \delta\gamma_i = 0$ . If the extremal  $\tilde{u}$  is locally optimal then such variations should not allow the reduction of the control time  $T$ :  $\sum_i \delta\tau_i \leq 0$ , where  $\delta\tau_i = \delta\tau_i^- + \delta\tau_i^+$ . This requirement leads to the following first-order (in  $\delta\tau_i$ ) necessary optimality condition:

$$\forall i, j : \frac{d\delta\gamma_i}{d\delta\tau_i} = \frac{d\delta\gamma_j}{d\delta\tau_j}. \quad (\text{F2})$$

Using simple geometrical analysis it is possible to explicitly calculate the derivatives in (F2),

$$\frac{d\delta\gamma_i}{d\delta\tau_i} = \frac{2\sqrt{\cos^2\left(\frac{\theta}{2}\right) + u_{\max}^2}}{\frac{\tilde{r}_{i,x}}{\tilde{r}_{i,y}} \tilde{u}_i^- \sin\left(\frac{\theta}{2}\right) - \sqrt{1 + u_{\max}^2} \cos\left(\frac{\theta}{2}\right)}. \quad (\text{F3})$$

We can conclude that equalities (F2) are equivalent to condition:  $\frac{\tilde{r}_{i,x}}{\tilde{r}_{i,y}} \tilde{u}_i^- = \text{const}$  which directly leads to conclusion that  $\vec{e}_z \in \lambda_{\pm 1}$  and completes the proof of Proposition 6.

*Remark 1.* It is worth stressing that the above proof of Proposition 6 does not explicitly depend on the time optimality of the trajectory  $\tilde{u}(\tau)$ . Thus, its statement is generally valid for any type I extremal locally optimal with respect to small variations of control  $\tilde{u}(\tau)$ , including the case of fixed control time  $T$ .

The proof of Proposition 7 follows from the analysis of the higher-order terms in sliding variation along the extremal trajectory. Calculations result in the following expression:

$$\delta\gamma_i = 2 \cos\left(\frac{\xi}{2}\right) \delta\tau_i - \left| \frac{\sin^3\left(\frac{\xi}{2}\right)}{u_{\max}} \right| q_i \delta\tau_i^2 + q_i^{(3)} \delta\tau_i^3 + o(\delta\tau_i^3), \quad (\text{F4})$$

where

$$q_i^{(3)} = \frac{1}{3} u_{\max}^2 \cos\left(\frac{\xi}{2}\right) \left[ 2 \sec^2\left(\frac{\eta}{2}\right) - 3q_i^2 \tan^4\left(\frac{\eta}{2}\right) - 6 \cot(\gamma_i) \left( \tan\left(\frac{\eta}{2}\right) + (q_i+1) \tan^3\left(\frac{\eta}{2}\right) \right) \right]. \quad (\text{F5})$$

The necessary condition of the local optimality is thus the inequality  $\sum_{i=1}^n q_i \delta\tau_i^2 \geq 0$  in which the variations  $\delta\tau_i$  are subject to constraint  $\sum_{i=1}^n \delta\tau_i = 0$ . The power of sliding variation is in the fact that the quadratic form in the left-hand side of this inequality is diagonal (i.e. the contributions of the sliding variations  $\delta\gamma_i$  are independent up to the second order in  $\delta\tau_i$ ). Thus, optimality implies non-negativity of the following simple quadratic form:

$$Q_{kj} = \delta_{kj} q_k + q_n \quad (k, j = 1, \dots, n-1), \quad (\text{F6})$$

which can be easily rewritten in the form of statement of Proposition 7.

## Appendix G: Proof of Proposition 9

Let  $q' = q_{i'} < 0$  be the smallest term in the set  $\{q_i\}$ . By applying Proposition 7 to the corner points adjacent to  $i'$ -th we have:  $q_{i'\pm 1} + q_{i'} < 0$ . These inequalities can be rewritten after some algebra as

$$\begin{aligned} \delta\gamma_{i'} &> -\frac{\eta}{2} - \arccos\left(\sqrt{\sin^2\left(\frac{\eta}{2}\right) (\cos(\eta) + 2)}\right); \\ \delta\gamma_{i'} &< \frac{\eta}{2} + \cos^{-1}\left(\sqrt{\sin^2\left(\frac{\eta}{2}\right) (\cos(\eta) + 2)}\right), \end{aligned} \quad (\text{G1})$$

where  $\delta\gamma_{i'} = (\gamma_{i'} \bmod \pi) - \frac{\pi}{2}$  ( $|\delta\gamma_{i'}| < \frac{\pi+\eta}{2}$ ). One can show that at least one of the inequalities (G1) holds if  $|\eta| < \arccos(\sqrt{2}-1)$ . From the definition of  $\eta$  it follows that the latter inequality holds for any  $u_{\max} > \sqrt{1+\sqrt{2}}$ . This means that for this range of controls the  $i'$ -th corner point can be only either the left-most or the right-most corner point of time-optimal extremal. Using Fig. 5 one can accordingly improve the estimate for  $n_{\max}$ :  $n_{\max} \leq \left\lceil \frac{|\eta|}{\pi-|\eta|} + 2 \right\rceil \leq 2$  for  $u_{\max} > \sqrt{1+\sqrt{2}}$  Q.E.D.

## Appendix H: Proof of Proposition 10

Suppose that  $\tilde{r}_{i'}$  is interior corner point of the globally time-optimal solution. From (23) it follows that  $\tilde{r}_{i',x} = \frac{|\tilde{u}_i^+|}{\tilde{u}_i^+} \sin(\zeta_i) \sin\left(\frac{\xi}{2}\right) \propto c \sin(\zeta_i)$ , where  $c$  is some real constant. Since  $|\sin(\zeta_{i'})| < \sin\left(\frac{\pi+\eta}{2}\right)$  and  $|\zeta_{i'} - \zeta_{i'\pm 1}| = \frac{\pi+\eta}{2}$  the following inequality holds:

$$\frac{\tilde{r}_{i',x} - \tilde{r}_{i'\pm 1,x}}{\tilde{r}_{i',x}} > 0. \quad (\text{H1})$$

Proposition 3 states that the trajectory curve in vicinity of  $\tilde{r}_{i',x}$  should be  $\Lambda$ -shaped ( $V$ -shaped) in the case of  $\tilde{r}_{i',x} < 0$  ( $\tilde{r}_{i',x} > 0$ ), as shown in Fig. 11. Together with (H1) this means that both left and right adjacent arcs intersect the plane  $x = \tilde{r}_{i',x}$  twice and have the second common point  $\{\tilde{r}_{i',x}, -\tilde{r}_{i',y}, \tilde{r}_{i',z}\}$ . However, the globally time optimal trajectories can not have intersections with themselves. This contradiction proves the statement of Proposition. The associated maximal number of switchings can be directly counted using Fig. 5.

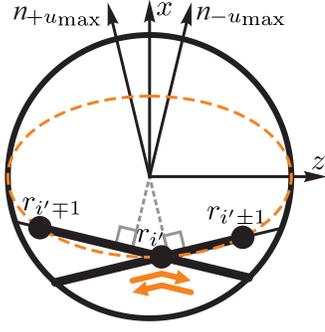


FIG. 11. Projection of the extremal on  $xz$ -plane in vicinity of the corner point  $\tilde{r}_{i'}$  in the case  $\tilde{r}_{i',x} < 0$ . Orange dashed ellipse is the projection of intersection of the Bloch sphere with the planes  $\lambda_{\pm 1}$ . Arrows indicates the admissible routes of passing the point  $\tilde{r}_{i'}$  according to Proposition 3.

### Appendix I: Proof of Proposition 11

The statement of Proposition will be proven by contradiction. Suppose that the first of inequalities (24) is violated (the case of violation of the second inequality can be treated similarly), i.e.  $\exists i : (\forall j : \tilde{r}_{i,x} \leq \tilde{r}_{j,x} \wedge \tilde{r}_{i,x} < 0)$ . Using Proposition 3 we conclude that  $\tilde{r}_{i,x} \leq \tilde{r}_{i-1,x}, \tilde{r}_{i+1,x}$  and that the trajectory around  $\tilde{r}_i$  is  $\Lambda$ -shaped:  $\exists \epsilon, \forall \delta \tau \in (-\epsilon, \epsilon) : \tilde{r}_x(\tilde{\tau}_i + \delta \tau) < \tilde{r}_x(\tilde{\tau}_i)$ . Similarly to the proof of Proposition 10, these observations mean that the both arcs  $\tau \in (\tilde{\tau}_{i-1}, \tilde{\tau}_i)$  and  $\tau \in (\tilde{\tau}_i, \tilde{\tau}_{i+1})$  should cross the plane  $x = \tilde{r}_{i,x}$  twice and thus have the common point  $\{\tilde{r}_{i,x}, -\tilde{r}_{i,y}, \tilde{r}_{i,z}\}$ . However, the latter contradicts with the assumed global time optimality of the trajectory  $r(\tau)$ .

### Appendix J: Proof of Proposition 12

Similarly to  $\tilde{r}^+$  and  $\tilde{r}^-$ , let us introduce the new notations  $r_{\pm} = \frac{\tilde{r}_1 + \tilde{r}_n}{2} \pm \text{sign}(|\tilde{r}_{1,x}| - |\tilde{r}_{n,x}|) \frac{\tilde{r}_1 - \tilde{r}_n}{2}$  for the first and the last corner points  $\tilde{r}_1$  and  $\tilde{r}_n$  of trajectory  $\tilde{r}(\tau)$ , so that  $|\tilde{r}_{+,x}| \geq |\tilde{r}_{-,x}|$ . Using Fig. 5 we find that

$$n_I = \left| \frac{\zeta_+ - \zeta_-}{\pi + \eta} \right| + 1 = \left| \frac{\arcsin(\tilde{r}_{+,x}\phi) - \arcsin(\tilde{r}_{-,x}\phi)}{2 \arctan(u_{\max}\phi)} \right| + 1, \quad (\text{J1})$$

where  $\phi = \frac{1}{\sin(\frac{\xi}{2})}$ . Eq. (J1) can be rewritten as

$$n_I = \frac{\int_0^\phi \left| \frac{\tilde{r}_{+,x}}{\sqrt{1-\phi^2\tilde{r}_{+,x}^2}} - \frac{\tilde{r}_{-,x}}{\sqrt{1-\phi^2\tilde{r}_{-,x}^2}} \right| d\phi}{\int_0^\phi \left( \frac{u_{\max}}{1+u_{\max}^2\phi^2} \right) d\phi} + 1. \quad (\text{J2})$$

The integrands in the numerator and denominator of (J2) are monotonically increasing and decreasing functions of  $\phi$  in the range of interest. Since  $\sin(\frac{\xi}{2}) \geq |\tilde{r}_{+,x}|$  one obtains the upper estimate  $n_I \leq n_{I,\max}$ , where

$$n_{I,\max} = n \Big|_{\phi = \frac{1}{|\tilde{r}_{+,x}|}} = \frac{\arccos\left(\frac{\tilde{r}_{-,x}}{\tilde{r}_{+,x}}\right)}{2 \arctan\left(\frac{u_{\max}}{|\tilde{r}_{+,x}|}\right)} + 1. \quad (\text{J3})$$

In order to make this result constructive, we will find the upper estimate for  $n_{I,\max}$  by replacing  $\tilde{r}_{+,x}$  and  $\tilde{r}_{-,x}$  in (J3) with their upper and lower estimates given in Proposition 11:  $|\tilde{r}_{-,x}| < |\tilde{r}_{+,x}| < |\tilde{r}_x^+|$ , and  $0 < |\tilde{r}_{-,x}| < |\tilde{r}_x^-|$ . Elementary analysis shows that  $n_{I,\max}(\tilde{r}_{+,x}, \tilde{r}_{-,x})$  is a monotonic function of  $\tilde{r}_{-,x}$  and reaches a maximum when  $\text{sign}(\tilde{r}_{+,x})\tilde{r}_{-,x}$  is minimal. At the same time,  $n_{I,\max}(\tilde{r}_{+,x}, \tilde{r}_{-,x})$  is a concave function of  $\tilde{r}_{+,x}$  when  $\tilde{r}_{+,x}\tilde{r}_{-,x} < 0$  and monotonically increasing function of  $|\tilde{r}_{+,x}|$  in the range  $\tilde{r}_{+,x}\tilde{r}_{-,x} > 0$ . Using these properties, we obtain inequality (25a) for the case  $\tilde{r}_x^+\tilde{r}_x^- < 0$  and the second of the estimates (25b) for the case  $\tilde{r}_x^+\tilde{r}_x^- > 0$ .

Note that the latter estimate directly accounts for the location of only one trajectory endpoint and can be further refined. Namely, due to (24) the corner points in the case  $\tilde{r}_{+,x}\tilde{r}_{-,x} > 0$  are located in the range  $\tilde{r}_{i,x} \in [0, \tilde{r}_x^+]$ . Since the  $x$ -coordinates of the corner points are monotonic functions of the index  $i$  (see Proposition 10 and Fig. 5), the trajectory can be split into two continuous parts  $R_1$  and  $R_2$  such that all  $n_{R_1}(n_{R_2})$  corner points in the segment  $R_1(R_2)$  belong to the range  $\tilde{r}_{i,x} \in (\tilde{r}_x^-, \tilde{r}_x^+]$  ( $\tilde{r}_{i,x} = [0, \tilde{r}_x^-]$ ), and their junction point  $\tilde{r}_c$  is chosen such that  $\tilde{r}_{c,x} = \tilde{r}_x^-$ . Using these range estimates and the extremal properties of function (J3) we obtain

$$\text{that } n_{R_1} \leq \frac{\arccos\left(\frac{\tilde{r}_x^-}{\tilde{r}_x^+}\right)}{2 \arctan\left(\frac{u_{\max}}{\tilde{r}_x^+}\right)} + 1. \quad \text{Let us show that } n_{R_2} \leq 3$$

(which will prove the first estimate in (25b)). Indeed, the duration  $\tilde{\Delta}\tau_{R_2}$  of this segment can not exceed  $\pi$  (the maximal duration of the trajectory with  $\tilde{u}(\tau) = 0$  connecting  $\tilde{r}^-$  and  $\tilde{r}_c$ ). At the same time, according to eq. (19) the minimal duration of each arc of the bang-bang trajectory is  $\frac{\pi}{2} \cos \alpha$ . Thus, the number of the interior bang segments of duration  $\tilde{\Delta}\tau$  in the case  $u_{\max} \leq 1$  can not exceed  $[2\sqrt{2}] = 2$ , i.e.  $n_{R_2} \leq 3$  (the same restriction for the case  $u_{\max} > 1$  trivially follows from Proposition (8)). Hence, Proposition is completely proven.

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